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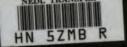
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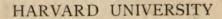
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# TABLES

MATHEMATICAL STATES







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6 tam (x+y) = tamy stamy 7 etn(x+y) = etn-xetny -1
ctny+etnx 8 pin(x-y) = sin x cosy-cosxsing q cos (x-y) = cosx cosy + pinx smy 10 tan(ry) = tany-tany 11 etn (x-y) = stn-x etny-101 etny-eth-x 12 Amax= samxeosk cos 3x = 4cos x-3cosx Am 3x = 3amx cos x-Am3x 13 cos 2x = cos 2x - Am 2x H tandy = 2 tank 15 etn 2 x = etn 2 x -1 16 sim = == = \ \ \frac{1-cos 2}{2} 17 cos 2 3 = ± \ Heos3 18 tan = = = 1-co 3 19 otn == = = 1+003 20 sin A tain B = 2 Sint (A+B) cost (A-B) or pinA-pin  $B = 2\cos \frac{1}{2}(A+13)\sin \frac{1}{2}(A-13)$ 12 cos A + cos B = 2 cos & (A+B) cos & (A-B) 23 cos A\_cos B = 2 sin \$ (A+B) sin \$ (A-B)

sin A+cos A = 1

4 prin(x+y)=sinxcosy+cosx siny

5 cos (xty) = cosxeosy-sinxamy

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3. Ani A xose A = 1 coo A x pec A = 1 tan A x etn A = 1 24 Ain A + Ain B = ton \( \frac{1}{2} (A+B) \)

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## LOGARITHMIC AND OTHER

## MATHEMATICAL TABLES

WITH EXAMPLES OF THEIR USE AND HINTS ON THE ART OF COMPUTATION

BY

#### SIMON NEWCOMB

Professor of Mathematics, in the Johns Hopkins University.



NEW YORK
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#### PREFACE.

In the present work an attempt is made to present to computers and students a set of logarithmic and trigonometric tables which shall have all the conveniences familiar to those who use German tables. The five-figure tables of F. G. GAUSS, of which fifteen editions have been issued, have, after long experience with them, been taken as the basis of the present ones, but modifications have been introduced wherever any improvement could be made.

Five places of decimals have been adopted as an advantageous mean. The results obtained by them, being nearly always reliable to the 10,000th part, are amply accurate for most computations, while the time of the student who uses them is not wasted in unnecessary calculation.

The Introduction is intended to serve not only as an explanation of the tables, but as a little treatise on the art of computation, and the methods by which the labor of computation may be abridged.

To avoid fostering the growing evil of nearsightedness among students, the author and publishers have spared neither pains nor expense in securing clearness of typography.



#### CONTENTS.

#### INTRODUCTION TO TABLES.

#### TABLE I.

LOGARITHMS OF NUMBERS.
Introductory Definitions
The Use of Logarithms
Arrangement of the Table of Logarithms
Characteristics of Logarithms
Interpolation of Logarithms
Labor-Saving Devices
Number Corresponding to Given Logarithm
Adjustment of Last Decimal
The Arithmetical Complement
Practical Hints on the Art of Computation
Imperfections of Logarithmic Calculation
Applications to Compound Interest and Annuities 25
Accumulation of an Annuity 28
TABLE II.
MATHEMATICAL CONSTANTS.
Explanation
TABLES III. AND IV.
LOGARITHMS OF TRIGONOMETRIC FUNCTIONS.
Angles less than 45° 32
Angles between 45° and 90°
Angles greater than 90°
Methods of Writing the Algebraic Signs
Angle Corresponding to a Given Function
Cases when the Function is very Small or Great
TABLE V.
NATURAL SINES AND COSINES.
Explanation. 42

#### TABLE VI.

Addition and Subtraction Logarithms.
PAGE
Use in Addition
Use in Subtraction
Special Cases
TABLE VIL
SQUARES OF NUMBERS,
Explanation
TABLE VIII.
Hours, Minutes, and Seconds into Decimals of a Day.
Explanation
TABLE IX.
To Convert Time into Arc.
Explanation
TABLE X.
Mean and Sidereal Time.
Explanation 55
OF DIFFERENCES AND INTERPOLATION.
General Principles
Fundamental Formulæ61
Transformations of the Formulæ
Formulæ of Stirling and Bessel
Special Cases of Interpolation—Interpolation to Halves 64
Interpolation to Thirds 66
Interpolation to Fifths
FORMULÆ FOR THE SOLUTION OF PLANE AND SPHERICIAL TRIANGLES.
Remarks
Formulæ

#### TABLES I. TO X.

#### TABLE I.

#### LOGARITHMS OF NUMBERS.

#### 1. Introductory Definitions.

Natural numbers are numbers used to represent quantities.

The numbers used in arithmetic and in the daily transactions of life are natural numbers.

To every natural number may be assigned a certain other number, called its logarithm.

The **logarithm** of a natural number is the exponent of the power to which some assumed number must be raised to produce the first number. The assumed number is called the **base**. E.g., the logarithm of 100 with the base 10 is 2, because  $10^2 = 100$ ; with the base 2, the logarithm of 64 would be 6, because  $2^6 = 64$ .

A system of logarithms means the logarithms of all positive numbers to a given base.

Although there may be any number of systems of logarithms, only two are used in practice, namely:

- 1. The natural or Napierian system, base = e = 2.718282.
- 2. The common system, base = 10.

The natural system is used for purely algebraic purposes.

The common system is used to facilitate numerical calculations and is the only one employed in this book.

If the natural number is represented by n, its logarithm is called  $\log n$ .

A logarithm usually consists of an integer number and a decimal part.

The integer is called the **characteristic** of the logarithm. The decimal part is called the **mantissa** of the logarithm.

A table of logarithms is a table by which the logarithm of any given number, or the number corresponding to any given logarithm, may be found.

The most simple form of table is that on the first page of Table I., which gives the logarithms of all entire numbers from 1 to 150; each logarithm being found alongside its number. The student may begin his exercises with this table.

Mathematical tables in general enable us, when one of two related quantities is given, to find the other.

In such tables the quantity supposed to be given is called the argument.

The argument is usually printed on the top, bottom, or side of the table.

The quantities to be found are called **functions** of the argument, and are found in the same columns or lines as the argument, but in the body of the table.

In a table of logarithms the natural number is the argument, and the logarithm is the function.

#### 2. The Use of Logarithms.

The following properties of logarithms are demonstrated in treatises on algebra.

- I. The logarithm of a product is equal to the sum of the logarithms of its factors.
- II. The logarithm of a quotient is found by subtracting the logarithm of the divisor from that of the dividend.
- III. The logarithm of any power of a number is equal to the logarithm of the number multiplied by the exponent of the power.
- IV. The logarithm of the root of a number is equal to the logarithm of the number divided by the index of the root.

We thus derive the following rules:

To find the product of several factors by logarithms.

Rule. Add the logarithms of the several factors. Enter the table with the sum as a new logarithm, and find the number corresponding to it.

This number is the product required.

Example 1. To multiply  $7 \times 8$ .

We find from the first page of Table I.

log 7 = 0.84510" 8 = 0.90309

Sum of logs = 1.74819 = log of product.

Having added the logarithms, we look in column log for a num-

ber corresponding to 1.788 19 and find it to be 56, which is the product required.

Ex. 2 To find the continued product  $2 \times 6 \times 8$ .

Sum of logs,  $1.98227 = \log product$ .

The number corresponding to this logarithm is found to be 96, which is the product required.

Ex. 3. To find the quotient of  $147 \div 21$ .

log 147, 2.167 32 " 21, 1.322 22

Difference, 0.845 10

We find this difference to be the logarithm of 7, which is the required quotient.

Ex. 4. To find the quotient arising from dividing the continued product  $98 \times 102 \times 148$  by the continued product  $21 \times 37 \times 68$ .

log 21, 1.322 22 log 98, 1.991 23 " 37, 1.568 20 " 102, 2.008 60 " 68, 1.832 51 " 148, 2.170 26

Sum = log divisor, 4.722 93 Sum = log dividend, 6.170 09 log divisor, 4.722 93

Difference = log quotient, 1.447 16

Looking into the table, we find the number corresponding to this logarithm to be 28, which is the required quotient.

NOTE. The student will notice that we have found this quotient without actually determining either the divisor or dividend, having used only their logarithms. If he will solve the problem arithmetically, he will see how much shorter is the logarithmic process.

Ex. 5. To find the seventh power of 2.

We have  $\log 2 = 0.30103$ 

 $\frac{1}{2.10721} = \log 128$ 

Hence 128 is the required power.

Ex. 6. To find the cube root of 125.

 $\frac{3 \mid 2.09691}{0.69897}$ 

The index of the root being 3, we divide the logarithm of 125 by it. Looking in the tables, we find the number to be 5, which is the root required.

#### Exercises.

Compute the following products, quotients, powers, and roots by logarithms.

1. 11.13. Ans. 143. 5. 
$$\frac{22.8^{\circ}}{\sqrt{121}}$$
. Ans. 128. 2. 12°. Ans. 144. 6.  $\frac{51.98\sqrt{81}}{34.63}$ . Ans. 21. 3.  $\frac{12^{\circ}}{6^{\circ}}$ . Ans. 48. 7.  $\frac{2^{\circ}.3^{\circ}}{6^{\circ}}$ . Ans. 144. 4.  $\frac{2.9^{\circ}.91.78}{13^{\circ}.21.3}$ . Ans. 108. 8.  $\frac{54.48}{8.9}$ . Ans. 36.

#### 3. Arrangement of the Table of Logarithms.

A table giving every logarithm alongside its number, as on the first page of Table I., would be of inconvenient bulk. For numbers larger than 150 the succeeding parts of Table I. are therefore used. Here the first three figures of the natural number are given in the left-hand column of the table. The first figure must be understood where it is not printed. The fourth figure is to be sought in the horizontal line at the top or bottom. The mantissa of the logarithm is then found in the same line with the first three digits, and in the column having the fourth digit at the top.

To save space the logarithm is not given in the column, but only its last three figures. The first two figures are found in the first column, and are commonly the same for all the logarithms in any one line.

Example 1. To find the logarithm of 2090.

We find the number 209, the figure 2 being omitted in printing, in the left-hand column of the table, and look in the column having the fourth figure, 0, at its top or bottom. In this column we find 320 15, which is the mantissa of the logarithm required.

Ex. 2. To find the logarithm of 2092.

Entering the table with 209 in the left-hand column, and choosing the column with 2 at the top, we find the figures 056. To these we prefix the figures 32 in column 0, making the total logarithm .320 56. Therefore

Mantissa of  $\log 2092 = .32056$ .

#### EXERCISES.

Find in the same way the mantissæ of the logarithms of the following numbers:

2240;	5133;
2242;	5256;
2249;	5504;
2895;	8925;
3644;	9557;
4688:	9780.

When the first two figures of the mantissa are not found in the same line in which the number is sought, they are to be found in the first line above which contains them.

Example. The first two figures of log 6250 are 79, which belongs to all the logarithms below as far as 6309. Therefore mantissa of  $\log 6250 = .79588$ .

#### EXERCISES.

Find the mantissæ of the logarithms of

6300; answer, .799 34. 6309; ".799 96. 6434; 6653; 6755; 6918; 7868.

Exception. There are some cases in which the first two figures change in the course of the line. In this case the first two figures are to be sought in the line above before the change and in the line next below after the change.

Example. The mantissa of log 6760 is .829 95. But the mantissa of log 6761 is .830 01. In this case the figures 83 are to be found in the next line below. To apprise the computer of these cases, each of the logarithms in which the two first figures are found in the line below is indicated by an asterisk.

#### EXERCISES.

#### Find the mantissa of

log 1022; answer, .009 45. log 1024; ".010 30.

1231;	1999;
1387;	3988;
1419;	4675;
1621;	4798;
1622;	5377;
1862;	8512;
1863;	1009.

#### 4. Characteristics of Logarithms.

The part of the table here described gives only the mantissa of each logarithm. The characteristic must be found by the general theory of logarithms.

The following propositions are explained in treatises on algebra:

$\mathbf{T}$ he	logarithm	of	1	is	0.
"	"	"	10	"	1.
"	"	"	100	"	2.
"	"	"	1000	"	3.
66	"	"	10 <sup>n</sup>	"	22

Since any number of one digit is between 0 and 10, its logarithm is between 0 and 1; that is, it is 0 plus some fraction. In the same way, the logarithm of a number of two digits is 1 + a fraction. And in general,

The characteristic of the logarithm of any number greater than 1 is less by unity than the number of its digits preceding the decimal point.

Example. The characteristic of the logarithm of any number between 1 and 10 is 0; between 10 and 100 it is 1; between 100 and 1000 it is 2, etc.

It is also shown in algebra that if a number be divided by 10 we diminish its logarithm by unity.

Logarithms of numbers less than unity are most conveniently expressed by making the characteristic alone negative.

For example:

$$\log 0.2 = \log 2 - 1 = -1 + .30103;$$
  
"  $0.02 = \log 2 - 2 = -2 + .30103.$ 

Hence: The mantissæ of the logarithms of all numbers which differ only in the position of the decimal point are the same.

Hence, also, in seeking a logarithm from the table we find the mantissa without any reference to the decimal point. Afterward we affix the characteristic according to the position of the decimal point.

For convenience, when a negative characteristic is written the minus sign is put above it to indicate that it extends only to the characteristic below it and not to the mantissa. Thus we write

$$\log .02 = \overline{2}.30103.$$

In practice, however, it is more common to avoid the use of negative characteristics by increasing them by 10. We then write

$$\log .02 = 8.30103 - 10.$$

If we omitted to write -10 after the logarithm, the latter would, in strictness, be the log of  $2 \times 10^{\circ}$ . But numbers so great as this product occur so rarely in practice that it is not generally necessary to write -10 after the logarithm. This may be understood.

A convenient rule for remembering what characteristic belongs to the logarithm of a decimal fraction is:

The characteristic is equal to 9, minus the number of zeros after the decimal point and before the first significant figure.

Examples. 
$$\log 34060 = 4.53224$$

"  $340.60 = 2.53224$ 

"  $3.4060 = 0.53224$ 

"  $.03406 = 8.53224 - 10$ 

"  $.0003406 = 6.53224 - 10$ 

It will be seen that we can find the logarithms of numbers from 1 to 150 without using the first page of the table at all, since all the mantissæ on this page are found on the following pages as logarithms of larger numbers.

#### EXERCISES.

Find the logarithms of the following numbers:

1.515	.003 899
.01 702	0.4276
18.62	464 700
.03 735	98.030

Find the numbers corresponding to the following logarithms:

```
3.241 80; 8.750 35 — 10; 9.999 91 — 10;

1.191 45; 7.411 28 — 10; 5.999 96;

5.653 21; ans. 450 000 6.889 97 — 10; 2.960 28;

6.748 27; ans. 5 601 000 9.116 94 — 10; 0.886 27;

7.560 03; ans. 36 310 000 7.250 18 0.000 87.
```

#### 5. Interpolation of Logarithms.

In all that precedes we have used only logarithms of numbers containing not more than 4 significant digits. But in practice numbers of more than four figures have to be used. To find the logarithms of such numbers the process of interpolation is necessary. This process is one of simple proportion, which can be seen from the following example.

To find log. 1167.23.

The table gives the logarithms of 1167 and of 1168, which we find to be as follows:

 $\log 1167 = 3.067 07$ " 1168 = 3.067 44Difference of logarithms = .000 37

Now the number of which we wish to find the logarithm being between these numbers, its logarithm is between these logarithms; that is, it is equal to 3.067 07 plus a fraction less than .000 37.

Since the difference 37 corresponds to the difference of unity in the two numbers, we assume that the quantity to be added to the logarithm bears the same proportion to .23 that 37 does to unity. We therefore state the proportion

1:.23:: 37: increase required.

The solution of this proportion gives  $.23 \times 37 = 8.51$ , which is the quantity to be added to log 1167 to produce the logarithm required.\* The result is 3.067 155 1.

But our logarithms extend only to five places of decimals, while the result we have written has seven. We therefore take only five places of decimals. If we write the mantissa 3.06715, the result will be too small by .51. If we write 3.06716, it will be too great by .49. Since the last result is nearer than the first, we give it the preference, and write for the required logarithm

 $\log 1167.23 = 3.06716.$ 

We thus have the following rule for interpolating:

Take from the table the logarithm corresponding to the first four significant digits of the number.

Considering the following digits as a decimal fraction, multiply the difference between the logarithm and the next one following by such decimal fraction.

<sup>\*</sup>In this multiplication we have used a decimal point to mark off the fifth order of decimals. This is a convenient process in all such computations.

This product being added to the logarithm of the table will give the logarithm required.

The whole operation by which we have found log 1167.23 would then be as follows:

The products for interpolation, 7.4 and 1.11, may be found by multiplying by the fifth and sixth figures of the number separately.

To facilitate this multiplication, tables of proportional parts are given in the margin. Each difference between two logarithms will be readily found in heavy type not far from that part of the table which is entered, and under it is given its product by .1, .2, etc., . . .9. We therefore enter this little table with the fifth figure, and take out the corresponding number to be added to the logarithm. Then if there is a sixth figure, we enter with that also and move the decimal one place to the left. We then add the two sums to the logarithm.

#### 6. Labor-saving Devices.

In using a table of logarithms, the student should accustom himself to certain devices by which the work may be greatly facilitated.

In the first place it is not necessary to take the whole difference between two consecutive logarithms. He has only to subtract the last figure of the preceding logarithm from the last one of the following, increased by 10 if necessary, and thus find the last figure of the difference.

The nearest difference in the margin of the table having this same last figure will always be the difference required.

Example. If the first four figures of the number are 1494, instead of subtracting 435 from 464 we say 5 from 14 leaves 9, and look for the nearest difference which has 9 for its last figure. This we readily find to be 29, at the top of the next page.

NOTE. In nearly all cases the difference will be found on the same page with the logarithm. The only exception is at the bottom of the first page, where, owing to the number of differences, they cannot all be printed.

In the preceding examples we have written down the numbers in full, which it is well that the beginner should do for himself. But after a little practice it will be unnecessary to write down anything but the logarithm finally taken out. The student should accustom himself to take the proportional parts mentally, adding them to the logarithm of the table and writing down the sum at sight. The habit of doing this easily and correctly can be readily acquired by practice.

Exercises. Find the logarit	hms of
792 638;	0.99997;
1000.77;	949.916;
1000.07;	20.8962;
100 007;	660 652;
181 982;	77.642;
281.936;	8.8953.

As a precaution in taking out logarithms, the computer should always, after he has got his result, look into the table and see that it does really fall between two consecutive logarithms in the table.

If the fraction to be interpolated is nearly unity, especially if it is equal to or greater than 9, it will generally be more convenient to multiply the difference of the logarithms by the complement\* of the fraction and subtract the product from the logarithm next succeeding. The following are examples of the two methods, which may always be applied whether the fraction be large or small:

 $\log 1004.28 = \log (1005 - .72).$ Example 1. log 1004, .001 73 log 1005, .002 17 pr. pt. for .7, pr. pt. for .2, 8.8 -30.866 66 66 66 66 66 .08, 3.5 .02, log, 3.001 85 log, 3.001 85 Ex. 2.  $\log 154993 = 155000 - 7$ . log 1549, .190 05 1550, .190 33 25.2 pr. pt. for -.07, pr. pt. for .9, -1.9666 66 66 0.8 .03, log, 5.190 31 log, 5.19031

<sup>\*</sup>By the complement or arithmetical complement of a decimal fraction is here meant the remainder found by subtracting it from unity or from a unit of the next order higher than itself. Thus:

co. .723 = .277 co. .1796 = .8204 co. .9982 = .0068.

## 7. To find the Number corresponding to a given Logarithm.

The reverse process of finding the number corresponding to a given logarithm will be seen by the following example:

To find the number of which the logarithm is 2.027 90.

Entering the table, we find that this logarithm does not exactly occur in the table. We therefore take the next smaller logarithm, which we find to be as follows:

 $\log 1066 = 2.02776$ .

Subtracting this from the given logarithm we find the latter to be greater by 14, while the difference between the two logarithms of the table is 40. We therefore state the proportion

40:14::1 to the required fraction.

The result is obtained by dividing 14 by 40, giving a quotient .35. The required number is therefore 106.635. It will be remarked that we take no account of the characteristic and position of the decimal until we write down the final result, when we place the decimal in the proper position.

The table of proportional parts is used to find the fifth and sixth figures of the number by the following rule:

If the given logarithm is not found in the table, note the excess of the given logarithm above the next smaller one in the table, which call  $\Delta$ .

Take the difference of the two tabular logarithms, and find it among the large figures which head the proportional parts.

That proportional part next smaller than  $\Delta$  will be the fifth figure of the required number.

Take the excess of  $\Delta$  above this proportional part; imagine its decimal point removed one place to the right, and find the nearest number of the table.

This number will be the sixth figure of the required number.

Example. To find the number of which the logarithm is 2.193 59.

Entering the table, we find the next smaller logarithm to be .193 40. Therefore  $\Delta = 19$ .

Also its tabular difference = 28.

Entering the table of proportional parts under 28, we find 16.8 opposite 6 to be the number next smaller than 19 the value of  $\triangle$ . Therefore the fifth figure of the number is 6.

The excess of 19 above 16.8 is 2.2. Looking in the same table for the number 22, we find the nearest to be opposite 8.

Therefore the fifth and sixth figures of the required number are 68. Now looking at the log .193 40 and taking the corresponding number, we find the whole required number to be

156 168.

The characteristic being 2, the number should have three figures before the decimal point. Therefore we insert the decimal point at the proper place, giving as the final result 156.168.

#### 8. Number of Decimals necessary.

In the preceding examples we have shown how with these tables the numbers may be taken out to six figures. In reality, however, it will seldom be worth while to write down more than five figures. That is, we may be satisfied by adding only one figure to the four found from the table. In this case, when we enter the table of proportional parts, we take only the number corresponding to the nearest proportional part.

To return to the last preceding example, where we find the number corresponding to 2.19359. We find under the difference 28 that the number nearest 19 is 19.6, which is opposite 7.

Therefore the number to be written down would be 156.17.

In the following exercises it would be well for the student to write six figures when the number is found on one of the first two pages of the table and only five when on one of the following pages. The reason of this will be shown subsequently.

#### EXAMPLES AND EXERCISES.

1. To find the square root of §.

We have log 3. 0

log \$, 0.176 09

+ 2,  $\log \sqrt{\frac{2}{8}}$ , 0.088 04

Here we have a case in which the half of an odd number is required. We might have written the last logarithm 0.088 045, but we should then have had six decimals, whereas, as our tables only give five decimals, we drop the sixth. If we write 4 for the fifth figure it will be too small by half a unit, and if we write 5 it will be too large by half a unit. It is therefore indifferent which figure we write, so far as mere accuracy is concerned.

A good rule to adopt in such a case is to write the nearest EVEN number. For example,

for the half of .261 81 we write .130 90; .261 83 .130 92: .261 85 .130 92: " .261 87 .130 94; " 66 .261 89 .130 94: " .261 97 " .130 98; " " .261 99 .131 00.

Returning to our example, we find, by taking the number corresponding to 0.08804,

$$\sqrt{\frac{3}{4}} = 1.22472.$$

2. To find the square root of 3.

The last logarithm is the same as

$$9.91196 - 10.$$

which is the form in which it is to be written in order to apply the rule of characteristics. The corresponding number is 0.816 50.

We have here a case in which, had we neglected considering the surplus -10 as we habitually do, the characteristic of the answer would have been 4 instead of 9 or -1. The easiest way to treat such cases is this:

When we have to divide a logarithm in order to extract a root, instead of increasing the characteristic by 10, increase it by 10  $\times$  index of root.

Thus we write  $\log \frac{2}{3} = 19.823 \ 91 - 20$ . Dividing by 2,  $\log \sqrt{\frac{2}{3}} = 9.911 \ 96 - 10$ , which is in the usual form.

3. To find the cube root of \frac{1}{2}.

which we write in the form

$$\log \frac{1}{2} = 29.69897 - 30.$$

Dividing this by 3,

$$\frac{1}{8}\log\frac{1}{2} = \log^{8}\sqrt{\frac{1}{2}} = 9.89966 - 10.$$

This logarithm is in the usual form, and gives

$$\sqrt[8]{\frac{1}{2}} = 0.79370.$$

The affix -30, or  $-10 \times \text{divisor}$ , can be left to be understood in these cases as in others. All that is necessary to attend to is that instead of supposing the characteristic to be one or more units less than 10, as in the usual run of cases, we suppose it to be one or more units less than  $10 \times \text{divisor}$ .

Find:

- 4. The square root of  $\frac{1}{2}$ ;
- 5. The cube root of 2;
- 6. The fourth root of 3;
- 7. The fifth root of 20;
- 8. The tenth root of 10;
- 9. The tenth root of 1.

#### 9. The Arithmetical Complement.

When a logarithm is subtracted from zero, the remainder is called its arithmetical complement.

If L be any logarithm, its arithmetical complement will be — L. Hence if

 $L = \log n$ .

then

arith. comp. 
$$= -L = \log \frac{1}{n}$$
;

that is,

The arithmetical complement of a given logarithm is the logarithm of the reciprocal of the number corresponding to the given logarithm.

Notation. The arithmetical complement of a logarithm is written co-log. It is therefore defined by the form

co-log 
$$n = \log \frac{1}{n}$$
.

Finding the arithmetical complement. To find the arithmetical complement of  $\log 2 = 0.30103$ , we may proceed thus:

co-log 2, 
$$9.69897 - 10$$
.

We subtract from zero in the usual way; but when we come to the characteristic, we subtract it from 10. This makes the remainder too large by 10, so we write -10 after it, thus getting a quantity which we see to be  $\log 0.5$ .

We may leave the - 10 to be understood, as already explained.

The arithmetical complement may be formed by the following rule:

Subtract each figure of the logarithm from 9, except the last significant one, which subtract from 10. The remainders will form the arithmetical complement.

For example, having, as above, the logarithm 0.30103, we form, mentally, 9-0=9; 9-3=6; 9-0=9; 9-1=8; 9-0=9; 10-3=7; and so write

9.698 97

as the arithmetical complement.

To form the arithmetical complement of 3.284 00 we have 9-3=6; 9-2=7; 9-8=1; 10-4=6. The complement is therefore

6.716 00.

The computer should be able to form and write down the arithmetical complement without first writing the tabular logarithm, the subtraction of each figure being performed mentally.

Use of the arithmetical complement. The co-log is used to substitute addition for subtraction in certain cases, on the principle: To add the co-logarithm is the same as to subtract the logarithm.

Example. We may form the logarithm of \( \frac{3}{2} \) in this way by addition:

Here there is really no advantage in using the co-log. But there is an advantage in the following example:

To find the value of  $P = \frac{2763 \times 419.24}{99}$ . We add to the logarithms of the numerator the co-log of the denominator, thus:

The use of the arithmetical complement is most convenient when the divisor is a little less than some power of 10.

#### EXERCISES.

Form by arithmetical complements the values of:

1. 
$$\frac{109 \times 216.26}{0.99316}$$
2. 
$$\frac{8263 \times 9162.7}{92 \times 99.618}$$
3. 
$$\frac{4 \times 6 \times 8219}{9 \times 992}$$

#### 10. Practical Hints on the Art of Computation.

The student who desires to be really expert in computation should learn to reduce his written work to the lowest limit, and to perform as many of the operations as possible mentally. We have already described the process of taking a logarithm from the table without written computation, and now present some exercises which will facilitate this process.

1. Adding and subtracting from left to right. If one has but two numbers to add it will be found, after practice, more easy and natural to write the sum from the left than from the right. The method is as follows:

In adding each figure, notice, before writing the sum, whether the sum of the figures following is less or greater than 9, or equal to it.

If the sum is less than 9, write down the sum found, or its last figure without change.

If greater than 9, increase the figure by 1 before writing it down.

If equal to 9, the increase should be made or not made according as the first sum following which differs from 9 is greater or less than 9.

If the first sum which differs from 9 exceeds it, not only must we increase the number by 1, but must write zeros under all the places where the 9's occur. If the first sum different from 9 is less than 9, write down the 9's without change.

The following example illustrates the process:

Here 7 and 8 are 15. 5+2 being less than 9, we write 15 without change. 3+0 being less than 9, we write 7 without change. 9+2 being greater than 9, we increase the sum 3+0 by 1 and write down 4. 7+1 being

less than 9, we write the last figure of 9+2, or 1, without change. 6+7 being greater than 9, we increase 7+1 by 1 and write down 9. Under 6+7 we write down 3 or 4. To find which, 8+1=9; 3+6=9; 5+4=9; 7+5=12. This first sum which is different from 9 being greater than 9, we write 4 under 6+7, and 0's in the three following places where the sums are 9. 7+5=12. Since 8+0<9, we write down 2. Before deciding whether to put 8 or 9 under 8+0, we add 5+4=9; 8+1=9; 8+1=9; 9+0=9; 2+2=4. This being less than 9, we write 8 under 8+0, and 9's in the four following places. Since 5+8=13>9, we write 5 under 2+2. Since 9+3=12>9, we write 4 under 5+8. Since 8+7=15>9, we write 3 under 9+3. Finally, under 8+7 we write 5.

This process cannot be advantageously applied when more than two numbers are to be added.

#### EXERCISES.

Let the student practise adding each consecutive pair of the following lines, which are spaced so that he can place the upper margin of a sheet of paper under the lines he is adding and write the sum upon it.

2	5	0	9	1	7	2	8	5	3	1	6	9	8	1	2	0	8
2	5	1	2	3	<b>5</b> .	9	6	4	6	9	2	1	8	4	3	6	8
7	9	1	6	1	5	8	3	2	3	1	6	6	4	6	8	9	ĺ
2	0	8	5	3	2	1	6	4	3	7	9	1	0	2	9	0	9
8	6	8	5	8	8	9	6	4	3	4	2	9	4	4	8	2	5
9	8	7	6	5	4	3	2	1	0	1	2	3	4	5	6	7	4

Subtracting. We subtract each figure of the subtrahend from the corresponding one of the minuend (the latter increased by 10 if necessary), as in arithmetic.

Before writing down the difference, we note whether the following figure of the subtrahend is greater, less, or equal to the corresponding figure of the minuend.

If greater, we diminish the remainder by 1 and write it down.\*

If less, we write the remainder without change.

If equal, we note whether the subtrahend is greater or less than the minuend in the first following figure in which they differ.

If greater, we diminish the remainder by 1, as before, and write 9's under the equal figures.

<sup>\*</sup> If the student is accustomed to carrying 1 to the figures of the minuend when he has increased the figure of his subtrahend by 10, he may find it easier to defer each subtraction until he sees whether the remainder is or is not to be diminished by 1, and, in the latter case, to increase the minuend by 1 before subtracting.

If less, write the remainder unchanged, putting 0's under the equal figures.

Example.

Here 7-2=5; because 4>2, we write 4. 12-4=8; because 2=2 and 6<9, we write 8; and write 0 in the following place. 9-6=3; because 8>8, we write 2. 18-8=5; 5=5; 1=1; 8>6; so under 13-8 we write 4, with 9's in the two next places. 16-8=8; because 0<2, we write 8. 2-0=2; 1=1; 4=4; 1<3; so under 2-0 we write 2, followed by 0's. 3-1=2; because 9=9, 8>4, we write 1, with 9 in the next place. 14-8=6, which we write as the last figure.

#### EXERCISES.

The preceding exercises in addition will serve as exercises in subtraction by subtracting each line from that above or below it. The student should be able to subtract with equal facility whether the minuend is written above or below the subtrahend.

Mental addition and subtraction. When an expert computer has to add or subtract two logarithms, as in forming a product or quotient of two quantities, he does not necessarily write both of them, but prefers to write the first and, taking the other mentally, add (or subtract) each figure in order from left to right, and write down the sum (or difference). He thus saves the time spent in writing one number, and, sometimes, the inconvenience of writing it where there is not sufficient room for it.

This process of inverted addition is most useful in adding the proportional part in taking a logarithm from the table. It is then absolutely necessary to save the computer the trouble of copying both logarithm and proportional part.

Expert computers can add seven-figure logarithms in this way without trouble. But with those who do not desire to become experts it will be sufficient to learn to add two or three figures, so as to be able to take a five-figure or seven-figure logarithm from the table without writing anything but the result.

#### 11. Imperfections of Logarithmic Calculations.

Nearly all practical computations with logarithms are affected by certain sources of error, arising from the omission of decimals. It is important that these errors should be understood in order not only to avoid them so far as possible, but to avoid spending labor in aiming at a degree of accuracy beyond that of which the numbers admit.

Mathematical results may in general be divided into two classes: (1) those which are absolutely exact, and (2) those which are only to a greater or less degree approximate.

As an example of the former case, we have all operations upon entire numbers which involve only multiplication and division. For example, the equations

$$\frac{16^2 = 256}{8^2} = \frac{16}{9}$$

are absolutely exact.

powerful microscope.

But if we express the fraction  $\frac{1}{7}$  as a decimal fraction, we have  $\frac{1}{7} = .142857...$ , etc., ad infinitum.

Hence the representation of ‡ as a decimal fraction can never be absolutely exact. The amount of the error will depend upon how many decimals we include. If we use only two decimals we shall certainly be within one hundredth; if three, within one thousandth, etc. Hence the degree of accuracy to which we attain depends upon the number of decimals employed. By increasing the number of decimals we can attain to any degree of accuracy. As an example, it is shown in geometry that if the ratio of the circumference of a circle to its diameter be written to 35 places of decimals, the result will give the whole circumference of the visible universe

without an error as great as the minutest length visible in the most

There are no numbers, except the entire powers of 10, of which the logarithms can be exactly expressed in decimals. We must therefore omit all figures of the decimal beyond a certain limit. The number of decimals to be used in any case depends upon the degree of accuracy which is required. The large tables of logarithms contain seven decimal places, and therefore give results correct to the ten-millionth part of the unit. This is sufficiently near the truth in nearly all the applications of logarithms.

With five places of decimals our numbers will be correct to the hundred-thousandth part of a unit. This is sufficiently near for most practical applications.

Accumulation of errors. When a long computation is to be made, the small errors are liable to accumulate so that we cannot rely upon this degree of accuracy in the final result. The manner

in which the tables are arranged so as to reduce the error to a minimum may be shown as follows:

We have to seven places of decimals

$$\log 17 = 1.2304489$$
"  $18 = 1.2552725$ 

When the tables give only five places of decimals the two last figures must be omitted. If the tables gave log 17=.23044, the logarithm would be too small by 89 units in the seventh place. It is therefore increased by a unit in the fifth place, and given .23045. This quantity is then too large by 11, and is therefore nearer the truth than the other. The nearest number being always given, we have the result:

Every logarithm in the table differs from the truth by not more than one half a unit of the last place of decimals.

Since the error may range anywhere from zero to half a unit, and is as likely to have one value as another between those limits, we conclude:

The average error of the logarithms in the tables is one fourth of a unit of the last place of decimals.

Errors in interpolation. When we interpolate the logarithm we add to the tabular logarithm another quantity, the proportional part, which may also be in error by half a unit, but of which the average error will only be one fourth of a unit.

As most logarithms have to be interpolated, the general result will be:

An interpolated logarithm may possibly be in error by a unit in the last place of decimals.

The sum of the average errors will, however, be only half a unit. But these errors may cancel each other, one being too large and the other too small. The theory of probabilities shows that, in consequence of this probable cancellation of errors, the average error only increases as the square root of the number of erroneous units added.

The square root of 2 is 1.41.

If, therefore, we add two quantities each affected with a probable error  $\pm$  .25, the result will be, for the probable error of the sum,

$$1.41 \times .25 = 0.35$$
.

We therefore conclude:

The average error of a logarithm derived from the table by interpelation is 0.35 of a unit of the last place.

Applying the above rule of the square root to the case in which

several logarithms are added or subtracted to form a quotient, we find the results of the following table:

No. of logs added or subtracted.	Average error.
1	0.35
2	0.50
3	0.63
4	0.72
δ	0.81
6	0.88
7	0.95
8	1.02
9	1.08
10	1 14

From this table we see that if we form the continued product of eight factors, by adding their logarithms the average error of the sum of the logarithms will be more than a unit in the last place.

As an example of the accumulation of errors, let us form the product 11.13.

We have from the table

$$\log 11 = 1.04139$$
" 13 = 1.11394
$$\log \text{ product}, 2.15533$$

We see that this is less than the given logarithm of the product 143 by a unit of the fifth order. But if we use seven decimals we have log 11, 1.041 392 7

Comparing this with the computation to five places, we see the source of the error.

If the numbers with which we enter the tables are affected by errors, these errors will of course increase the possible errors of the logarithms.

In determining to what degree of accuracy to carry our results, we have the following practical rule:

It is never worth while to carry our decimals beyond the limit of precision given by the tables, which limit may be a considerable fraction of the unit in the last figure of the tables.

Let us have a logarithm to five places of decimals, 1.929 49, of which we require the corresponding number. Entering the table, we

perceive that the corresponding number is between 85.01 and 85.02. If this logarithm is the result of adding a number of logarithms, each of which may be in error in the way pointed out, we may suppose it probably affected by an error of half a unit in the last figure and possibly by an error of a whole unit or more. That is, its true value may be anywhere between 92 948 and 92 950.

The number corresponding to the former value is 85.012, and that corresponding to the latter 85.016. Since the numbers may fall anywhere between these limits, we assign to it a mean value of 85.014, which value, however, may be in error by two units in the last place. It is not, therefore, worth while to carry the interpolation further and to write more than five digits.

Next suppose the logarithm to be 2.02170. Entering the table, we find in the same way that the number probably lies between the limits 105.121 and 105.126. There is therefore an uncertainty of five units in the sixth place, or half a unit in the fifth place. If the greatest precision is desired, we should write 105.124. But our last figure being doubtful by two or three units, the question might arise whether it were worth while to write it at all. As a general rule, if the sixth figure is required to be exact, we must use a six- or seven-place table of logarithms.

Still, near the beginning of the table, the probable error will be diminished by writing the sixth figure.

Now knowing that at the beginning of the table a difference of one unit in the number makes a change ten times as great in the logarithm as at the end of the table, we reach the conclusions:

In taking out a number in the first part of the table, it can never be worth while to write more than six significant figures, and very little is added to the precision by writing more than five.

In the latter part of the table it is never worth while to write more than five significant figures.

Sometimes no greater accuracy is required than can be gained by using four-figure logarithms. There is then no need of writing the last figure. If, however the printed logarithm is used without change, the fourth figure must be increased by unity whenever the fifth figure exceeds 5. When the fifth figure is exactly 5, the increase should or should not be made according as the 5 is too small or too great. To show how the case should be decided, a stroke is printed above the 5 when it is too great. In these cases the fourth figure should be used as it stands, but, when there is no stroke, it should be increased by unity.

## 12. Applications of Logarithms to the Computation of Annuities and Accumulations of Funds at Compound Interest.

One of the most useful applications of logarithms is to fiscal calculations, in which the value of moneys accumulating for long periods at compound interest is required.

Compound interest is gained by any fund on which the interest is collected at stated intervals and put out at interest.

As an example, suppose that \$10 000 is put out at 6 per cent interest, and the interest collected semi-annually and put out at the same rate. The principal will then grow as follows:

Principal at starting	
Amount at end of 6 months  Interest on this amount = 3 per cent	
Amount at end of 1 year	
Amount at end of $1\frac{1}{2}$ years	
Amount at end of 2 years	<b>\$</b> 11 255.09

Although in business practice interest is commonly payable semiannually, it is in calculations of this kind commonly supposed to be collected and re-invested only at the end of each year. This makes the computation more simple, and gives results nearer to those obtained in practice, because a company cannot generally invest its income immediately. If it had to wait three months to invest each semi-annual instalment of interest collected, the general result would be about the same as if it collected interest only once a year and invested it immediately.

If r be the rate per cent per annum, the annual rate of increase will be  $\frac{r}{100}$ . Let us put

- $\rho$ , the annual rate of increase  $=\frac{r}{100}$ ;
- p, the amount at interest at the beginning of the time, or the principal;
  - a, the amount at the end of one or more years.

 $a = p (1+\rho)^n. \tag{1}$ 

To compute by logarithms, let us take the logarithms of both members. We then have

$$\log a = \log p + n \log (1 + \rho). \tag{2}$$

Example. Find the amount of \$1250 for 30 years at 6 per cent per annum.

Here 
$$ho = .06$$
  
 $1 + 
ho = 1.06$   
 $\log (1 + 
ho) = 0.025\,306$  (end of Table L.)  
 $30$   
 $n \log (1 + 
ho), \quad 0.759\,18$   
 $\log p, \quad 3.096\,91$   
 $\log a, \quad 3.856\,09$   
 $a, \$7179.50 = \text{required amount.}$ 

#### EXERCISES.

- 1. Find the amount of \$100 for 100 years at 5 per cent compound interest.
- 2. A man bequeathed the sum of \$500 to accumulate at 4 per cent interest for 80 years after his death. After that time the annual interest was to be applied to the support of a student in Harvard College. What would be the income from the scholarship?
- 3. If the sum of one cent had been put out at 3 per cent per annum at the Christian era, and accumulated until the year 1800, what would then have been the amount, and the annual interest on this amount?

It is only requisite to give three significant figures, followed by the necessary number of zeros.

4. Solve by logarithms the problem of the horseshoeing, in which a man agrees to pay 1 cent for the first nail, 2 for the second, and so on, doubling the amount for every nail for 32 nails in all.

Note. It is only necessary to compute the amount for the 32d nail, because it is easy to see that the amount paid for each nail is 1 cent more than for all the preceding ones.

- 5. A man lays aside \$1000 as a marriage-portion for his new-born daughter, and invests it so as to accumulate at 8 per cent compound interest. The daughter is married at the age of 25. What does the portion amount to?
- 6. A man of 30 pays \$2000 in full for a \$5000 policy of insurance on his life. Dying at the age of 80, his heirs receive \$7000, policy and dividends. If the money was worth 4 per cent to him, how much have the heirs gained or lost by the investment?
- 7. What would have been the answer to the previous question, had the man died at the age of 40, and the amount paid been \$6000?

Other applications of the formulæ. By means of the equations (1) and (2) we may obtain any one of the four quantities a, p,  $\rho$ , and n when the other three are given.

CASE I. Given the principal, rate of interest, and time, to find the amount.

This case is that just solved.

CASE II. Given the amount, time, and rate per cent, to find the principal.

Solution. Equation (1) gives

$$p=\frac{a}{(1+\rho)^n}.$$

Taking the logarithms,

$$\log p = \log a - n \log (1 + \rho),$$

by which the computation may be made.

CASE III. Given the principal, amount, and time, to find the rate. Solution. Equation (2) gives

$$\log (1+\rho) = \frac{\log a - \log p}{n} = \frac{1}{n} \log \frac{a}{p}.$$

Example. A man wants a principal of \$600 to amount to \$1000 in 10 years. At what rate of interest must he invest it?

Solution. 
$$\log a = 3.000\ 00$$

$$\log p = 2.778\ 15$$

$$\log \frac{a}{p} = 0.221\ 85$$

$$\frac{1}{10} \log \frac{a}{p} = 0.022\ 185 = \log (1 + \rho).$$

Hence, from last page of logarithms,

$$1 + \rho = 1.05241;$$
  
rate = 5.241.

and

rate = 5.241

or 51 per cent, nearly.

#### EXERCISES.

- 1. At what rate of interest will money double itself every ten years?

  Ans. 7.177.
  - 2. At what rate will it treble itself every 15 years? Ans. 7.599.
- 3. A man having invested \$1000, with all the interest it yielded him, for 25 years, finds that it amounts to \$3386. What was the rate of interest?

  Ans. 5 per cent.
- 4. A life company issued to a man of 20 a paid-up policy for \$10,000, the single premium charged being \$3150. If he dies at the age of 60, at what rate must the company invest its money to make itself good?

  Ans. 2.93 per cent.
- 5. A man who can gain 4 per cent interest wants to invest such a sum that it shall amount to \$5000 when his daughter, now 5 years old, attains the age of 20. How much must he invest? Ans. \$2776.62.
- 6. How much must a man leave in order that it may amount to \$1,000,000 in 500 years at 2½ per cent interest? Ans. \$4.36½
- 7. How much if the time is 1000 years, the rate being still  $2\frac{1}{2}$  per cent, and the amount \$1,000,000? Ans. 0.0019 of a cent.
- 8. A man finds that his investment has increased fivefold in 25 years. What is the average rate of interest he has gained?

Ans. 6.65.

9. An endowment of \$7500 is payable to a man when he attains the age of 65. What is its value when he is 45, supposing the rate of interest to be 4 per cent?

Ans. \$3423.

# 13. Accumulation of an Annuity.

It is often necessary to ascertain the present or future value of a series of equal annual payments. Thus it is very common to pay a constant annual premium for a policy of life insurance. The value of such a series of payments at any epoch is found by reducing the value of each one to the epoch, allowing for interest, and taking the sum. Supposing the epoch to be the present time, the problem may be stated as follows:

A man agrees to pay p dollars a year for n years, the first payment being due in one year, and the total number of payments n. What is the present value of all n payments?

Putting, as before,  $\rho = \frac{\text{rate of interest}}{100}$ , the present value of p dollars payable after y years will, by § 12, Case II., be

$$\frac{p}{(1+\rho)^{y}}$$
.

Putting in succession, y = 1, y = 2, ... y = n, the sum of the present values is

$$\frac{p}{1+\rho} + \frac{p}{(1+\rho)^3} + \frac{p}{(1+\rho)^3} + \cdots + \frac{p}{(1+\rho)^n}.$$

This is a geometrical progression in which

First term 
$$=\frac{p}{1+\rho}$$
;  
Common ratio  $=\frac{1}{1+\rho}$ ;

Number of terms = n.

By College Algebra, § 212, the sum of this progression will be

$$\Sigma_{1} = \frac{p}{1+\rho} \cdot \frac{1 - \left(\frac{1}{1+\rho}\right)^{n}}{1 - \frac{1}{1+\rho}} = p \frac{(1+\rho)^{n} - 1}{(1+\rho)^{n+1} - (1+\rho)^{n}} \\
= \frac{p}{(1+\rho)^{n}} \cdot \frac{(1+\rho)^{n} - 1}{\rho} \cdot$$
(1)

If the first payment is to be made immediately, instead of at the end of a year, the last or nth payment will be due in n-1 years, and the progression will be

$$p + \frac{p}{1+\rho} + \frac{p}{(1+\rho)^2} + \ldots + \frac{p}{(1+\rho)^{n-1}}$$

We find the sum of the geometric progression to be

$$\Sigma_{2} = p \frac{(1+\rho)^{n} - 1}{(1+\rho)^{n} - (1+\rho)^{n-1}}$$
 (2)

#### EXERCISES.

1. What is the present value of 15 annual payments of \$85 each, of which the first is due in one year, the rate being 5 per cent?

We find by substitution

Present value = 
$$85 \frac{1.05^{15} - 1}{1.05^{15} - 1.05^{15}} = \frac{85}{1.05^{15}} \cdot \frac{1.05^{15} - 1}{.05}$$
  
=  $\frac{1700 (1.05^{15} - 1)}{(1.05)^{15}}$ .  
log 1.05, 0.021 189 1.05<sup>15</sup>, 2.078 95 1.05<sup>15</sup> - 1, 1.078 95 log 1.05<sup>15</sup>, 0.317 84 log, 0.033 00 co-log 1.05<sup>15</sup>, 9.682 16 log 1700, 3.230 45 Value, \$882.28 log value,  $\frac{2.945}{61}$ 

- 2. The same thing being supposed, what would be the present value if the rate of interest were 4 per cent?

  Ans. \$945.80
- 3. What is the present value of 25 annual payments of \$1000 each, the first due immediately, if the rate of interest is 3 per cent?

  Ans. \$17,935
- 4. A debtor owing \$10,000 wishes to pay it in 10 equal annual instalments, the first being payable immediately. If the rate of interest is 6 per cent, how much should each payment be?

Ans. \$1281.76.

NOTE. This problem is the reverse of the given one, since, in the equation (2), we have given  $\Sigma_2 = 10\,000$ ,  $\rho = 0.06$ , and n = 10, to find p.

5. The same thing being supposed, what should be the annual payment in case the payments should begin in a year?

Ans. \$1358.69.

Perpetual annuities. If the rate of interest were zero, the present value of an infinity of future payments would be infinite. But with any rate of interest, however small, it will be finite. For if, in the first equation (1), we suppose n infinite,  $\left(\frac{1}{1+\rho}\right)^n$  will converge toward zero, and we shall have

$$\Sigma = \frac{p}{(1+\rho)\left(1-\frac{1}{1+\rho}\right)} = \frac{p}{\rho}.$$
 (3)

This result admits of being put into a concise form, thus:

Since  $\Sigma$  is the present value of the perpetual annuity p, the annual interest on this value will be  $\rho\Sigma$ . But the equation (3) gives  $\rho\Sigma = p$ .

Hanca.

The present value of a perpetual annuity is the sum of which the annuity is the annual interest.

Example. If the rate of interest were 3½ per cent, the present value of a perpetual annuity of \$70 would be \$2000.

#### EXERCISES.

1. A government owing a perpetual annuity of \$1000 wishes to pay it off by 10 equal annual payments. If the rate of interest is 4 per cent, what should be the amount of each payment?

Ans. \$3082.30.

2. A government bond of \$100 is due in 15 years with interest at 6 per cent. The market rate of interest having meanwhile fallen to 3½ per cent, what should be the value of the bond?

Note. We find, separately, the present value of the 15 annual instalments of interest, and of the principal.

# TABLE IL

## MATHEMATICAL CONSTANTS.

14. In this table is given a collection of constant quantities which frequently occur in computation, with their logarithms.

The logarithms are given to more than five decimals, in order to be useful when greater accuracy is required. When used in five-place computations, the figures following the fifth decimal are to be dropped, and the fifth decimal is to be increased by unity in case the figure next following is 5 or any greater one.

## TABLES III. AND IV.

## LOGARITHMS OF TRIGONOMETRIC FUNCTIONS.

15. By means of these tables the logarithms of the six trigonometric functions of any angle may be found.

The logarithm of the function instead of the function itself is given, because the latter is nearly always used as a factor.

We begin by explaining Table IV., because Table III. is used only in some special cases where Table IV. is not convenient.

I. Angles less than 45°. If the angle of which a function is sought is less than 45°, we seek the number of degrees at the top of the table and the minutes in the left-hand column. Then in the line opposite these minutes we find successively the sine, the tangent, the cotangent, and the cosine of the angle, as given at the heading of the page.

Example.  $\log \sin 31^{\circ} 27' = 9.71747;$   $\log \tan 31^{\circ} 27' = 9.78647;$   $\log \cot 31^{\circ} 27' = 0.21353;$ 

 $\cos 31^{\circ} 27' = 9.931 00.$ 

The sine, tangent, and cosine of this angle being all less than unity, the true mantissæ of the logarithm are negative; they are therefore increased by 10, on the system already explained.

If the secant or cosecant of an angle is required, it can be found by taking the arithmetical complement of the cosine or sine. It is shown in trigonometry that

$$secant = \frac{1}{cosine},$$

and

$$cosecant = \frac{1}{sine}.$$

Therefore  $\log \operatorname{secant} = 0 - \log \operatorname{cosine} = \operatorname{co-log cosine};$   $\log \operatorname{cosec} = 0 - \log \operatorname{sine} = \operatorname{co-log sine}.$ 

We thus find  $\log \sec 31^{\circ} 27' = 0.069 00;$ 

 $\log \csc 31^{\circ} 27' = 0.28253.$ 

After each column, upon intermediate lines, is given the differ-

ence between every two consecutive logarithms, in order to facilitate interpolation.

In the case of tangent and cotangent, only one column of differences is necessary for both functions.

If we use no fractional parts of minutes, no interpolation is necessary; but if decimals of a minute are employed, we can interpolate precisely as in taking out the logarithms of numbers.

Where the differences are very small they are sometimes omitted.

Tables of proportional parts are given in the margin, the use of which is similar to those given with the logarithms of numbers.

Example 1. To find the log sin of 31° 27'.7.

We have from the tables,  $\log \sin 31^{\circ} 27' = 9.71747$ Under diff. 20, P.P. for 7,

 $\log \sin 31^{\circ} 27'.7 = 9.71761$ 

Ex. 2. To find log cot 15° 44'.34.

The tables give  $\log \cot 15^{\circ} 44' = 0.550 19$ Under diff. 48, opposite 0.3, P.P., -14.4"  $0.4 \div 10$ , -1.9

log cot 15° 44'.34, 0.55003

Since the tabular quantity diminishes as the angle increases, the proportional parts are subtractive.

#### EXERCISES.

Find from the tables:

- 1. log cot 43° 29'.3;
- 2. log tan 43° 29'.3;
- 3. log cos 27° 10′.6;
- 4. log sin 27° 10′.6;
- 5. log tan 12° 9'.43;
- 6. log cot 12° 9'.43.

In the case of sines and tangents of small angles the differences vary so rapidly that in most cases the exact difference will not be found in the table of proportional parts. In this case, if the proportional parts are made use of, a double interpolation will generally be necessary to find the fraction of a minute corresponding to a given sine or tangent. If only tenths of minutes are used, an expert computer will find it as easy to multiply or divide mentally as to refer to the table.

II. Angles between 45° and 90°. It is shown in trigonometry that if we compute the values of the trigonometric functions for the

first 45°, we have those for the whole circle by properly exchanging them in the different parts of the circle. First, if we have

$$\alpha + \beta = 90,$$

then  $\alpha$  and  $\beta$  are complementary functions, and

$$\sin \beta = \cos \alpha;$$
  
 $\tan \beta = \cot \alpha.$ 

Therefore if our angle is between 45° and 90°, we may find its complement. Entering the table with this complement, the complementary function will then be the required function of the angle.

Example. To find the sine of  $67^{\circ}$  23', we may enter the table with  $22^{\circ}$  37' (=  $90^{\circ}$  -  $67^{\circ}$  23') and take out the cosine of  $22^{\circ}$  37', which is the required sine of  $67^{\circ}$  23.

To save the trouble of doing this, the complementary angles and the complementary denominations of the functions are given at the bottom of the page.

The minutes corresponding to the degrees at the bottom are given on the right hand. Therefore:

To find the trigonometric functions corresponding to an angle between 45° and '90°, we take the degrees at the bottom of the page and the minutes in the right-hand column. The values of the four functions log sine, log tangent, log cotangent, and log cosine, as read at the bottom of the page, are then found in the same line as the minutes.

Example 1. For 52° 59' we find

log sin = 
$$9.90225$$
;  
log tan =  $0.12262$ ;  
log cot =  $9.87738$ ;  
log cos =  $9.77963$ .

Ex. 2. To find the trigonometric functions of 77° 17'.28.

#### EXERCISES.

Find the logarithms of the six functions of the following angles:

III. When the angle exceeds 90°.

Rule. Subtract from the angle the greatest multiple of 90° which it contains.

If this multiple is 180°, enter the table with the excess of the angle over 180° and take out the functions required, as if this excess were itself the angle.

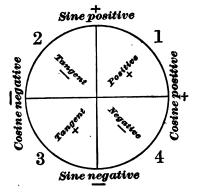
If the multiple is 90° or 270°, take out the complementary function to that required.

By then assigning the proper algebraic sign, as shown in trigonometry, the complete values of the function will be obtained.

The computer should be able to assign the proper algebraic sign according to the quadrant, without burdening his memory with

the special rules necessary in each case. This he can do by carrying in his mind's eye the following scheme. He should have at command the arrangement of the four quadrants as usually represented in trigonometry, so as to know, when an angle is stated, where it will fall relatively to the horizontal and vertical lines through the centre of the circle. Then, in the case of—

Sine or cosecant. If the angle is above the horizontal line (which



it is between 0° and 180°), the sine is positive; if below, negative.

Cosine or secant. If the angle is to the right of the vertical central line (as it is in the first and fourth quadrants), the cosine and secant are positive; if to the left (as in the second and third quadrants), negative.

Tangent or cotangent. Through the opposite first and third quadrants, positive; through the opposite second and fourth quadrants, negative.

Example 1. To find the tangent and cosine of 122° 44'. Subtracting 90°, we enter the table with 32° 44' and find

log cot 
$$32^{\circ} 44' = 0.19192$$
;  
log sin  $32^{\circ} 44' = 9.73298$ .

Therefore, writing the algebraic sign before the logarithm, we have

$$\log \tan 122^{\circ} 44' = -0.19192;$$
  
 $\log \cos 122^{\circ} 44' = -9.73298.$ 

Ex. 2. To find the sine and cotangent of 322° 58'.

Entering the table with  $52^{\circ} 58' = 322^{\circ} 58' - 270^{\circ}$ , and taking out the complementary functions, we find

```
\log \sin 322^{\circ} 58' = -9.779 80;
\log \cot 322^{\circ} 58' = -0.122 36.
```

Ex. 3. To find the sine and tangent of 253° 5'.

Entering with 73° 5', we take out the sine and tangent, finding

$$\log \sin 253^{\circ} 5' = -9.89079;$$
  
 $\log \tan 253^{\circ} 5' = +0.51693.$ 

Ex. 4. To find the six trigonometric functions of 152° 38'. We have

```
log sin 152° 38' = log cos 62° 38' pos. = + 9.662 46;
log cos 152° 38' = log sin 62° 38' neg. = - 9.948 45;
log tan 152° 38' = log cot 62° 38' neg. = - 9.714 01;
log cot 152° 38' = log tan 62° 38' neg. = - 0.285 99;
log sec = co-log cos = - 0.051 55;
log cosec = co-log sin = + 0.337 54.
```

#### EXERCISES.

Find the six trigonometric functions of the following angles:

```
276° 29′.3;
66° 0′.5;
96° 59′.8;
252° 20′.3;
318° 10′.7;
— 25° 22′.2;
—155° 30′.7.
```

# 16. Method of Writing the Algebraic Signs.

As logarithms are used in computation, they may always be considered positive. It is true that the logarithms of numbers less than unity are in reality negative, but, for convenience in calculation, we increase them by 10, so as to make them positive.

The number corresponding to a given logarithm may, in computation, be positive or negative. There are two ways of distinguishing the algebraic sign of the number, between which the computer may choose for himself.

I. Write the algebraic sign of the number before the logarithm. As usually interpreted, the algebraic sign written thus would apply to the logarithm, which it does not. It is therefore necessary for the

computer to bear in mind that the sign belongs, not to the logarithm, as written, but to the number.

II. Write the letter n after the logarithm when the number is negative. This plan is theoretically the best, but, should the computer accidentally omit the letter, the number will be treated as positive, and a mistake will be made. It therefore requires vigilance on his part. An improvement would be to write a letter not likely to be mistaken for n, s for instance, after all positive logarithms.

# 17. To Find the Angle Corresponding to a Given Trigonometric Function.

Disregarding algebraic signs, there will always be four angles corresponding to each function, one in each quadrant. These angles will be:

The smallest angle, as found in the table;

This angle increased by 180°;

The complementary angle increased by 90°;

The complementary angle increased by 270°.

For instance, for the angle of which log tan is 0.611 92, we find 76° 16'. But we should get this same tangent for 103° 44', 256° 16', and 283° 44'.

Of the four functions corresponding to the four angles, two will always be positive and two negative; so that, in reality, there will only be two angles corresponding to a function of which both the sign and the absolute value are given. These values are found by selecting from the four possible ones the two for which the functions have the given algebraic sign. After selecting them, they may be checked by the following theorems, which are easily deduced from the relations between the values of each function as given in trigonometry:

The sum of the two angles corresponding to the same sine is  $180^{\circ}$  or  $540^{\circ}$ .

The sum of the two angles corresponding to the same cosine is  $360^{\circ}$ .

The difference of the two angles corresponding to the same tangent is 180°.

Which of the two possible angles is to be chosen depends upon the conditions of the problem or the nature of the figure to which the angle belongs. If neither the conditions nor the figure decide the question, the problem is essentially ambiguous, and either or both angles are to be taken.

#### EXERCISES.

Find the pairs of values of the angle  $\alpha$  from the following value: of the trigonometric functions:

```
1. \log \sin \alpha = +9.90243;
                                     12. \log \sec \alpha = +0.22106;
2. \log \sin \alpha = -9.90243;
                                     13. \log \sec \alpha = -0.22106;
                                     14. \log \sec \alpha = -0.09920;
3. \log \cos \alpha = +9.90243;
                                     15. \log \sec \alpha = +0.123.46;
4. \log \cos \alpha = -9.90243;
                                     16. \log \sin \alpha = +8.9903;
5. \log \tan \alpha = +0.14316;
                                     17. \log \sin \alpha = -8.99030;
6. \log \tan \alpha = -0.14316;
                                     18. \log \cos \alpha = +9.21867;
 7. \log \cot \alpha = +0.14316;
                                     19. \log \cos \alpha = -9.21867;
8. \log \cot \alpha = -0.14316;
                                     20. \log \tan \alpha = -9.13690;
 9. \log \tan \alpha = -9.02481;
10. \log \tan \alpha = -0.97519;
                                     21. \log \tan \alpha = +9.13690;
11. \log \tan \alpha = +0.97519;
                                     22. \log \cot \alpha = +9.13690.
```

# 18. Cases when the Function is very Small or Great.

When the angle of which we are to find the functions approaches to zero, the logarithms of the sine, tangent, and cotangent vary so rapidly that their values to five figures cannot be readily interpolated. The same remark applies to the cosine, cotangent, and tangent of angles near 90° or 270°. The mode of proceeding in these cases will depend upon circumstances.

In the use of five-place logarithms, there is little advantage in carrying the computations beyond tenths of minutes, though the hundredths may be found when the tangent or cotangent is given. Where greater accuracy than this is required, six- or seven-place tables must be used.

If the angles are only carried to tenths of minutes, there is no necessity for taking out the sine, tangent, or cotangent to more than four decimals when the angle is less than 3°, and three decimals suffice for angles less than 30′. The reason is that this number of decimals then suffice to distinguish each tenth of minute.

When the decimals are thus curtailed, an expert computer will be able to perform the multiplication and division for the tenths of minutes mentally. If, however, this is inconvenient, the following rule may be applied.

To find the log sine or log tangent of an angle less than 2° to four places of decimals:

Rule. Enter the table of logarithms of numbers with the value

of the angle expressed in minutes and tenths, and take out the logarithm.

To this logarithm add the quantity 6.4637.

The sum will be the log sine, and the log tangent may be assumed to have the same value.

Example 1. To find log sin 1° 22'.6.

This rule is founded on the theorem that the sines and tangents of very small arcs may be regarded as equal to the arcs themselves. Since, in using the trigonometric functions, the radius of the circle is taken as unity, an arc must be expressed in terms of the unit radius when it is to be used in place of its sine or tangent. Now, it is shown in trigonometry that the unit radius is equal to 57°.2958 or 3437'.747 or 206 264'.8. Hence we must divide the number of angular units in the angle by the corresponding one of these coefficients to obtain the length of the corresponding arcs in unit radius. Now,

$$\log 3437.747 = 3.5363$$
  
 $\operatorname{co-log......} 6.4637$ 

which may be added instead of subtracting the logarithm.

To find the cosine of an angle very near 90°, we find the sine of its complement, which will then be a very small angle, positive or negative.

## Exercises.

Find to four places of decimals:

- 1. log sin 22'.73;
- 2. log sin 1° 1'.12;
- 3. log cos 90° 0'.78;
- 4. log tan 88° 59'.35;
- 5. log cot 90° 28′.76;
- 6. log cos 89° 22'.23;
- 7.  $\log \sin 0^{\circ} 0'.25$ .

If an angle corresponding to a given sine or tangent is required, the rule is:

From the given log sine or tangent subtract 6.4637 or add 3.5363. The result is the logarithm of the number of minutes.

Of course this rule applies only to angles less than 2°, in the value of which only tenths of minutes are required.

#### EXERCISES.

Find  $\alpha$  from:

1.  $\log \sin \alpha = 7.2243$ ; 3.  $\log \tan \alpha = -2.8816$ ;

2.  $\log \cot \alpha = 2.8816$ ; 4.  $\log \cos \alpha = 6.9218$ .

When the small angle is given in seconds. Although the computer may take out his angles to tenths of minutes, cases often arise in which a small angle is given in seconds, or degrees, minutes, and seconds, and in which the trigonometric function is required to five decimals. In this case the preceding method may not always give accurate results, because the arc and its sine or tangent may differ by a greater amount than the error we can admit in the computation.

Table III. is framed to meet this case. The following are the quantities given:

In the second column: The argument, in degrees and minutes, as already explained for Table IV.

In the first column: This argument reduced to seconds. From this column the number of seconds in an arc of less than 2°, given in degrees, minutes, and seconds, may be found at sight.

Example. How many seconds in 1° 28′ 39″? In the table, before 1° 28′, we find 5280″, which being increased by 39″ gives 5319″, the number required.

- Col. 3. The logarithm of the sine of the angle. This is the same as in Table IV.
- Col. 4. The value of log sine minus log arc; that is, the difference between the logarithm of the sine and the logarithm of the number of seconds in the angle.
  - Col. 5. The same quantity for the tangent.
- Cols. 6 and 7. The complements of the preceding logarithms, distinguished by accents.

The use of the tables is as follows.

To find the sine or tangent of an angle less than 2°:

Express the angle in seconds by the first two columns of the table.

Write down the logarithm in column S or column T, according as the sine or a tangent is required.

Find from Table I. the logarithm of the number of seconds.

Adding this logarithm to S or T, the sum will be the log sine or log tangent.

Example. Find log sin 1° 2' 47".9.

S. 4.685 55

 $1^{\circ} 2' 47''.9 = 3767''.9; \log, 3.576 10$ 

log sin 1° 2′ 47″.9, 8.261 65

To find the arc corresponding to a given sine or tangent:

Find in the column L. sin. the quantity next greater or next smaller than the given logarithm.

Take the corresponding value of S' or T' according as the given function is a sine or tangent, and add it to the given function.

The sum is the logarithm of the number of seconds in the required angle.

Example. Given log tan x = 8.40125, to find x. log tan x, 8.40125

T', 5.314 33

 $\log x$ , 3.715 58

 $x = 5194''.9 = 1^{\circ} 26' 34''.9$ , from col. 2.

#### EXERCISES.

Find:

- 1. log sin 0° 20′ 20″.25;
- 2. log tan 0° 0′ 1″.2273;
- 3. log sin 1° 59′ 22″.7;
- 4. log tan 1° 0′ 59″.7.

Find x from:

- 1.  $\log \tan x = 8.42796$ ;
- 2.  $\log \tan x = 7.42796$ ;
- 3.  $\log \tan x = 6.42796$ ;
- 4.  $\log \sin x = 5.35435$ ;
- 5.  $\log \sin x = 4.22619$ ;
- 6.  $\log \sin x = 8.54078$ .

When the cosine or cotangent of an angle near 90° or 270° is required, we take its difference from 90° or 270°, and find the complementary function by the above rules.

Remark. The use of the logarithms of the trigonometric functions is so much more extensive than that of the functions themselves that the prefix "log" is generally omitted before the designation of the logarithmic function, where no ambiguity will result from the omission.

## TABLE V.

## NATURAL SINES AND COSINES.

19. This table gives the actual numerical values of the sine and cosine for each minute of the quadrant.

To find the sine or cosine corresponding to a given angle less than 45°, we find the degrees at the top of a pair of columns and the minutes on the left.

In the two columns under the degrees and in the line of minutes we find first the sine and then the cosine, as shown at the head of the column.

A decimal point precedes the first printed figure in all cases, except where the printed value of the function is unity.

If the given angle is between 45° and 90°, find the degrees at the bottom and the minutes at the right.

Of the two numbers above the degrees, the right-hand one is the sine and the left-hand one the cosine.

For angles greater than 90° the functions are to be found according to the precepts given in the case of the logarithms of the sines and tangents.

## TABLE VI.

### ADDITION AND SUBTRACTION LOGARITHMS.

20. Addition and subtraction logarithms are used to solve the problem: Having given the logarithms of two numbers, to find the logarithm of the sum or difference of the numbers.

The problem can of course be solved by finding the numbers corresponding to the logarithms, adding or subtracting them, and taking out the logarithm of their sum or difference. The table under consideration enables the result to be obtained by an abbreviated process.

I. Use in addition. The principle on which the table is constructed may be seen by the following reasonings. Let us put

$$S = a + b$$

a and b being two numbers of which the logarithms are given. We shall have

$$S = a\left(1 + \frac{b}{a}\right) = a\left(1 + x\right);$$

putting, for clearness,  $x = \frac{b}{a}$ .

We then have

$$\log S = \log a + \log (1 + x).$$

Since  $\log a$  and  $\log b$  are both given, we can find  $\log x$  from the equation

$$\log x = \log b - \log a,$$

which is therefore a known quantity.

Now, for every value of  $\log x$  there will be one definite value of each of the quantities x, 1+x, and  $\log (1+x)$ . Therefore a table may be constructed showing, for every value of  $\log x$ , the corresponding value of  $\log (1+x)$ .

Such a table is Table VI.

The argument, in column A, being log x, the quantity B in the table is log (1+x).

Example.  $\log 0.25 = 9.39794$ .

Entering the table with A = 9.39794, we find

B = 0.09691,

which is the logarithm of 1.25.

Therefore, entering the table with  $\log x$  as the argument, we take out  $\log (1+x)$ , which added to  $\log a$  will give  $\log S$ .

We have therefore the following precept for using the table in addition:

Take the difference of the two given logarithms.

Enter the table with this difference as the argument A, and take out the quantity B.

Adding B to the subtracted logarithm, the sum will be the required logarithm of the sum.

It is indifferent which logarithm is subtracted, but convenience in interpolating will be gained by subtracting the greater logarithm from the lesser increased by 10. The number B will then be added to the greater logarithm.

Example. Given  $\log m = 1.62974$ ,  $\log n = 2.20386$ ; find  $\log (m+n)$ .

The required logarithm is found in either of the following two ways:

The figures in parentheses show the order in which the numbers are written.

#### EXERCISES.

Log a and log b having the following values, find log (a + b).

- 1.  $\log a = 1.70037$ ;  $\log b = 0.92169$ .
- 2.  $\log a = 0.62460$ ;  $\log b = 9.88126$ .
- 3.  $\log a = 9.79186$ ;  $\log b = 9.32209$ .
- 4.  $\log a = 1.60162$ ;  $\log b = 1.30606$ .
- 5.  $\log a = 0.79290$ ;  $\log b = 9.22127$ .
- 6.  $\log a = 0.60132$ ;  $\log b = 9.00168$ .
- 7.  $\log a = 4.79643$ ;  $\log b = 3.98186$ .

II. Use in subtraction. The problem is, having given  $\log a$  and  $\log b$ , to find the logarithm of

We have 
$$D = a - b.$$

$$D = b \left(\frac{a}{b} - 1\right);$$
whence 
$$\log D = \log b + \log \left(\frac{a}{b} - 1\right).$$

Since  $\log \frac{a}{b}$  is found by subtracting  $\log b$  from  $\log a$ , if we can

find  $\log \left(\frac{a}{b}-1\right)$  from  $\log \frac{a}{b}$ , the problem will be solved.

From the construction of the table already explained, if we have

$$B=\log\frac{a}{b},$$

we must have

$$A = \log \left(\frac{a}{b} - 1\right).$$

We now have the following precept for subtraction:

Subtract the lesser of the given logarithms from the greater.

Enter the table so as to find the difference of the logarithms in the numbers B of the table.

Add the corresponding value of A to the lesser of the given logarithms. The sum will be the logarithm of the difference.

Example. Find  $\log (n-m)$  in the example of the preceding section.

$$\log n$$
, 2.203 86 (1)

$$\log m$$
, 1.629 74 (2)  
A, 0.439 45 (4)

$$\log \frac{n}{m} = B, \ 0.574 \ 12 \quad (3)$$

$$\log (n-m), \overline{2.06919}$$
 (5)

#### EXERCISES.

Find the logarithms of the differences of the quantities a and b in the preceding section.

Remark. In the use of addition and subtraction logarithms, the precepts apply to numerical sums and differences, without respect to the algebraic signs of the quantities. For example, the algebraic difference between + 1473 and - 29 462 is to be found by addition, and the algebraic sum of a positive and negative quantity by subtraction.

Case where the quotient is large. Near the end of the table, A and B become nearly equal; the structure of the table is therefore changed so as to simplify its use. It is evident that if b is very small compared with a, the logarithms of a + b and a - b will not differ much from the logarithm of a itself. Hence, in this case, we shall have smaller numbers to use if we can find the quantity which must be added to  $\log a$  to give  $\log (a + b)$ , or subtracted from

log a to give log (a - b). Now, the equations already written give, when a > b,  $\log a = \log b + A$ ,

$$\log (a+b) = \log b + B;$$

whence, by subtraction,

$$\log (a+b) - \log a = B - A,$$

or

$$\log (a + b) = \log a + B - A$$
. (with Arg. A)

We find in the same way,

$$\log (a - b) = \log a - (B - A). \text{ (with Arg. B)}$$

Now, whenever  $\log a - \log b$  is greater than 1.65, we shall find it more convenient to take out B - A from the table than either A or B. We notice that the last two figures of B in this part of the table vary slowly, and we need only attend to them in interpolating. For instance, in the horizontal line corresponding to A = 1.66 we find:

for 
$$A = 1.660\ 00$$
;  $B = 1.669\ 40$ ;  $B - A = .009\ 40$ ; .661\ 00; .670\ 38; .009\ 38; .662\ 00; .671\ 36; .009\ 36; .663\ 00; .672\ 33; .009\ 33; .664\ 00; .673\ 31; .009\ 31; .665\ 00; .674\ 29; .009\ 29; etc. etc. etc.

The interpolation of B-A is now very easy whether the quantity given is A or B. We note that B-A has but three significant figures, of which the first is found in column zero, and the other two are the last two figures of B as printed.

As an example, let us find  $\log (a + b)$  from

$$\log a = 2.79163$$

$$\log b = 1.12819$$

$$A = 1.66344$$

Entering the table with this value of A, we find by column 0 that B - A falls between .009 40 and .009 19. Following the horizontal line A = 1.66 to column 3 and interpolating the last two figures between 33 and 31 for .44, with the difference -2, we find

$$B-A=.00932$$

Then

$$\log a = 2.79163$$

$$\log{(a+b)} = 2.80095$$

Next, if  $\log (a - b)$  is required, we have to find the difference 1.663 44 in the part B of the table. We find in the table:

for 
$$B = 1.66255$$
;  $B - A = .00955$ ; for  $B = 1.66353$ ;  $B - A = .00953$ .

Therefore

for 
$$B = 1.66344$$
;  $B - A = .00953$ .

Subtracting this from log a, we have

$$\log (a - b) = 2.78210.$$

#### EXERCISES.

Find  $\log (a + b)$  and  $\log (a - b)$  from:

8. 
$$\log a = 0.36702$$
;  $\log b = 8.46283$ .

9. 
$$\log a = 0.00126$$
;  $\log b = 8.32907$ .

10. 
$$\log a = 2.06923$$
;  $\log b = 0.11085$ .

11. 
$$\log a = 5.80735$$
;  $\log b = 3.83809$ .

For values of A and B greater than 2.00, the table is so arranged that no interpolation at all is necessary. The computer has only to find what value of A or B given in the table comes nearest his value of  $\log a - \log b$  and take the corresponding value of B - A. He must remember that column A is to be entered for addition, and B for subtraction.

In this part of the table A and B are given to fewer than five decimals; because five decimals are not necessary to give B-A with accuracy. The nearer the end of the table is approached, the fewer the decimals necessary in taking the difference.

Example. Find  $\log (a + b)$  and  $\log (a - b)$  from

$$\log a = 1.26532$$

$$\log b = 9.22230$$

$$\log a - \log b$$
, 2.043 02

Entering column A with this difference, we find the nearest tabular value of A to be 2.0425, to which corresponds B - A = .00392. Hence

$$\log(a+b) = 1.26532 + .00392 = 1.26924.$$

Entering column B with the same difference, we find B - A = .00395; whence

$$\log (a-b) = 1.26532 - .00395 = 1.26137.$$

#### EXERCISES.

Find  $\log (a + b)$  and  $\log (a - b)$  from:

- 1.  $\log a = 4.06905$ ;  $\log b = 2.00132$ .
- 2.  $\log a = 3.92693$ ;  $\log b = 1.20159$ .
- 3.  $\log a = 3.06164$ ;  $\log b = 0.12615$ .
- 4.  $\log a = 1.220$  68;  $\log b = 7.321$  56.
- 5.  $\log a = 0.69317$ ;  $\log b = 6.01023$ .
- 6.  $\log a = 2.30620$ ;  $\log b = 7.02301$ .

Case of nearly equal numbers. Near the beginning of the table the reverse is true: it is not possible to find A with accuracy to five places of decimals. But here the value of A taken from the tables, though it be found to only two, three, or four places of decimals, will give as accurate a result as the computation of a and b to five places will admit of. Let us suppose, for example, that we have to find  $\log (a - b)$  from

$$\log a = 9.883 \, 15$$

$$\log b = 9.882 \, 96$$

$$B = 0.000 \, 19$$

$$A = 6.64 - 10;$$
whence 
$$\log (a - b) = 6.52 - 10.$$

We note that the value of A may be 6.63 or 6.65 as well as 6.64, so that the result cannot be carried beyond two decimals. To show that these two are as accurate as the work admits of, we find the natural numbers a and b from Table I.

$$a = 0.764 10$$

$$b = 0.763 77$$

$$a - b = 0.000 33$$

Since a-b has but two significant figures, and the first of these is less than 5, two figures in the logarithm are all that can be accurate.

## TABLE VII.

# SQUARES OF NUMBERS.

21. By means of this table the square of any number less than 1000 may be found at sight, and that of any number less than 10000 by a simple and easy interpolation.

The first page gives the squares of the first 100 numbers, which it is often convenient to have by themselves.

On the second and third pages (98 and 99) the hundreds of the number to be squared are found at the tops of the several columns, and the tens and units in the left-hand column. The first three or four figures of the square are in the column under the hundreds, and opposite the tens and units, and the last two figures on the right of the page after the column 9  $\spadesuit$ 

```
Examples. The square of 634 is 401 956;

" 329 " 108 241;

" 265 " 70 225;

" 153 " 23 409;

" 999 " 998 001.
```

The same table may be used for any number of three significant figures by attention to the position of the decimal-point. Thus:

$$51100^{2} = 2611210000;$$

$$511^{2} = 261121;$$

$$51.1^{2} = 2611.21;$$

$$5.11^{3} = 26.1121;$$

$$0.511^{2} = 0.261121.$$

When there are four significant figures, an interpolation may be executed in several ways. If n be the nearest number the square of which is found in the table, and h the excess of the given number over this, so that n + h is the number whose square is required, we shall have

$$(n+h)^{2} = n^{2} + 2nh + h^{2} = n^{2} + h(2n+h)$$
  
=  $n^{2} + h(N+n)$ ;

where N = n + h, the given number.

We may therefore find the square of 257.4 in the following way:

$$257^{\circ} = 66\,049$$

$$514.4 \times .4 = 205.76$$

$$(257.4)^{\circ} = 66\,254.76$$

To find the square of 9037 we proceed thus:

$$\begin{array}{ccc}
9037 \\
9030^{\circ} & = 81\,540\,900 \\
\hline
18067 \times 7 & = 126\,469 \\
9037^{\circ} & = 81\,667\,369
\end{array}$$

In many cases only one more figure will be required in the square than in the given number. The square can then be interpolated with all required accuracy by the differences, the last two figures of which are found in the last column of the table, while the remaining figures are found by taking the difference between two consecutive numbers in the principal column.

To return to the last example, we find the difference between 257° and 258° to be 515, the first figure being the difference between 660 and 665, and the last two, 15, in the last column. Then

$$257^{2} = 66 049$$

$$515 \times 0.4 = 206$$

$$(257.4)^{2} = 66 255$$

-which is correct to the nearest unit.

It will be remarked that the two methods are substantially the same when only five figures are sought in the result. The substantial identity rests upon the general theorem that

The difference of the squares of two consecutive numbers is equal to the sum of the numbers.

We prove this theorem thus:

$$(n+1)^2 - n^2 = 2n + 1 = n + (n+1).$$

When the tabular difference is taken in the way already described, it will often happen that the difference between the numbers in the columns of hundreds is to be diminished by unity. Thus, although 4173-4160=13, the difference between  $645^{\circ}$  and  $646^{\circ}$  is not 1391, but 1291. These cases are noted by the asterisk after the number in the last column.

The squares of numbers of more than four figures may be found in the same way, but in such cases it will generally be easier to use logarithms than the table of squares.

## TABLE VIII.

# TO CONVERT HOURS, MINUTES, AND SECONDS INTO DECIMALS OF A DAY, AND VICE VERSA.

22. The familiar method of solving this problem is to convert the seconds into decimals of a minute, and the minutes into decimals of an hour, by dividing by 60, and then the hours into decimals of a day by dividing by 24. The reverse problem is solved by multiplying by 24, 60, and 60.

Table VIII. enables us to perform these operations without division. Column D gives each hundredth of a day, but its numbers may also be regarded as ten thousandths or millionths of a day, according to which of the following three columns is used. In column H.M.S. are found the hours, minutes, and seconds corresponding to these hundredths. In the next column is one hundredth of column H.M.S., or the minutes and seconds in the number of ten thousandths of a day in column D. Finally, column  $\frac{H.M.S.}{100^3}$  shows the number of seconds in the number of millionths of a day found in column D.

Example. To convert 0d.532 946 into hours, minutes, and seconds.

It will be seen that we divide the figures of the given decimal of a day into pairs, and enter the three columns of time with these three pairs in succession.

If seven decimals are given, we may interpolate the last number, as in taking out a logarithm.

In practice the computer will perform the interpolation mentally, adding  $.7 \times .08 = .06$  to the number 5.36 of the table in his head, and writing down 5.42 as the last quantity to be added.

#### EXERCISES.

Convert into hours, minutes, and seconds:

Hence

be 302.

- 1. 0d.203 079 2;
- 2. 0d.783 605 8;
- 3. 0d.010 203 4;
- 4. 0d.990 990 9.

To use the table for the reverse operation, we proceed as in the following example:

It is required to convert 17<sup>h</sup> 29<sup>m</sup> 30<sup>s</sup>.93 into decimals of a day. Looking in the table, we find that the required decimal is between 0.72 and 0.73. Hence the first two figures are 0.72, the equivalent of 17<sup>h</sup> 16<sup>m</sup> 48<sup>s</sup>. Subtracting the lat-17h 29m 30s,93 ter from the given number, we 0.72  $=17^{h} 16^{m} 48^{s}$ have a remainder 12<sup>m</sup> 42<sup>s</sup>.93, to be 12m 42s,93 .0088 12<sup>m</sup> 40<sup>s</sup>.32 sought for in column  $\frac{H.M.S.}{100}$ . This .0000302 =gives 88 as the next two figures. Subtracting the equivalent of .0088 or 12<sup>m</sup> 40°.32, we have left 2°.61, which we are to seek in column  $\frac{H.M.S.}{100^3}$ . We find the corresponding number of column D to

 $17^{h} 29^{m} 30^{s}.93 = 0^{d}.7288302.$ 

In solving this problem the computer should be able, after a little practice, to perform the subtractions and carry the remainders mentally, thus saving himself the trouble of writing down the numbers.

#### Exercises.

Take the answers obtained from the four preceding exercises, subtract each result from 24<sup>h</sup> 0<sup>m</sup> 0<sup>s</sup>, change the remainder to decimals of a day, and see if when added to the decimals of the preceding exercises the sum is 1<sup>d</sup>.000 000 0, as it should be.

## TABLE IX.

## TO CONVERT TIME INTO ARC, AND VICE VERSA.

23. In astronomy the right ascensions of the heavenly bodies are commonly given in hours, minutes, and seconds, the circumference being divided into 24 hours, each hour into 60 minutes, and each minute into 60 seconds.

Since  $360^{\circ} = \text{one circumference},$  we have  $1^{h} = 15^{\circ};$   $1^{m} = 15';$   $1^{s} = 15';$ 

the signs h, m, and s indicating hours, minutes, and seconds of time.

Hence we may change time into arc by multiplying by 15, and arc into time by dividing by 15, the denominations being changed in each case. Table IX. enables us to do this by simple addition and subtraction by a process similar to that employed in changing hours, minutes, and seconds into decimals of a day.

To turn time into arc, we find in the table the whole number of degrees contained in the time denomination next smaller than the given one, and subtract the former time denomination from the latter.

Next we find the minutes of arc corresponding to the given time next smaller than the remainder, and again subtract.

Lastly we interpolate the seconds corresponding to the second remainder.

Example. Change 15<sup>h</sup> 29<sup>m</sup> 46<sup>s</sup>.24 to arc.

Given time, 15<sup>h</sup> 29<sup>m</sup> 46<sup>s</sup>.24

The table gives 232° =  $15^h$  28<sup>m</sup>

Remainder,  $1^m$  46<sup>s</sup>.24

The table gives 26' =  $1^m$  44<sup>s</sup>

Remainder,  $2^s$ .24 = 33'.6

Hence

 $15^{h} 29^{m} 46^{s}.24 = 232^{\circ} 26' 33'.6.$ 

The computer should be able to go through this operation without writing down anything but the result.

The operation of changing arc into time is too simple to require description, but it is more necessary to write down the work.

### EXERCISES.

Change the following times to arc, and then check the results by changing the arcs into time and seeing whether the original times are reproduced:

- 1. 7<sup>h</sup> 29<sup>m</sup> 17<sup>s</sup>.86;
- 2. 0h 4m 0s.25;
- 3. 12h 4m 0s.25;
- 4. 13h 48m 16s.40;
- 5. 19h 7m 59s.92.

## TABLE X.

# TO CONVERT MEAN TIME INTO SIDEREAL TIME, AND SIDEREAL INTO MEAN TIME.

24. Since 365½ solar days = 366½ sidereal days (very nearly), any period expressed in mean time may be changed to sidereal time by increasing it by its  $\frac{1}{365.25}$  part, and an interval of sidereal time may be changed to mean time by diminishing it by its  $\frac{1}{366.25}$  part.

The first part of the table gives, for each 10 minutes of the argument, its  $\frac{1}{365.25}$  part, by which it is to be increased. The second part of the table gives the  $\frac{1}{366.25}$  part of the argument.

The small table in the margin shows the change for periods of less than 10 minutes.

Example 1. To change 17<sup>h</sup> 48<sup>m</sup> 36<sup>s</sup>.7 of mean time to sidereal time.

Ex. 2. To change this interval of sidereal time back to mean time.

#### EXERCISES.

Change to sidereal time:

- 1. 3<sup>h</sup> 42<sup>m</sup> 36<sup>s</sup>.5 m. t.; 3. 22<sup>h</sup> 3<sup>m</sup> 5<sup>s</sup>.61 m. t. 2. 18<sup>h</sup> 46<sup>m</sup> 29<sup>s</sup>.82 " 4. 0<sup>h</sup> 1<sup>m</sup> 12<sup>s</sup>.55 "
- Change to mean time:
  - 5. 0h 7m 16s.3 sidereal time;
  - 6. 22<sup>h</sup> 17<sup>m</sup> 29<sup>s</sup>.65

# OF DIFFERENCES AND INTERPOLATION.\*

# 25. General Principles.

We call to mind that the object of a mathematical table is to enable one to find the value of a function corresponding to any value whatever of the variable argument. Since it is impossible to tabulate the function for all values of the argument, we have to construct the table for certain special values only, which values are generally equidistant. For example, in the tables of sines and cosines in the present work the values of the functions are given for values of the argument differing from each other by one minute.

The process of finding the values of functions corresponding to values of the argument intermediate between those given is called *interpolation*.

We have already had numerous examples of interpolation in its most simple form; we have now to consider the subject in a more general and extended way.

In the first place, we remark that, in strictness, no process of interpolation can be applicable to all cases whatever. From the mere facts that

To the number 2 corresponds the logarithm 0.301 03, "" " 0.477 12.

we are not justified in drawing any conclusion whatever respecting the logarithms of numbers between 2 and 3. Hence some one or more hypotheses are always necessary as the base of any system of interpolation. The hypotheses always adopted are these two:

- 1. That, supposing the argument to vary uniformly, the function varies according to some regular law.
- 2. That this law may be learned from the values of the function given in the table.

These hypotheses are applied in the process of differencing, the

<sup>\*</sup> The study of this subject will be facilitated by first mastering so much of it as is contained in the author's College Algebra, §§ 299-302.

It is also recommended to the beginner in the subject that, before going over the algebraic developments, he practise the methods of computation according to the rules and formulæ, so as to have a clear practical understanding of the notation. He can then more readily work out the developments.

nature of which will be seen by the following example, where it is applied to the logarithms of the numbers from 30 to 37:

	Function.	⊿′	⊿''	⊿'''	<b>⊿</b> ¹+
log 30.	1.477 12	1424			
" 31.	$1.491\ 36\ \mathrm{T}$	1379	<b> 45</b>	⊥ 9	
<b>~~32.</b>	$1.505\ 15\ $	1336	<b>- 43</b>	IÃ	+ 2
<b>"</b> 33.	1.51851	1297	<b>— 39</b>	$T_{1}$	<b>— 3</b>
" <b>34</b> .	1.531 48 $\top$	1259	<b>— 38</b>	$\frac{1}{2}$	+1
<b>" 35.</b>	1.544 07	1223	<b>— 36</b>	$+\tilde{3}$	+1
<b>" 36.</b>	1.556 30 🚆	1190	<b>—</b> 33	T 0	
" <b>37.</b>	1.568 20 T	- 1100			

The column  $\Delta'$  gives each difference between two consecutive values of the function, formed by subtracting each number from that next following. These differences are called *first differences*.

The column  $\Delta''$  gives the difference between each two consecutive first differences. These are called second differences.

In like manner the numbers in the succeeding columns, when written, are called third differences, fourth differences, etc.

Now if, in continuing the successive orders of differences, we find them to continually become smaller and smaller, or to converge toward zero, this fact shows that the values of the functions follow a regular law, and the first hypothesis is therefore applicable.

In order to apply interpolation we must then assume that the intermediate values of the function follow the same law. The truth of this assumption must be established in some way before we can interpolate with mathematical rigor, but in practice we may suppose it true in the absence of any reason to the contrary.

26. Effect of errors in the values of the functions. In the preceding example it will be noticed that if we continue the orders of differences beyond the fourth, they will begin to increase and become irregular. This arises from the imperfections of the logarithms, owing to the omission of decimals beyond the fifth, already described in § 11.

When we find the differences to become thus irregular, we must be able to judge whether this irregularity arises from actual errors in the original numbers, which ought to be corrected, or from the small errors necessarily arising from the omission of decimals.

The great advantage of differencing is that any error, however small, in the quantities differenced, unless it follows a regular law, will be detected by the differences. To show the reason of this, we investigate what effect errors in the given functions will have upon the successive orders of differences.

THEOREM. The differences of the sum of two quantities are equal to the sums of their differences.

General proof. Let

$$f_1$$
,  $f_2$ ,  $f_3$ , etc., be one set of functions;  $f_1'$ ,  $f_2'$ ,  $f_3'$ , etc., another set.

$$f_1 + f_1'$$
,  $f_2 + f_3'$ ,  $f_3 + f_3'$ , etc., will then be their sums.

In the first of the following columns we place the first differences of f, in the second those of f', and in the third those of f + f', each formed according to the rule:

$$f_{\bullet} - f_{1}$$
  $f_{\bullet}' - f_{1}'$   $f_{\bullet} + f_{0}' - (f_{1} + f_{1}')$   
 $f_{\bullet} - f_{\bullet}$  etc.  $f_{\bullet}' - f_{0}'$   $f_{\bullet} + f_{\bullet}' - (f_{0} + f_{0}')$ 

It will be seen that the quantities in the third column are the sums of those in the first two.

#### NUMERICAL EXAMPLE.

f <u>A</u> '	f' ∆'	$f+f'$ $\Delta'$
$^{14}$ $_{\perp}$ 25	$1_{\perp 2}$	15 _ 27
$\frac{39}{50} + \frac{20}{11}$	$\frac{3}{a} + \frac{\sim}{3}$	$\frac{42}{50} + \frac{7}{14}$
$     \begin{array}{r}                                     $	$egin{array}{c} rac{1}{3} + 2 \\ 6 + 3 \\ 10 + 4 \end{array}$	$15 + 27 \\ 42 + 14 \\ 56 + 14 \\ 9 - 47$

We see that the third set of values of  $\Delta'$  follow the theorem.

Because the second differences are the differences of the first, the third the differences of the second, etc., it follows that the theorem is true for differences of any order.

Now when we write a series of functions in which the decimals exceeding a certain order are omitted, we may conceive each written number to be composed of the algebraic sum of two quantities, namely:

- 1. The true mathematical value of the function.
- 2. The negative of the omitted decimals.

Example. In the preceding collection of logarithms, since the true value of log 30 is 1.477 121 3..., we may conceive the quantity written to be

$$1.477\,12 = \log 30 - .000\,001\,3\ldots$$

Hence the differences actually written are the differences of the true logarithms minus the differences of the errors. Now suppose the errors to be alternately +0.5 and -0.5 = the point marking off the last decimal. Their differences will then be as follows:

It is evident that the *n*th order of differences of the errors are equal to  $\pm 2^{n-1}$ . Hence, in this case, if the *n*th order of differences of the true values of the function were zero, still, in consequence of the omission of decimals, the actual differences of the *n*th order would be  $2^{n-1}$ .

This, however, is a very extreme case, since it is beyond all probability that the errors should alternate in this way. A more probable average example will be obtained by supposing a single number to have an error of 0.5, while the others are correct. We shall then have:

In this case the maximum value of the difference of the *n*th order is 1.5 in the differences of the third order, 3 in those of the fourth, 5 in those of the fifth, etc. Its general expression is

$$\frac{1}{2}\frac{n(n-1)(n-2)\ldots(n-s+1)}{1\cdot 2\cdot 3\cdot \ldots s}$$
,

where n is the order of differences, and

$$s = \frac{n}{2} \text{ or } \frac{n-1}{2}$$

according as n is even or odd. Thus:

$$\Delta' = \frac{1}{2};$$

$$\Delta'' = \frac{1}{2} \cdot \frac{2}{1} = 1;$$

$$\Delta''' = \frac{1}{2} \cdot \frac{3}{1} = 1.5;$$

$$\Delta^{1v} = \frac{1}{2} \cdot \frac{4 \cdot 3}{1 \cdot 2} = 3;$$

$$\Delta^{\tau} = \frac{1}{2} \cdot \frac{5 \cdot 4}{1 \cdot 2} = 5;$$
etc.
etc.

This being about the average case, in actual practice the differences may be two or three times as great without necessarily implying an error greater than 0.5 in the numbers written.

We have now the following general rule for judging whether a series of numbers do really follow a uniform law:

Difference the series until we reach an order of differences in which the + and - signs either alternate or follow each other irregularly.

If none of the differences of this order expressed in units of the last place of decimals exceed the limit

$$\frac{n(n-1)\ldots(n-s+1)}{1\cdot 2\cdot 3\cdot \ldots s}$$

—that is, the value of the largest binomial coefficient of the nth order—the given numbers may be assumed to follow a regular law, and therefore to be correct to a unit in the last figure.

If some differences exceed this limit, their quotient by the above binomial coefficient may be considered to show the maximum error with which the number opposite it is probably affected.

We can thus detect an isolated error in a series of numbers with great certainty. Suppose, for example, an error of 2 in some number of the series. Differencing the series 0, 0, 0, 2, 0, 0, we shall find the four largest differences of the fifth order to be -10, +20, -20, +10, which would enable us to hit at once upon the erroneous number and judge of the magnitude of its error.

An error near the beginning and end of the series of numbers of which the differences are taken cannot be detected by the differences unless it is considerable. If, for instance, the first or last number is in error by 1, the error of each order of differences will only be 1, as we may easily see by the following example:

It is only in those differences which are on or near the same line as the numbers which are magnified in the way we have shown. But at the beginning and end of the series we cannot determine these differences.

Examining the various tables of differences, we see that n numbers have n-1 first differences, n-2 second differences, and so on, the number diminishing by 1 with each succeeding order. Hence, unless the number of given functions exceeds the index expressing the order of differences which we have to form, no certain conclusion can be drawn.

What is here said of the correctness of the numbers when the differences run properly must be understood as applicable to isolated errors only. If all the numbers were subject to an error following a regular law, this error would not be detected by the differences because, from the nature of the case, the latter only show deviations from some regular law.

# 27. Fundamental Formulæ of Interpolation.

We suppose a series of numbers to be differenced in the way already shown, and the various differences to be designated as in the following scheme, which is supposed to be a selection from a series preceding and following it.

It will be seen that the lower indices are chosen so as to show on which line a difference of any order falls. Thus all quantities with index 2 are on one horizontal line, those with index  $\frac{1}{2} = 2\frac{1}{2}$  are half a line below, etc. This notation is a little different from that used in algebra, but the change need not cause any confusion.

It is shown in algebra that if n be any index, we have

$$u_{n} = u_{0} + n\Delta'_{0} + \frac{n(n-1)}{1.2}\Delta''_{1} + \frac{n(n-1)(n-2)}{1.2.3}\Delta'''_{0} + \text{etc.}; \qquad (a)$$

the notation being changed as in the preceding scheme.

Now the fundamental hypothesis of interpolation is that this formula, which can be demonstrated only for integral values of n, is true also for fractional values; that is, for values of the function u between those given in the table or in the above scheme. We therefore suppose this formula to express the value of the function u for any value of n between 0 and 1.

For values between +1 and +2 we have only to increase the indices of u and its differences by unity, thus:

$$u_{1+n} = u_1 + n\Delta'_{\frac{1}{2}} + \frac{n(n-1)}{1\cdot 2}\Delta''_{\frac{1}{2}} + \text{etc.},$$

and by supposing n to increase from 0 to 1 in this formula we shall have values of u from u, to u.

Increasing the indices again—that is, applying our general formulæ to a row of quantities one line lower—we shall have

$$u_{n+n} = u_n + n\Delta'_n + \frac{n(n-1)}{1 \cdot n^2}\Delta''_n + \text{etc.}$$

The equation (a) is known as Newton's formula of interpolation.

#### 28. Transformations of the Formula of Interpolation.

In the equation (a) and those following it, the formula of interpolation is not in its most convenient form. We shall therefore transform it so that the differences employed shall be symmetrical with respect to the functions between which the interpolation is to be made.

In working these transformations we shall suppose the sixth and following orders of differences to be so small as not to affect the result. These differences being supposed zero, any two consecutive fifth differences may be supposed equal.

First transformation. Let us first find what the original formula (a) will become when, instead of using the series of differences

 $\Delta'_{1}$ ,  $\Delta''_{1}$ ,  $\Delta'''_{1}$ ,  $\Delta^{1}_{1}$ , etc.,

we use

$$\Delta'_{\frac{1}{2}}$$
,  $\Delta'''_{0}$ ,  $\Delta''''_{\frac{1}{2}}$ ,  $\Delta^{1v}_{0}$ , etc.

To effect the transformation we must find the values of the first series of differences in terms of the second, and substitute them in the formula (a).

We find, by the mode of forming the differences,

$$\Delta''_{1} = \Delta''_{0} + \Delta'''_{1}; 
\Delta'''_{1} = \Delta'''_{1} + \Delta^{1}_{1}; 
= \Delta'''_{1} + \Delta^{1}_{1} + \Delta^{1}_{1}; 
\Delta^{1}_{1} = \Delta^{1}_{0} + \Delta^{1}_{1} + \Delta^{1}_{1}; 
\Delta^{1}_{1} + \Delta^{1}_{1} + \Delta^{1}_{1} + \Delta^{1}_{1}; 
\Delta^{1}_{1} + \Delta^{1}_{1} + \Delta^{1}_{1} + \Delta^{1}_{1}; 
\Delta^{1}_{1} + \Delta^{$$

for which, because we suppose the values of  $\Delta^{v}$  to be equal, we may put

$$\Delta^{iv}_{2} = \Delta^{iv}_{0} + 2\Delta^{v}_{1};$$
  
 $\Delta^{v}_{3} = \Delta^{v}_{1}.$ 

Making these substitutions in (a), we have

$$u_{n} = u_{o} + n\Delta'_{i} + \frac{n(n-1)}{1 \cdot 2} (\Delta''_{o} + \Delta'''_{i})$$

$$+ \frac{n(n-1)(n-2)}{1 \cdot 2 \cdot 3} (\Delta'''_{i} + \Delta^{1}_{o} + \Delta^{1}_{i})$$

$$+ \frac{n(n-1)(n-2)(n-3)}{1 \cdot 2 \cdot 3 \cdot 4} (\Delta^{1}_{o} + 2\Delta^{1}_{i})$$

$$+ \frac{n(n-1) \cdot \dots \cdot (n-4)}{1 \cdot 2 \cdot 3 \cdot 4 \cdot 5} \Delta^{1}_{i}.$$

Reducing by collecting the coefficients of equal differences, we find

$$u_{n} - u_{o} = n\Delta'_{i} + \frac{n(n-1)}{1 \cdot 2} \Delta'''_{o} + \frac{(n+1)n(n-1)}{1 \cdot 2 \cdot 3} \Delta'''_{i} + \frac{(n+1)n(n-1)(n-2)}{1 \cdot 2 \cdot 3 \cdot 4} \Delta^{iv}_{o} + \frac{(n+2)(n+1)n(n-1)(n-2)}{1 \cdot 2 \cdot 3 \cdot 4 \cdot 5} \Delta^{v}_{o}.$$
 (b)

Second transformation. Next, instead of the series of this last formula, (b),

 $\Delta'_{\frac{1}{2}}$ ,  $\Delta''_{\frac{1}{2}}$ ,  $\Delta'''_{\frac{1}{2}}$ ,  $\Delta^{i}v_{\frac{1}{2}}$ , etc.,

let us use

$$\Delta'_{-\frac{1}{2}}$$
,  $\Delta'''_{0}$ ,  $\Delta'''_{-\frac{1}{2}}$ ,  $\Delta^{iv}_{0}$ , etc.

To effect this transformation we substitute in (b) for  $\Delta'_{i}$ ,  $\Delta''_{i}$ , etc.,

$$\Delta'_{\frac{1}{2}} = \Delta'_{-\frac{1}{2}} + \Delta''_{0};$$
  
 $\Delta'''_{\frac{1}{2}} = \Delta'''_{-\frac{1}{2}} + \Delta^{1v}_{0};$   
 $\Delta^{v}_{\frac{1}{2}} = \Delta^{v}_{-\frac{1}{2}}.$ 

The series (b) then changes into

$$u_{n} - u_{0} = n\Delta'_{-\frac{1}{2}} + \frac{n(n+1)}{1 \cdot 2} \Delta''_{0} + \frac{(n+1)n(n-1)}{1 \cdot 2 \cdot 3} \Delta'''_{-\frac{1}{2}} + \frac{(n+2)(n+1)n(n-1)}{1 \cdot 2 \cdot 3 \cdot 4} \Delta^{\frac{1}{2}}_{0} + \frac{(n+2)(n+1)n(n-1)(n-2)}{1 \cdot 2 \cdot 3 \cdot 4 \cdot 5} \Delta^{\frac{1}{2}}_{-\frac{1}{2}}.$$
 (c)

Third transformation. Stirling's formula. We effect a third transformation by taking the half sum of the equations (b) and (c), which gives us a formula perfectly symmetrical with respect to the lines of differences, namely,

$$u_{n} - u_{0} = n \frac{\Delta'_{-\frac{1}{2}} + \Delta'_{\frac{1}{2}}}{2} + \frac{n^{2}}{2} \Delta''_{0} + \frac{n(n^{2} - 1)}{1 \cdot 2 \cdot 3} \frac{\Delta'''_{-\frac{1}{2}} + \Delta'''_{\frac{1}{2}}}{2} + \frac{n^{2}(n^{2} - 1)}{1 \cdot 2 \cdot 3} \Delta^{1}_{0} + \frac{n(n^{2} - 1)(n^{2} - 4)}{1 \cdot 2 \cdot 3} \frac{\Delta''_{-\frac{1}{2}} + \Delta'}{2} + \text{etc.}, (d)$$

which is known as Stirling's formula of interpolation.

It will be seen that we have put

$$n^{2}-1$$
 for  $(n+1)$   $(n-1)$ ,  $n^{2}-4$  for  $(n+2)$   $(n-2)$ , etc.

Fourth transformation. In the equation (b), instead of the series of differences

 $\Delta'_{\frac{1}{2}}$ ,  $\Delta'''_{\frac{1}{2}}$ ,  $\Delta^{iv}_{\frac{1}{2}}$ , etc.,

let us use

$$\Delta'_1$$
,  $\Delta'''_1$ ,  $\Delta'''_1$ ,  $\Delta^{iv}_1$ , etc.

To effect this we put

$$\Delta^{\prime\prime}_{\bullet} = \Delta^{\prime\prime}_{\bullet} - \Delta^{\prime\prime\prime}_{\bullet};$$

$$\Delta^{iv}_{\bullet} = \Delta^{iv}_{\bullet} - \Delta^{v}_{\bullet}.$$

Making these substitutions in (b), it becomes

$$u_{n} - u_{o} = n\Delta'_{i} + \frac{n(n-1)}{1.2}\Delta''_{i} + \frac{n(n-1)(n-2)}{1.2.3}\Delta'''_{i} + \frac{(n+1)n(n-1)(n-2)}{1.2.3.4}\Delta^{1v}_{i} + \frac{(n+1)n(n-1)(n-2)(n-3)}{1.2.3.4.5}\Delta^{v}_{i}.$$
 (e)

Fifth transformation. Bessel's formula. Let us take half the sum of the equations (e) and (b). We then have

$$u_{n} - u_{o} = n\Delta'_{i} + \frac{n(n-1)}{1 \cdot 2} \frac{\Delta''_{o} + \Delta''_{o}}{2} + \frac{n(n-1)(n-\frac{1}{2})}{1 \cdot 2 \cdot 3} \Delta'''_{i} + \frac{(n+1)n(n-1)(n-2)}{1 \cdot 2 \cdot 3 \cdot 4} \frac{\Delta^{1}}{2} + \frac{(n+1)n(n-1)(n-2)(n-\frac{1}{2})}{1 \cdot 2 \cdot 3 \cdot 4 \cdot 5} \Delta^{r}_{i}, \quad (f)$$

which is commonly known as Bessel's formula of interpolation, and which is the one most convenient to use in practice.

In applying this formula to find a value of the function intermediate between two given values, we must always suppose the index 0 to apply to the given value next preceding that to be found, and the index 1 to apply to that next following. The quantity n will then be a positive proper fraction.

29. Example of interpolation to halves. If we increase the logarithms of 30, 31, etc., already given, by unity, we shall have the logarithms of 300, 310, 320, etc. It is required to find, by interpolation, the logarithms of the numbers half way between the given ones (omitting the first and last), namely, the logarithms of 315, 325, 335, etc.

Here, the required quantities depending upon arguments half way between the given ones, we have  $n = \frac{1}{2}$ , and the values of the Besselian coefficient, so far as wanted, are

$$\frac{n(n-1)}{2} = -\frac{1}{8};$$

$$\frac{n(n-1)(n-\frac{1}{2})}{6} = 0.$$

The subsequent terms are neglected, being insensible. So, if we put  $a_0$  and  $a_1$  for any consecutive two of the numbers 300, 310, etc., we have

and 
$$\log (a_{\bullet} + 5) = \log a_{\bullet} + \left(\frac{1}{2}\Delta'_{\bullet} - \frac{1}{8}\frac{\Delta''_{\bullet} + \Delta''_{\bullet}}{2}\right)$$

$$\log (a_{\bullet} - 5) = \log a_{\bullet} - \left(\frac{1}{2}\Delta'_{\bullet} + \frac{1}{8}\frac{\Delta''_{\bullet} + \Delta''_{\bullet}}{2}\right),$$
(h)

where we put  $\Delta_{\mathbf{i}}$  for that first difference between  $a_{\mathbf{i}}$  and  $a_{\mathbf{i}}$ .

These two formulæ are two expressions for the same quantity, because  $a_0 + 5 = a_1 - 5$ . They are both used in such a way as to provide a check upon the accuracy of the work. For this purpose we compute the two quantities

$$\log (a_{\bullet} + 5) - \log a_{\bullet} = \frac{1}{2} \Delta'_{\frac{1}{4}} - \frac{1}{8} \frac{\Delta''_{\bullet} + \Delta''_{1}}{2}, \log a_{1} - \log (a_{\bullet} + 5) = \frac{1}{2} \Delta'_{\frac{1}{4}} + \frac{1}{8} \frac{\Delta''_{\bullet} + \Delta''_{1}}{2}.$$
(k)

The most convenient and expeditious way of doing the work is shown in the accompanying table, where we give every figure which it is necessary to write, besides those found on p. 57. The following is the plan of computation:

No. Log. Diff. 
$$\frac{1}{2}\Delta'_1$$
,  $\frac{1}{8}\frac{\Delta''_0 + \Delta''_1}{2}$ .  $\frac{\Delta''_0 + \Delta''_1}{2}$ .  $\frac{\Delta''_0 + \Delta''_1}{2}$ .  $\frac{310}{2}$ .  $\frac{3491}{2}$ .  $\frac{369}{2}$ .  $\frac{315}{2}$ .  $\frac{3498}{2}$ .  $\frac{31}{684}$ .  $\frac{684}{683}$ .  $\frac{684}{683}$ .  $\frac{668.0}{688.0}$ .  $\frac{511}{5}$ .  $\frac{668}{683}$ .  $\frac{668.0}{648.5}$ .  $\frac{51}{5}$ .  $\frac{653}{634}$ .  $\frac{648.5}{648}$ .  $\frac{531}{625}$ .  $\frac{48}{634}$ .  $\frac{648.5}{625}$ .  $\frac{540}{625}$ .  $\frac{648.5}{625}$ .  $\frac{648.5}{625}$ .  $\frac{540}{625}$ .  $\frac{648}{625}$ .  $\frac{648.5}{625}$ .  $\frac{648.5}{625}$ .  $\frac{540}{625}$ .  $\frac{648}{625}$ .  $\frac{648.5}{625}$ .  $\frac{648}{625}$ .  $\frac{648.5}{625}$ .  $\frac{648}{625}$ .  $\frac{648}{62$ 

We compute the right-hand column by the formula

$$\frac{\varDelta^{\prime\prime}{}_{\circ}+\varDelta^{\prime\prime}{}_{_{1}}}{2}=\varDelta^{\prime\prime}{}_{\circ}+\frac{1}{2}\varDelta^{\prime\prime\prime}{}_{\flat}=\varDelta^{\prime\prime}{}_{_{1}}-\frac{1}{2}\varDelta^{\prime\prime\prime}{}_{\flat},$$

using the values of  $\Delta$  given in the scheme, p. 57.

This mode of computing the half sum of two numbers which are nearly equal is easier than adding and dividing by 2.

In the next two columns to the left, the sixth place of decimals

is added in order that the errors may not accumulate by the addition of several quantities. This precaution should always be taken when the interpolated quantities are required to be as accurate as the given ones.

The fourth column from the right is formed by adding and subtracting the numbers of the second and third columns according to the formula (k). The additional figure is now dropped, because no longer necessary for accuracy. The numbers thus formed are the first differences of the series of logarithms found by inserting the interpolated logarithms between the given ones, as will be seen by equation (k).

We write the first logarithm of the series, namely,

$$\log 310 = 2.49136$$
,

and then form the subsequent ones by continual addition of the differences, thus:

$$\log 315 = \log 310 + 695;$$
  
 $\log 320 = \log 315 + 684;$   
 $\log 325 = \log 320 + 673;$   
etc. etc. etc.

If the work is correct, the alternate logarithms will agree with the given ones in the former table.

The continuance of the above process for a few more numbers, say up to 450, is recommended to the student as an exercise.

**30.** Interpolation to thirds. Let us suppose the value of a quantity to be given for every third day, and the value for every day to be required. By putting  $n = \frac{1}{3}$  and applying formula (f) to each successive given quantity, we shall have the value for each day following one of those given, and by putting  $n = \frac{2}{3}$  we shall have values for the second day following, which will complete the series. But the interpolation can be executed by a much more expeditious process, which consists in computing the middle difference of the interpolated quantities and finding the intermediate differences by a secondary interpolation.

Let us put

 $f_{\bullet}$ ,  $f_{\bullet}$ ,  $\bar{f}_{\bullet}$ , etc., the given series of quantities;

 $f_{\bullet}$ ,  $f_{1}$ ,  $f_{2}$ ,  $f_{4}$ , etc., the required interpolated series;

- $\Delta'$ ,  $\Delta''$ , etc., the first differences, second differences, etc., of the given series;
- $\delta'$ ,  $\delta''$ , etc., the first differences, second differences, etc., of the interpolated series.

We may then put

$$\begin{array}{ll} f_{\bullet} - f_{\bullet} = \Delta'_{\bullet} & \text{(in the given series);} \\ f_{1} - f_{0} = \delta'_{\bullet} \\ f_{1} - f_{1} = \delta'_{\bullet} \\ f_{\bullet} - f_{1} = \delta'_{\bullet} \end{array}$$
 (in the interpolated series).

We shall then have

$$\delta'_1 + \delta'_2 + \delta'_4 = \Delta'_1$$

The value of  $f_1 - f_0 = \delta_1$  is given by putting  $n = \frac{1}{8}$  in the Besselian formula (f). Thus we find

$$\begin{split} \delta'_{1} &= \frac{1}{3} \varDelta'_{1} - \frac{1}{9} \frac{\varDelta''_{1} + \varDelta''_{1}}{2} + \frac{1}{162} \varDelta'''_{1} \\ &+ \frac{5}{243} \frac{\varDelta^{1}_{1} + \varDelta^{1}_{2}}{2} - \frac{1}{1458} \varDelta^{1}_{1}, \end{split}$$

Putting  $n = \frac{2}{3}$ , we have the value of  $f_1 - f_2$ , that is, of  $\delta'_1 + \delta'_2$ . Thus we find

$$\delta'_{1} + \delta'_{2} = \frac{2}{3} \Delta'_{1} - \frac{1}{9} \frac{\Delta''_{1} + \Delta''_{1}}{2} - \frac{1}{162} \Delta'''_{1} + \frac{5}{243} \frac{\Delta^{1}_{1} + \Delta^{1}_{1}}{2} + \frac{1}{1458} \Delta^{1}_{1}$$

Subtracting these expressions, we have

$$\delta'_{i} = \frac{1}{3} \Delta'_{i} - \frac{1}{81} \Delta'''_{i} + \frac{1}{729} \Delta'_{i}$$

which is most easily computed in the form

$$\delta'_{\bullet} = \frac{1}{3} \left\{ \Delta'_{\bullet} - \frac{1}{27} \left( \Delta'''_{\bullet} - \frac{1}{9} \Delta^{\mathsf{v}}_{\bullet} \right) \right\}. \tag{m}$$

We see that the computation of  $\delta'_{\sharp}$ , the middle difference of the interpolated quantities, is much simpler than that of  $\delta'_{\sharp}$ . It will therefore facilitate the work to compute only these middle differences, and to find the others by interpolation.

This process is again facilitated, in case the second differences are considerable, by first computing the second differences of the interpolated series on the same plan. The formulæ for this purpose are derived as follows:

Let us put

$$\delta'_{i} = f_{i} - f_{i}.$$

The second difference of which we desire the value is then

$$\delta''_{\bullet} = \delta'_{\bullet} - \delta'_{\bullet}.$$

The value of  $\delta'$  is given by the equation

$$\delta'_{\bullet} = \Delta'_{\bullet} - (\delta'_{\bullet} + \delta'_{\bullet}),$$

and the value of  $\delta'_{4}$  is found from that of  $\delta'_{4}$  by simply increasing the indices of the differences by unity, because it belongs to the next lower line.

We thus find

$$\delta'_{i} = \frac{1}{3} \Delta'_{i} - \frac{1}{9} \frac{\Delta''_{i} + \Delta''_{i}}{2} + \frac{1}{162} \Delta'''_{i}$$

$$+ \frac{5}{243} \frac{\Delta^{i}_{i} + \Delta^{i}_{i}}{2} - \frac{1}{1458} \Delta'_{i};$$

$$\delta'_{i} = \frac{1}{3} \Delta'_{i} + \frac{1}{9} \frac{\Delta''_{i} + \Delta''_{i}}{2} + \frac{1}{162} \Delta'''_{i}$$

$$- \frac{5}{243} \frac{\Delta^{i}_{i} + \Delta^{i}_{i}}{2} - \frac{1}{1458} \Delta'_{i}.$$

Then by subtraction,

$$\begin{split} \delta^{\prime\prime\prime}_{\bullet} &= \frac{1}{3} (\varDelta^{\prime}_{\bullet} - \varDelta^{\prime}_{\bullet}) - \frac{1}{9} \, \frac{\varDelta^{\prime\prime}_{\bullet} + 2\varDelta^{\prime\prime}_{,} + \varDelta^{\prime\prime}_{,}}{2} + \frac{1}{162} (\varDelta^{\prime\prime\prime}_{\bullet} - \varDelta^{\prime\prime\prime}_{\bullet}) \\ &+ \frac{5}{243} \, \frac{\varDelta^{\mathsf{l}\,\mathsf{v}}_{\bullet} + 2\varDelta^{\mathsf{l}\,\mathsf{v}}_{,} + \varDelta^{\prime\prime}_{,}}{2} - \frac{1}{1458} (\varDelta^{\mathsf{v}\,\mathsf{g}} - \varDelta^{\mathsf{v}}_{\bullet}). \end{split}$$

Reducing the first of these terms, we have

$$\Delta'_{\bullet} - \Delta'_{\bullet} = \Delta''_{\bullet}.$$

For the second term,

$$\Delta''_{\bullet} = \Delta''_{1} - \Delta'''_{1};$$
 $\Delta''_{\bullet} = \Delta''_{1} + \Delta'''_{1};$ 

whence

and

$$\Delta''_{\bullet} + \Delta''_{\bullet} = 2\Delta''_{1} + \Delta'''_{\bullet} - \Delta'''_{\bullet} = 2\Delta''_{1} + \Delta^{\mathsf{Iv}}_{\bullet},$$

$$\frac{\Delta''_{\bullet} + 2\Delta''_{1} + \Delta''_{2}}{2} = 2\Delta''_{1} + \frac{1}{2}\Delta^{\mathsf{Iv}}_{\bullet}.$$

For the third term,

$$\Delta^{\prime\prime\prime\prime} = \Delta^{\prime\prime\prime\prime} = \Delta^{1} ,$$

For the fourth term, dropping the terms in  $\Delta^{vi}$  as too small in practice, we may put

$$\frac{\Delta^{\mathrm{i}\mathsf{v}}_{\bullet} + 2\Delta^{\mathrm{i}\mathsf{v}}_{1} + \Delta^{\mathrm{i}\mathsf{v}}_{2}}{2} = 2\Delta^{\mathrm{i}\mathsf{v}}_{1}.$$

The difference of the fifth terms may also be dropped, because they contain only sixth differences.

Making these substitutions in the value of  $\delta''$ , we find

$$\delta''_{\bullet} = \frac{1}{3} \Delta''_{1} - \frac{1}{9} \left( 2\Delta''_{1} + \frac{1}{2} \Delta^{i} \mathbf{v}_{1} \right) + \frac{1}{162} \Delta^{i} \mathbf{v}_{1} + \frac{10}{243} \Delta^{i} \mathbf{v}_{1}$$

$$= \frac{1}{9} \Delta''_{1} - \frac{2}{243} \Delta^{i} \mathbf{v}_{1}$$

$$= \frac{1}{9} \left( \Delta''_{1} - \frac{2}{27} \Delta^{i} \mathbf{v} \right). \tag{n}$$

By this formula we may compute every third value of  $\delta''$ , and then interpolate the intermediate values. By means of these values we find by addition the intermediate values of  $\delta'$ , of which every third value has been computed by formula (m). Then, by continually adding the values of  $\delta'$ , we find those of the function f.

As an example of the work, we give the following values of the sun's declination for every third day of part of July, 1886, for Greenwich mean noon:

The values of  $\Delta^{iv}$  are too small to have any influence.

The whole work of interpolation is shown in the following table, where, as before, the right-hand column is that first computed, and gives the value of  $\Delta' - \frac{1}{27}\Delta'''$  according to formula (m):

To make the process in the example clear, the computed differences, etc., are printed in heavier type than the interpolated ones.

It is also to be remarked that the sum of the three consecutive values of  $\delta''$ , formed of one computed value and the interpolated values next above and below it, should be equal to the difference between the corresponding computed first differences. For instance,

$$23''.27 + 23''.10 + 22''.93 = 7' 49''.59 - 6' 40''.29$$
.

But in the first computation this condition will seldom be exactly fulfilled, owing to the errors arising from omitted decimals and other sources. If the given quantities are accurate, the errors should never exceed half a unit of the last decimal in the given quantities, or five units in the additional decimal added on in dividing.

To correct these little imperfections after the interpolation of the second differences, but before that of the first differences, the sum of the last two figures in each triplet of second differences should be formed, and if it does not agree with the difference of the first differences, the last figures of the second difference should each be slightly altered, to make the sum exact.

The first differences can then be formed by addition.

In the same way, the sum of three consecutive first differences should be equal to the difference between the given quantities. If, as is generally the case, this condition is not exactly fulfilled, the differences should be altered accordingly. This alteration may, however, be made mentally while adding to form the required interpolated functions.

As an exercise for the student we give the continuance of the sun's declination for the remainder of the month, to be interpolated for the intermediate dates from July 15th onward:

	0	,	"
July 21	20	27	16.5
24			
27	19	11	22.7
30	18	29	4.8
Aug. 2	17	44	3.1

As another exercise the logarithms of the intermediate numbers from 998 to 1014 may be interpolated by the following table:

Number.	Logarithm.
994	. 2.997 386 4
997	. 2.998 695 2
1000	. <b>3.</b> 000 000 0
1003	. 3.001 300 9
1006	. 3.002 598 0
1009	. 3.003 891 2
1012	. 3.005 180 5
1015	
1018	

32. Interpolation to fifths. Let us next investigate the formulæ when every fifth quantity is given and the intermediate ones are to be found by interpolation. By putting  $n = \frac{n}{2}$  in the Besselian formula, we shall have the value of the interpolation function second

following one of the given ones, and by putting  $n = \frac{n}{2}$  that third following. The difference will be the middle interpolated first difference of the interpolated series. Putting  $n = \frac{n}{2}$  in (f), we have

$$u_{1} = u_{0} + \frac{2}{5}\Delta'_{1} - \frac{2.3}{2.5^{3}}\frac{\Delta''_{0} + \Delta''_{1}}{2} + \frac{2.3.1}{2^{3}.3.5^{3}}\Delta'''_{1} + \frac{2.3.7.8}{2.3.4.5^{4}}\frac{\Delta^{1}_{0} + \Delta^{1}_{1}}{2} - \frac{2.3.7.8.1}{2^{3}.3.4.5}\Delta'_{1}.$$

Putting  $n = \frac{3}{5}$ , we have

$$u_{i} = u_{o} + \frac{3}{5}\Delta'_{i} - \frac{2.3}{2.5^{2}}\frac{\Delta''_{o} + \Delta''_{1}}{2} - \frac{2.3.1}{2^{2}.3.5^{3}}\Delta'''_{i} + \frac{2.3.7.8}{2.3.4.5^{4}}\frac{\Delta^{1}_{o} + \Delta^{1}_{1}}{2} + \frac{8.3.2.7.1}{2^{2}.3.4.5.5^{3}}\Delta'_{i}$$

The difference of these expressions, being reduced, gives

$$u_{i} - u_{i} = \frac{1}{5} \Delta'_{i} - \frac{1}{125} \Delta'''_{i} + \frac{14}{15625} \Delta^{v}_{i}$$
$$= \frac{1}{5} \left\{ \Delta'_{i} - \frac{1}{25} \left( \Delta'''_{i} - \frac{14}{125} \Delta^{v}_{i} \right) \right\}.$$

The term in  $\Delta^{\tau}$  will not produce any effect unless the fifth differences are considerable, and then we may nearly always, in practice, put  $\frac{1}{4}$  instead of  $\frac{14}{125}$ .

The interpolated second differences opposite the given functions are most readily obtained by Stirling's formula, (d). Putting  $n = \frac{1}{2}$ , we have the following value of the interpolated first differences immediately following a given value of the function:

$$u_{\frac{1}{4}} - u_{\bullet} = \frac{1}{5} \frac{\Delta'_{-\frac{1}{4}} + \Delta'_{\frac{1}{4}}}{2} + \frac{1}{50} \Delta''_{\bullet} - \frac{24}{6.5.25} \frac{\Delta'''_{-\frac{1}{4}} + \Delta'''_{\frac{1}{4}}}{2} - \frac{24}{6.5.20.25} \Delta^{\text{lv}}_{\bullet} + \text{etc.}$$

Again, putting  $n = -\frac{1}{5}$ , and changing the signs, we find for the first difference next preceding a given function

$$u_{\bullet} - u_{-\frac{1}{2}} = \frac{1}{5} \frac{\Delta'_{-\frac{1}{2}} + \Delta'_{\frac{1}{2}}}{2} - \frac{1}{50} \Delta''_{\bullet} - \frac{24}{6.5.25} \frac{\Delta'''_{-\frac{1}{2}} + \Delta'''_{\frac{1}{2}}}{2} + \frac{24}{6.5.20.25} \Delta^{1}_{\bullet} - \text{etc.}$$

The difference of these quantities gives the required second difference, which we find to be

$$\delta''_{\bullet} = \frac{1}{25} \Delta''_{\bullet} - \frac{2}{625} \Delta^{!v}_{\bullet} = \frac{1}{25} (\Delta''_{\bullet} - \frac{2}{25} \Delta^{!v}_{\bullet}).$$

As an example and exercise we show the interpolation of logarithms when every fifth logarithm is given:

Number.	Logarithm.	δ'	δ"	⊿′	⊿"
1000	<b>3.</b> 000 000 0			+ 21 661	
1005	3.002 166 1	4319.2	-4.32	,	- 108
1006	.002 598 0	4314.9	<b>- 4.31</b>		
1007	.003 029 5	4310.6	-4.30		
1008	.003 460 6	4306.3	<b>- 4.30</b>	+21553	
1009	.003 891 2	4302.0	-4.29	•	
1010	3.004 321 4		-4.28		- 107
1011	.004 751 2	4297.7	-4.27		
1012	.005 180 5	4293.5	-4.26		
1013	.005 609 4	4289.2	-4.23	+ 21 446	
1014	.006 037 9	4285.0	-4.20	•	
1015	3.006 466 0	4280.8	<b>- 4.16</b>	+ 21 342	<b>- 104</b>
1020	3.008 600 2			•	
1025	3.010 723 9				
1030	3.012 837 2				
1035	3.014 940 3				
1040	3.017 033 3				

### FORMULÆ

FOR THE SOLUTION OF

PLANE AND SPHERICAL TRIANGLES.

#### REMARKS.

1. It is better to determine an angle by its tangent than by its sine or cosine, because a small angle or an angle near 180° cannot be accurately determined by its cosine, nor one near either 90° or 270° by its sine.

Sometimes, however, the data of the problem are such that the angle can be determined only through its sine or cosine. Any uncertainty which may then arise from the source pointed out is then inherent in the problem; e.g., if the hypothenuse and one side of a right triangle are 0.39808 and 0.39806 respectively (sixth and following decimals being omitted), the value of the included angle may be anywhere between 0° 25′ and 0° 42′, no matter what method of computation be adopted.

- 2. If the sine and cosine can be independently computed, their agreement as to the angle will generally serve as a check on the accuracy of the computation. If they agree, their quotient will give the tangent.
- 3. It is desirable, when possible, to have a check upon the accuracy of the computation; that is, to make a computation which must give a certain result if the work is right. But no check can give a positive assurance of accuracy: all it can do is to make it more or less improbable that a mistake exceeding a certain limit exists.
- 4. In the following list several formulæ are sometimes given as applicable to the same problem. In such cases, the most convenient for the special purpose must be chosen.

**Notation.** a, b, and c are the three sides. A, B, and C are the opposite angles.

### PLANE TRIANGLES.

Given.	Required.	$s = \frac{1}{2}(a+b+c).$
a, b, c, the three sides.	A, one angle.	$\tan \frac{1}{2} A = \sqrt{\frac{(s-b)(s-c)}{s(s-a)}}.$
sides.	A, B, C, all the	$H = \sqrt{\frac{(s-a)(s-b)(s-c)}{s}};$
	angles.	$\tan \frac{1}{2}A = \frac{H}{s-a};$
		$\tan \frac{1}{2}B = \frac{H}{s-b};$
		$\tan \frac{1}{2} C = \frac{H}{s-c}.$
		Checks: $A + B + C = 180^{\circ}$ ; $\frac{a}{\sin A} = \frac{b}{\sin B} = \frac{c}{\sin C}$
		$\sin A - \sin B - \sin C$
b, c, A, two sides	B and $C$ , the other	$\tan \frac{1}{2}(B-C) = \frac{b-c}{b+c} \cot \frac{1}{2}A;$
and the	angles.	. • • • • • • • • • • • • • • • • • • •
included		$\frac{1}{2}(B+C) = 90^{\circ} - \frac{1}{2}A;$ $B = \frac{1}{2}(B+C) + \frac{1}{2}(B-C);$
angle.		$C = \frac{1}{2}(B+C) + \frac{1}{2}(B-C),$ $C = \frac{1}{2}(B+C) - \frac{1}{2}(B-C).$
		Check, as before.
	a, B, C,	$a \sin \frac{1}{2}(B-C) = (b-c) \cos \frac{1}{2}A;$
	the .	$a\cos\frac{1}{2}(B-C)=(b+c)\sin\frac{1}{2}A.$
	remaining parts.	Having found $a$ and $\frac{1}{2}(B-C)$ , proceed as in the last case.
		as in the last case.
a, b, A,	c, B, C,	$\sin B = \frac{b}{a} \sin A$ ; (two values of B.)
two sides	the re-	. u
and the angle oppo-	maining parts.	$C = 180^{\circ} - (A + B);$
site one of	Lar op-	$c = \frac{b \sin C}{\sin R} = \frac{a \sin C}{\sin A}.$
them.		SILL D SILL A

Given.

a, A, B,
one side
and any
two angles.

Required.
b, c, C,
the remaining
parts.

$$C = 180^{\circ} - (A + B);$$

$$b = \frac{a \sin B}{\sin A};$$

$$c = \frac{a \sin C}{\sin A} = \frac{a \sin (A + B)}{\sin A}.$$

#### RIGHT SPHERICAL TRIANGLES.

a, b, the sides containing the right angle.	A, B, or c.	c is the hypothenuse. $\cot A = \cot a \sin b;$ $\cot B = \cot b \sin a;$ $\cos c = \cos a \cos b;$ $\sin c = \frac{\sin a}{\sin A}.$
	A and c.	$\sin c \sin A = \sin a;$ $\sin c \cos A = \cos a \sin b;$ $\cos c = \cos a \cos b^*$
	$\it B$ and $\it c$	$\sin c \sin B = \sin b;$ $\sin c \cos B = \sin a \cos b.$
a, c, one side and the hy- pothenuse.		$\sin A = \frac{\sin a}{\sin c};$ $\cos B = \tan a \cot c;$ $\cos b = \frac{\cos c}{\cos a}.$
a, A, one side and the opposite angle.	b, c, or B.	$\sin b = \tan a \cot A;$ $\sin c = \frac{\sin a}{\sin A};$ $\sin B = \frac{\cos A}{\cos a}.$
a, B, one side and the adjacent	b, c, or A.	$\tan b = \sin a \tan B;$ $\tan c = \frac{\tan a}{\cos B};$ $\cos A = \cos a \sin B.$
angle.	c and A.	$\sin A \sin c = \sin a;$ $\sin A \cos c = \cos a \cos B;$ $\cos A = \cos a \sin B.$

Given.	Required.	
a, B.	b and A.	$\sin A \sin b = \sin a \sin B;$
•		$\sin A \cos b = \cos B.$
c, A,	a, b,  or  B.	$\sin a = \sin c \sin A;$
the hypo-		$\tan b = \tan c \cos A;$
thenuse		$\cot B = \cos c \tan A.$
and one angle.	a and B.	$\cos a \sin B = \cos A;$ $\cos a \cos B = \sin A \cos c;$ $\sin a = \sin A \sin c.$
	a and b.	$\cos a \sin b = \cos A \sin c;$ $\cos a \cos b = \cos c.$
$\overline{A, B,}$ the two angles.	a, b, or c.	$\cos a = \frac{\cos A}{\sin B};$ $\cos B$
		$\cos b = \frac{\cos B}{\sin A};$
		$\cos c = \cot A \cot B$ .

#### QUADRANTAL SPHERICAL TRIANGLES.

a, b, the two sides.	A, B, or C, either angle.	c is the omitted side equal to 90°.  C is the angle opposite this side. $\cos A = \frac{\cos a}{\sin b};$ $\cos B = \frac{\cos b}{\sin a};$ $\cos C = -\cot a \cot b.$
a, C, one side and the angle oppo-	A, B, or b.	$\sin A = \sin a \sin C;$ $\tan B = -\cos a \tan C;$ $\cot b = -\tan a \cos C.$
site the	A and b.	$\cos A \sin b = \cos a$ ;
right side.		$\cos A \cos b = -\sin a \cos C,$ $\sin A = \sin a \sin C.$
	A and B.	$\cos A \sin B = \cos a \sin C;$ $\cos A \cos B = -\cos C.$

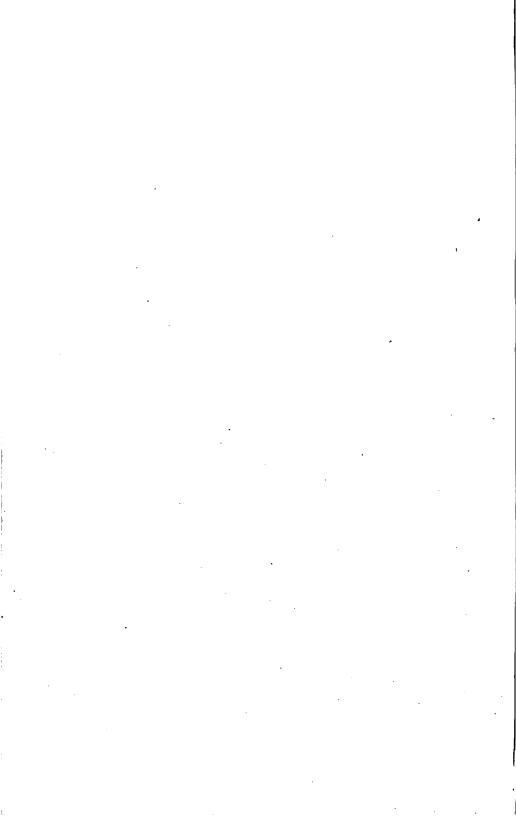
Given.  A, b, one angle and the adjacent side.	Required. $a$ , $B$ , or $C$ . $a$ and $B$ .	$\cos a = \cos A \sin b;$ $\tan B = \sin A \tan b;$ $\cot C = -\cot A \cos b.$ $\sin a \sin B = \sin A \sin b;$ $\sin a \cos B = \cos b;$
	a and C.	$\cos a = \cos A \sin b.$ $\sin a \sin C = \sin A;$ $\sin a \cos C = -\cos A \cos b.$
a, A, one side and the opposite angle.  A, C, one angle and the angle opposite the	a, b, or B.	$\sin b = \frac{\cos a}{\cos A};$ $\sin B = \cot a \tan A;$ $\sin C = \frac{\sin A}{\sin a}.$ $\sin a = \frac{\sin A}{\sin C};$ $\cos b = -\tan A \cot C;$ $\cos B = -\frac{\cos C}{\cos A}.$
right side.	a, b, or C.  a and C.	$\cot a = \cot A \sin B;$ $\cot b = \sin A \cot B;$ $\cos C = -\cos A \cos B.$ $\sin C \sin a = \sin A;$
	b and C.	$\sin C \cos a = \cos A \sin B;$ $\cos C = -\cos A \cos B.$ $\sin C \sin b = \sin B;$ $\sin C \cos b = \sin A \cos B.$

#### SPHERICAL TRIANGLES IN GENERAL.

		D HIGHWOODS IN OBNISHED.
Given.  a, b, c,	Required.  A, B, C,	$s=\frac{1}{2}(a+b+c);$
the three sides.	the three	$H = \sqrt{\frac{\sin(s-a)\sin(s-b)\sin(s-c)}{\sin s}};$
	J	$\tan \frac{1}{2}A = \frac{H}{\sin (s-a)};$
		$\tan \frac{1}{2}B = \frac{H}{\sin (s-b)};$
		$\tan \frac{1}{2} C = \frac{H}{\sin (s-c)}.$
		Check: $\frac{\sin a}{\sin A} = \frac{\sin b}{\sin B} = \frac{\sin c}{\sin C}$
$\overline{a, b, C}$	A and $c$ ,	$\sin c \sin A = \sin a \sin C;$
two sides	one angle	$\sin c \cos A = \cos a \sin b - \sin a \cos b \cos C;$
and the	and the	$\cos c = \cos a \cos b + \sin a \sin b \cos C.$
included	remaining	•
angle.	side.	
	B and $c$ .	$\sin c \sin B = \sin b \sin C;$
		$\sin c \cos B = \sin a \cos b - \cos a \sin b \cos C.$
	l l	If addition and subtraction logarithms
		are not available for this computation, we
		may compute $k$ and $K$ from
		$k \sin K = \sin a \cos C;$
		$k \cos K = \cos a$ .
		Then
		$\sin c \cos A = k \sin (b - K);$
	ļ ,	$\cos c = k \cos (b - K).$
		Also,
		$h \sin H = \sin b \cos C;$
		$h \cos H = \cos b$ .
		Then
		$\sin c \cos B = h \sin (a - H);$ $\cos c = h \cos (a - H).$
		$\cos v = n \cos (a - n).$
	A, B, c,	$\sin \frac{1}{2}c \sin \frac{1}{2}(A-B) = \cos \frac{1}{2}C \sin \frac{1}{2}(a-b);$
	all the	$\sin \frac{1}{2} c \cos \frac{1}{2} (A - B) = \sin \frac{1}{2} C \sin \frac{1}{2} (a + b);$
	remaining	$\cos \frac{1}{2} c \sin \frac{1}{2} (A + B) = \cos \frac{1}{2} C \cos \frac{1}{2} (a - b);$
		$\cos \frac{1}{2} \cos \frac{1}{2} (A+B) = \sin \frac{1}{2} C \cos \frac{1}{2} (a+b).$

Given.  a, b, A, two sides and an opposite angle.	Required.  B, C, c, all the remaining parts.	$\sin B = \frac{\sin A \sin b}{\sin a}  \text{(two values of } B\text{);}$ $\tan \frac{1}{2} C = \frac{\cos \frac{1}{2} (a - b) \cot \frac{1}{2} (A + B)}{\cos \frac{1}{2} (a + b)};$ $\tan \frac{1}{2} c = \frac{\cos \frac{1}{2} (A + B) \tan \frac{1}{2} (a + b)}{\cos \frac{1}{2} (A - B)}$
$\overline{A, B, c}$	a and $C$ ,	$\sin C \sin a = \sin A \sin c;$
two angles	one side	$\sin C \cos a = \cos A \sin B + \sin A \cos B \cos c;$
and the.	and the	$\cos C = -\cos A \cos B + \sin A \sin B \cos c.$
included side.	third angle.	
2-40.	b and $C$ .	$\sin C \sin b = \sin B \sin c;$
		$\sin C \cos b = \sin A \cos B + \cos A \sin B \cos c.$
		If we compute $k$ and $K$ from
		$k \sin K = \cos A$ ,
		$k\cos K = \sin A\cos c,$
		then $\sin C \cos a = k \cos (B - K);$
		$\cos C = k \sin (B - K).$ If we compute h and H from
		$h \sin H = \cos B,$
		$h \cos H = \sin B \cos c$ ,
		then $\sin C \cos b = h \cos (A - H);$
		$\cos C = h \sin (A - H).$
	a, b, C,	$\sin \frac{1}{2} C \sin \frac{1}{2} (a+b) = \sin \frac{1}{2} c \cos \frac{1}{2} (A-B);$
	all the	$\sin \frac{1}{2} C \cos \frac{1}{2} (a+b) = \cos \frac{1}{2} c \cos \frac{1}{2} (A+B);$
	remaining	$\cos \frac{1}{2} C \sin \frac{1}{2} (a - b) = \sin \frac{1}{2} c \sin \frac{1}{2} (A - B);$
	parts.	$\cos \frac{1}{2} C \cos \frac{1}{2} (a-b) = \cos \frac{1}{2} c \sin \frac{1}{2} (A+B).$
A, B, α, two angles	b, c, C, all the	$\sin b = \frac{\sin a \sin B}{\sin A}  \text{(two values of } b\text{);}$
and an opposite	remaining parts.	$\tan \frac{1}{2}c = \frac{\cos \frac{1}{2}(A+B)\tan \frac{1}{2}(a+b)}{\cos \frac{1}{2}(A-B)};$
side.		$\tan \frac{1}{2} C = \frac{\cos \frac{1}{2} (a - b) \cot \frac{1}{2} (A + B)}{\cos \frac{1}{2} (a + b)}.$
$\overline{A, B, C}$	$\overline{a, b, c}$	$S = \frac{1}{2} \left( A + B + C \right);$
the three	the three	$-\cos S$
angles.	sides.	$P = \sqrt{\frac{-\cos S}{\cos (S-A)\cos (S-B)\cos (S-C)}};$
		$\tan \frac{1}{2}a = P\cos (S - A);$
		$\tan \frac{1}{2}b = P\cos (S-B);$
		$\tan \frac{1}{2} c = P \cos (S - C).$





## TABLE I.

# COMMON LOGARITHMS OF NUMBERS.

N.	Log.	N.	Log.	N.	Log.	N.	Log.	N.	Log.
0	— Infinity.	80	1.47 712	60	1.77 815	90	1.95 424	120	2.07 918
1	0.00 000	31	1.49 136	61	1.78 533	91	1.95 904	121	2.08 279
2	0.30 103	32	1.50 51 <del>5</del>	62	1.79 239	92	1.96 379	122	2.08 636
3	0.47 712	33	1.51 851	63	1.79 934	93	1.96 848	123	2.08 991
4	o.60 206	34	1.53 148	64	1.80 618	94	1.97 313	124	2.09 342
5	o.69 897	35	1.54 407	65	1.81 291	95	1.97 772	125	2.09 691
6	o.77 815	36	1.55 630	66	1.81 954	96	1.98 227	126	2.10 037
7	0.84 510	37	1.56 820	67	1.82 607	97	1.98 677	127	2.10 380
8	0.90 309	38	1.57 978	68	1.83 251	98	1.99 123	128	2.10 721
9	0.95 424	39	1.59 106	69	1.83 885	99	1.99 564	129	2.11 059
10	1.00 000	40	1.60 206	70	1.84 510	100	2.00 000	180	2.11 394
11	1.04 139	41	1.61 278	71	1.85 126	101	2.00 432	131	2.11 727
12	1.07 918	42	1.62 325	72	1.85 733	102	2.00 860	132	2.12 057
13	1.11 394	43	1.63 347	73	1.86 332	103	2.01 284	133	2.12 385
14	1.14 613	44	1.64 345	74	1.86 923	104	2.01 703	134	2.12 710
15	1.17 609	45	1.65 321	75	1.87 506	105	2.02 119	135	2.13 033
16	1.20 412	46	1.66 276	76	1.88 081	106	2.02 531	136	2.13 354
17	1.23 045	47	1.67 210	77	1.88 649	107	2.02 938	137	2.13 672
18	1.25 527	48	1.68 124	78	1.89 209	108	2.03 342	138	2.13 988
19	1.27 875	49	1.69 020	79	1.89 763	109	2.03 743	139	2.14 301
20	1.30 103	50	1.69 897	80	1.90 309	110	2.04 139	140	2.14 613
21	1.32 222	51	1.70 757	81	1,90 849	111	2.04 532	141	2.14 922
22	1.34 242	52	1.71 600	82	1,91 381	112	2.04 922	142	2.15 229
23	1.36 173	53	1.72 428	83	1,91 908	113	2.05 308	143	2.15 534
24	1.38 021	54	I.73 239	84	1.92 428	114	2.05 690	144	2.15 836
25	1.39 794	55	I.74 036	85	1.92 942	115	2.06 070	145	2.16 137
26	1.41 497	56	r.74 819	86	1.93 450	116	2.06 446	146	2.16 435
27	1.43 136	57	1.75 587	87	I .93 952	117	2.06 819	147	2.16 732
28	1.44 716	58	1 76 343	88	I .94 448	118	2.07 188	148	2.17 026
29	1.46 240	59	1.77 085	89	I .94 939	119	2.07 555	149	2.17 319
80	1.47 712	60	1.77 815	90	1.95 424	120	2.07 918	150	2.17 609

N.		0	1	2	8	4	5	6	7	8	9	Prop. Pts.
100	00	<b>000</b> 0	043	087	130	173	217	260	303	346	389	
01		432	475	518	561	604	647	689	732	775	817	į
02		860	903	945	988	*030	*072	*113	*157	*199	*242	44   43   42
03	OI	284	326	368	410	452	494	536	578	620	662	2 4.4 4 3 4 2
04		703	745	787	828	870	912	953	993	+036	*078	2 8 8 8 6 8 4
05	02	119	160	202	243	284	325	366	407	449	490	3 23.2 22 9 12 6
06		531	572	612	653	694	735	776	816	857	898	4 17.6 17 2 16 8
07				١.	*060			*181			-	5 22 0 21 5 21 0
08	-	938	979	*019		*100	*141		*222	*262 663	*302	6 26 4 25 8 25.2
09	03	342	383 782	423 822	463 862	503 902	543	583 981	623 *021	<b>*</b> 060	703 *100	7 30 8 30.1 29 4
		743	<u>-</u>				941		l <del></del> -			8 35.2 34 4 33.6 9 39.6 38 7 37.8
110	04_	139	179	218	258	297	336	376	415	454	493	9.39.0130 7137.0
11		532	571	610	650	689	727	766	805	844	883	
12		922	961	999	<b>*0</b> 38	*077	<b>*</b> 115	*154	*192	*231	*269	41 40 39
13	05	308	346	385	423	461	500	538	576	614	652	1 4 1 4.0 39
14		690	729	767	8o <del>5</del>	843	881	918	956	994	*032	2828078
15	06	070	108	145	183	221	258	296	333	371	408	3 12 3 12 0 11 7
16		446	483	521	558	595	633	670	707	744	781	4 16 4 16 0 15 6
17	ı	819	856	893		967	*004	*041	*078	*115		5 20 5 20 0 19 5 6 24 6 24 0 23.4
18	07	188	225	262	930	335	372	408		- 482	*151 518	7 28 7 28 0 27 3
19	٥,	555	591	628	664	700	737	773	445 809	846	882	8 32 .8 32.0 31.2
120	-					*063						9 36.9 36.0 35.1
		918	954	990	*027	1003	*099	*135	*171	*207	*243	
21		279	314	350	386	422	458	493	529	565	600	1 38   37   36
22		636	672	707	743	778	814	849	884	920	955	1 1 1 1 si
23		991	*026	*061	<b>*0</b> 96	*132	*167	*202	*237	*272	*307	3.8 3.7 3.6
24	09	342	377	412	447	482	517	552	587	621	656	3 11.4 11.1 30.8
25	_	691	726	76ò	795	830	864	899	934	968	*003	3 11.4 11.1 10.8 4 15.2 14 8 14.4
26	10	037	072	106	140	175	209	243	278	312	346	519.018.518.0
27		38o	413	449	483	517	551	585	619	653	687	C 22.8 22.2 21.6
28		721	755	789	823	857	890	924	958	992	*025	7 26.6 25 9 25.2
29	11	059	093	126	160	193	227	261	294	327	361	8 30 4 29 6 28.8
130	-		428	461		528	561	<del></del>	628	661		9 34-2 33-3 32-4
	-	394		ļ	494			594			694	<b>✓</b>
31 32		727	760	793	826	860	893	926	959	992	*024	35   34   33
33	12	O57	090	123	156	189	222	254	287	320	352	1 3.5 3 4 3.3
		385	418	450		516	548	581	613	646	678	2 7.0 6.8 6.6
34		710	743	775	808	840	872	905	937	969	*00I	3 10.5 10 2 9.9
35	-13	033	066	098	130	162	194	226	258	290	322	4 14 0 13.6 13.2
36.		354	386	418	450	481	513	545	577	609	640	5 17 5 17 0 10 5
37		672	704	735	767	799	830	862	893	925	956	621 0 20.4 19.8
38		988	*019	*05 I	*082	*114	*145	*176	*208	*239	*270	7 24 5 23 8 23.1
<b>39</b>	14	301	333	364	395	426	457	489	520	551	582	8 28.0 27.2 26.4 9 31.5 30.6 2g.75
140	_	613	644	675	706	737	768	799	829	860	891	A 97 - 2130 Tollail - A
41	· -	922		983	*014	*045	*076	*106	*137	*168	*198	
42	15	229	953 259	290	320	351	381	412	442	473	503	32 31
43	5	534	564	594	625	$65\overline{5}$	685	715	746	776	806	3.2 3.1 3.0
			866	l l					1	1	1	2 6.4 6.2 6.0
44	16	836		897	927	957	987	*017	*047	*077	*107	3 9 6 9 3 9 0
45 46		137	167 465	197	227	256	286	316	346	376	406	4 12.8 12.4 10.00
		435	-	495	524	554	584	613	643	673	702	5 16.0 15.5 15.0 6 19 2 18.6 18.0
47.	,	732	761	791	820	850	879	909	938	967	997	7 22 4 21 2 23 0
48	17	026	056	085	114	143	173	202	231	260	289	8 25 6 24 8 24.0
49	_	319	348	377	406	435	464	493	522	551	580	9 28 8 27 9 27 0
150		609	638	667	696	725	754	782	811	840	869	
N.		0	1	2	3	4	5	6	7	8	•	Prop. Pts.

	. N.		0	1	2	8	4	5	6	7	8	9	Prop. Pts.
I	150	17	609	638	667	696	725	754	782	811	840	869	
I	51		898	926	955	984	*013	*041	*070	*099	*127	*156	29   28
ı	52	18	184	213	241	270	298	327	355	384	412	441	1 2.9 2.8
ı	53		469	498	526	554	583	611	639	667	696	724	2 5.8 5.6
H	54 55		752	780 061	808	837	863	893	921 201	949	977	*005 285	3 8.7 8.4
ı	56	14	033 312	340	368	396	145 424	173 451	479	507	25 <u>7</u> 535	562	4 11.6 11.2 5 14.5 14.0
	57		590	618	645	673	700	728	756	783	811	838	6 17.4 16.8
	58		866	893	921	948	976	+003	*030	<b>*</b> 058	*085	*112	7 20.3 19.6
H	59	20	140	167	194	222	249	276	303	330	358	383	8 23.2 22.4 9 26.1 25.2
	160		412	439	466	493	520	548	573	602	629	656	0 20.1 20.2
	61		683	710	737	763	792	817	844	871	898	923	27   26
ı	62	21	952	978	*005	<b>*</b> 032	₹059	*085	*112 378	*139 405	*165	*192 458	1 2.7 2.6
H	63		-	245	272	299	325	352		1	431	1	2 5.4 5.2
	64 65		484 748	775	537 801	564 827	590 854	617 880	643 906	669 932	958	722 985	3 8.1 7.8 4 10.8 10.4
	66	22	011	037	063	089	115	141	167	194	220	246	5 13.5 13.0
	67		272	298	324	350	376	401	427	453	479	505	6 16.2 15.6
	68	l	531	557	583	608	634	660	686	712	737	763	$7   18.9   18.2 \\ 8   21.6   20.8 $
Ħ	69	١.	789	814	840	866	891	917	943	968	994	*019	9 24.3 23.4
H	170	23	043	070	096	121	147	172	198	223	249	274	1
I	71		300	325	350	376	401	426	452	477	502	528	25
ı	72 73		55 <u>3</u> 805	578 830	60 <u>3</u> 85 <u>5</u>	629 880	905	679 930	70 <u>4</u> 955	729 980	75 <u>4</u> *005	779 *030	1 2.5
i		۱		- 1		l		180	1	t i	1	_	2 5.0 3 7.5
I	74 75	24	05 <u>5</u> 304	080 329	10 <u>5</u> 353	130 378	15 <del>5</del> 403	428	204 452	229 477	254 502	279 527	4 10.0
I	76		551	576	601	625	650	674	699	724	748	773	5 12.5
ì	77	ŀ	797	822	846	871,	895	920	944	969	993	*o18	6 15.0 7 17.5
ı	78	25	042	066	100	115	139	164	188	212	237	261	8 20.0
H	79		285	310	334	358	382	406	431	455	479	503	9 22.5
ł	180		527	551	575	600	624	648	672	696	720	744	124   28
I	81	~6	768 007	792	816	840	864	888 126	912	935	959 198	983 221	
I	82 83	20	245	031 269	055 253	979 316	102 340	364	387	174 411	435	458	1 2.4 2.3 2 4.8 4.6
I	84		482	505	529		576	600	623	647	670	694	3 7.2 6.9
۲	85		717.	741	764	553 788	811	834	858	188	905	928	4 9.6 9.2
	85 88	2	126	975.	998	*021	*045	<b>*</b> 068	*091	<sup>*</sup> 114	*138	*161	5 12.0 11.5 6 14.4 13.8
	818	27	184	207	231.	254	277	300	323	346	370	393	7 16.8 16.1
			416.	439	462	485	508	531 761	554 784	577 807	600 830	623 852	8 19.2 18.4
			646	669	692	715	738	989	*012	*035	*058	*081	9 21.6 20.7
	***	28	475	898	921	944	967		240	262	285	307	22   21
	4		103; 330	126 353	149 375	308	194 421	217 443	466	488	511	533	1 2.2 2.1
		7	556	578,	601	623	646	668	691	713	735	758	2 4.4 4.2
			780	803:	827	847	870	892	914	937	959 181	981	3 6.6 6.3 4 8.8 8.4
	95	29	003	026	048	. 070	092	115	137	159		203	5 11.0 10.5
	96	1	226	248	270.	292	314	336	358	.380	403	425	6 13.2 12.6
I	97	1	447 667	469 688	491	513	535	557	579 798	601 820	623	64 <del>5</del> 863	7 15.4 14.7 8 17.6 16.8
F	98 90		885	907	710 929	732 951	754 973	776 994	*016		842 *060	*081	9 19.8 18.9
	200	-	103	125	146	168	190	211	233	255	276	298	
ł	N.		. 0	1	2	. 9.	4	5	6	7	8	9	Prop. Pts.
Ł						4_							

N.	0	1	9	3	4	5	6	7	8	9	Prop. Pts.
200	30 103	123	146	168	190	211	233	253	276	298	
01	320	341	363	384	406	428	449	471	492	514	22   21
02 03	5 <u>3</u> 5 750	557 771	578 792	600 814	621 835	643 856	664 878	685 899	707 920	728 942	1 2.2 2.1
04	963	984	*006	*027	<b>*</b> 048	*069	<b>*0</b> 91	*112	*133	*154	2 4.4 4.2 3 6.6 6.3
05	31 175	197	218	239	260	281	302	323	345	366	4 8.8 8.4
06	387	408	429	450	.471	492	513	534	555	576	5 11.0 10.5
07 08	<b>5</b> 97 <b>80</b> 6	618 827	639 848	660 869	681 890	702	723 931	744 952	76 <del>5</del> 973	785 994	6 13.2 12.6 7 15.4 14.7
09	32 013	035	056	077	098	118	139	160	181	201	8 17.6 16.8
210	222	243	263	284	303	325	346	366	387	408	9 19.8 18.9
11	428	449	469	490	510	531.	552	. 572	593	613	20
12 13	634 838	654 858	67 <del>5</del> 879	69 <u>5</u> 899	715	736 940	756 960	980	797 * <b>0</b> 01	818 *021	1 2.0
14	33 041	062	082	102	122	143	163	183	203	224	2 4.0 3 6.0
15	244	264	284	304	325	345	363	385	405	425	4 8.0
16	445	465	486	506	526	546	566	586	606	626	5 10.0 6 12.0
17 18	646 846	666 866	686 885	706 905	726 925	746 945	766 965	786 985	806 *00₹	826 *025	7 14.0
19	34 044	064	084	104	124	143	163	183	203	223	8 16.0 9 18.0
220	242	262	282	301	321	341	361	380	400	420	'
21	439	459	479	498	518	537	557	577	596	616	19-
22 23	635 830	655 850	674 869	694 889	713 908	733 928	753 947	772 967	792 986	*005	$\begin{array}{c cccc} 1 & 1.9 \\ 2 & 3.8 \end{array}$
24	35 025	044	064	083	102	122	141	160	180	199	3 5.7
25	218	238	257	276	295	313	334	353	372	392	4 7.6 5 9.5
26	411	430	449	468	488	507	526	545	564	583	$\begin{array}{c c} 5 & 9.5 \\ 6 & 11.4 \end{array}$
27 28	603 793	622 813	832	660 851	679 870	698 889	908	736	755 946	774 965	7 13.3
29	984	*003	*021	*040	*059	*078	*097	*116	*135	*154	8 15.2 9 17.1
230	<b>3</b> 6 173	192	211	229	248	267	286	303	324	342	1
31	361	380 568	399 586	418	436	455	474	493	511	530	18
32 33	549 736	754	773	603 791	810	642 829	661 847	680 866	698 884	903	1 1.8 2 3.6
34	922	940	959	977	996	*014	*033	*051	*070	*o88	3 5.4
35	37 107	125	144	162	181	199	218	236	254	273	4 7.2 5 9.0
36	291	310	328.	1	365	383	401	420	438	457	6 10.8
i 37 38	473 658	493 676	511 694	530 712	548 731	566 749	58 <del>5</del>	785	621 803	639 822	7 12.6 8 14.4
39	840	858	876	894	912	93í	949	967	985	*003	9 16.2
240	38 021.	039	057	075	093	112	130	148	166	184	17
41 42	202 382	399.	238 417	256	274	292 471	310 480	328 507	346 527	364	1 1.7
43	561	578	596	435 614	453 632	650	668	686	525 703	543 721	2 3.4
43 44 45 46	739	757	773	792	810	828	846	863	188	899	3 5.1 4 6.8
45	917	934	952 129	970	987 164	*005 182	*023	*041	*058	*076	5 8.5
46	39 094 270	287	i	146		i i	199	217	235	252	6 10.2 7 11.9
47 48	445	463	30 <u>5</u> 480	322 498	340 515	358 533	375 550	393 568	585	428 602	8 13.6
49	620	637	653	672	690	707	724	742	759	777	9 15.3
250	794	811	829	846	863	881	898	915	933	950	
N.	0	1	2	3	4	5	6	7	8.	9	Prop. Pts.

N.	0	1	2	8	4	5	6	7	8	9	Prop. Pts.
250	39 794	811	829	846	863	881	898	915	933	950	
51	967	985	*002	*019	*037	*054	*07 I	*o88	*106	*123	18
52	40 140		175	192	209	226	243	261	278	295	1 1.8
53	312	329	346	364	381	398	415	432	449	466	2 3.6
. 54	483	500	518	533	552	569	586	603	620	637	3 5.4
55 56	654 824	671	688	70 <u>5</u> 875	722 892	739	756 926	773	790 960	807 976	4 7.2
1		ł			1 - 1	909		943	1		5 9.0 6 10.8
57 58	993 41 162	*010	*027	*044 212	*061 229	*078 246	*095 263	*111 280	*128 296	*145 313	7 12.6
59	41 162 330	179 347	196 363	380	397	414	430	447	464	481	8 14.4
260	497	514	531	547	564	581	597	614	631	647	9 16.2
61	664	681	697	714	731	747	764	780	797	814	17
62	830		863	880	896	913	929	946	963	979	l   '
63	996	*012	*029	*045	*062	*078	*09 <del>5</del>	*111	*127	*144	$\begin{array}{c c} 1 & 1.7 \\ 2 & 3.4 \end{array}$
64	42 160	177	193	210	226	243	259	275	292	308	3 5.1
65	325	341	357	374	390	406	423	439	455	472	4 6.8
66	488	504	521	537	553	570	586	602	619	635	5 8.5
67	651	667	684	700	716	732	749	763	781	797	6 10.2 7 11.9
68 69	813		846 *008	862 *024	878 <b>*</b> 040	894 <b>*0</b> 56	911 *072	927 *088	943 *104	959 *120	8 13.6
11	975	991	1				<u> </u>	<u> </u>		281	9 15.3
270	43 136		169	183	201	217	233	249	263		. 10
71 72	297	313	329 489	345	361 521	377	393	409 569	423 584	441 600	16
73	457 616	473 632	648	505 664	680	537 696	553 712	727	743	759	1 1.6
74		1	807	823	838	854	870	886	902	917	2 3.2 3 4.8
75	<b>7</b> 75 933	791 949	965	981	996	*012	*028	*044	*059	*075	4 6.4
76	44 <b>0</b> 91	107	122	138	154	170	185	201	217	232	5 8.0
77	248	264	279	295	311	326	342	358	373	389	6 9.6
78	404	420	436	451	467	483	498	514	529	545	7 11.2 8 12.8
79	<b>5</b> 60	576	592	607	623	638	654	669	683	700	9 14.4
280	716	731	747	762	778	793	809	824	840	855	
81	871	886	902	917	932	948	963	979	994	*010	15
82	45 025	040	056	071	086	102	117	133	148	163	1 1.5
83	179	194	209	225	240	255	271	286	301	317	2 3.0 3 4.5
84	332	347	362	378	393	408	423	439	454	469	4 6.0
85 86	484 637	652	667	530 682	545 697	561 712	728	743	758	773	5 7.5
87		1 -	1			864	1 -	_	)		6 9.0
88	788 939	803 954	969	834 984	849 *000	*015	879 * <b>03</b> 0	894 *045	909 *060	924 *075	7 10.5 8 12.0
89	46 090	105	120	135	150	165	180	195	210	225	9 13.5
290	240	-	270	285	300	315	330	345	359	374	i i
91	389		419	434	449	464	479	494	509	523	14
92	538	553	568	583	598	613	627	642	657	672	1 1.4 •
93	687	702	.716	731	.746	761	776	790	805	820	2 2.8
94	835	850	864	879	894	909	923	938	953	967	3 4.2 4 5.6
.95	982		*012	*026		<b>*05</b> 6	*070	*085	*100	*114	5 7.0
96	47 129	1	159	173	188	202	217	232	246	261	6 8.4
97	276		303	319	334	349	363	378	392	407	7 9.8
98 99	422 567	436 582	451 596	465	480 625	494 640	509 654	524 669	538 683	553 698	8 11.2 9 12.6
800	712	727	741	756	770	784	799	813	828	842	
N.	0	1	2	3	4	5	6	7	8	9	Prop. Pts.

Prop. Pts.

N.

N.		0	1	.2	. 3	-4	5	6	7	8	9	Prop. Pts.
850	54	497	419	432	444	456	469	481	494	506	518	
51		531	543	555	568	580	593	603	617	630	642	
52 53	Ì	654 777	667 790	679 802	814	704 827	716 839	728 851	741 864	753 876	765 888	18
54		900	913	925	937	949	962	974	986	998	*011	1 1.3
55	55	023	035	047	060	072	084	096	108	121	133	2 2.6
56		143	157	169	182	194	206	218	230	242	255	3 3.9 4 5.2
57 58		267 388	279 400	291 413	30 <u>3</u>	315 437	328 449	340 461	352 473	364 485	376 497	5 6.5
59	١.	509	522	534	546	558	570	582	594	606	618	6 7.8 7 9.1
860	١.	630	642	654	666	678	691	703	713	727	739	8 10.4
61 62		751 871	763 883	77 <u>5</u> 89 <u>5</u>	787	799	931	823 943	83 <u>5</u> 955	847 967	859 979	9 11.7
63		991	* <b>003</b>	*015	*027	<b>*</b> 038	<b>*</b> 050	*062	*074	<b>*086</b>	* <del>0</del> 98	
64	56	110	122	134	146	158	170	182	194	205	217	1.40
65 66		229 348	241 360	253 372	26 <del>5</del>	277 396	289 407	30I 419	312 431	324 443	336 453	12
67		467	478	490	502	514	526	538	549	561	573	1 1.2 2 2.4
68		583	597	608	620	632	644	656	667	679	691	3 3.6
69		703	714	726	738	750	761	773	785	797	808	4 4.8 5 6.0
870 71		820	832	844 961	855	867 984	879	891 *008	902 *019	914 *031	926 *043	6 7.2
72	57	937 054	949 <b>o</b> 66	078	972 989	101	996 113	124	136	148	159	7 8.4 8 9.6
73		171	183	194	206	217	229	241	252	264	276	9 10.8
74 75		287 403	299	310	322	334	345	357	368 484	380	392	
76		519	530	426 542	438 553	44 <u>9</u> 565	461 576	473 588	600	496 611	507 623	
77		634	646	657	669	680	692	703	713	726	738	11
78 79		749 864	761	772 887	784 898	. 795	807	818	830	841	852 967	11.1
880	-	978	990	*001	*013	910 *024	921 *035	933 *047	944 *058	955 *070	*081	$\begin{array}{c c} 2 & 2 & 2 \\ 3 & 3 & 3 \end{array}$
81	58		104	115	127	138	149	161	172	184	195	44.4
82		206	218	229	240	252	263	274	286	297	309	5 5.5 6 6.6
83		320	331	343	354	365	377	388	399	410	422	77.7
84 85		433 546	444 557	456 569	467 580	478 591	490 602	501 614	512 625	524 636	53 <del>5</del>	88.8 99.9
86		659	670	68í	692	704	713	726	737	749	760	•
87 88		771	782	794	803	816	827	838	850	168	872	
89		88 <u>3</u>	894 *006	906 *017	917 <b>*02</b> 8	928 <b>*</b> 040	939 *051	950 *062	961 *073	973 <b>*</b> 084	984 *095	10
79 880 81 82 83 84 85 86 87 88 89 91	59	106	118	129	140	151	162	173	184	195	207	11.0
91		218	229	240	251	262	273	284	295	306	318	$\begin{array}{c c} 2 & 2 & 0 \\ 3 & 3 & 0 \end{array}$
		329 439	340 450	351 461	362 472	373 483	384 494	395 506	406 517	417 528	428 539	44.0
94		550	561		583	594	603	616	627.	638	649	5 5.0 6 6.0
95		wo	671	572 682	693	704	713	726	737 846	748	759 868	77.0
96		770	780	791	802	813	824	835		857		88.0 99.0
97 98		879 988	890 999	90I *0IO	912 *021	923 *032	934 *043	94 <u>5</u> *054	956 *065	966 *076	977 *o86	9,5,5
99	60	097	108	119	130	141	152	163	173	184	195	
400		206	217	228	239	249	260	271	282	293	304	`.*
93 94 95 96 97 98 99 400 N.		0	. 1	2	3	4	5	6	7	8	9	Prop. Pts.

N.		•	1	9	3	4	5	6	7	8	9	Prop. Pts.
400	60	206	217	228	239	249	260	27 I	282	293	304	
01	•	314	325	336	347	358	369	379	390	401	412	
02		423	433	444	455	466	477	487	498 606	509 617	520	
03		531	541	552	563	574	584	595			627	
04 05		638 746	649 756	660 767	670 778	681 788	692 799	703 810	713 821	724 83.1	735 842	
06		853	863	874	883	895	906	917	927	938	949	11
07		959	970	981	991	<b>*</b> 002	<b>*</b> 013	<b>*</b> 023	*034	<b>*</b> 045	<b>*</b> 055	11.1
08	61	<b>o</b> 66	077	087	098	109	119	130	140	151	162	2 2.2 3 3.3
09	-	278	183	194	204	213	225	236	247	257	268	44.4
410	-	384		300	416	32I 426	331	342 448	352 458	363 469	374	5 5.5 6 6.6
11 12		490	395 500	405 511	521	532	437 542	553	563	574	479 584	77.7
13		595	<b>60</b> 6	616	627	637	648	658	669	679	690	8 8.8
14		700	711	721	731	742	752	763	773 878	784	794	9 9.9
15 16		803	920	826	836	847	857 962	868	982	888	899 *003	
1	60	909	-	930	941	951	066	972 076	086	993	107	
17 18	02	118	024 128	034 138	045 149	055	170	180	190	097 201	211	
19		22 I	232	242	252	263	273	284	294	304	313	
420	١.	325	335	346	356	366	377	387	397	408	418	
21		428	439	449	459	469	480	490	500	511	521	10
22 23		531 634	542 644	552 653	562 663	<b>572</b> 675	583 685	593 696	706	613	624 726	1 1.0 2 2.0
24		737	747	757	767	778	788	798	808	818	829	3 3.0
25		839	849	859	870	880	890	900	910	921	931	44.0 55.0
26		941	951	961	972	982	992	*002	*012	*022	*033	66.0
27	63	043	053	063	073	083	094	104	114	124	134	77.0
28 29		144 246	155 256	165 266	175 276	18 <del>5</del> 286	195 296	205 306	215 317	225 327	236 337	8 8.0 9 9.0
480	-	347	357	367	377	387	397	407	417	428	438	ا
31	-	448	458	468	478	488	498	508	518	528	538	
32	ŀ	548	558	568	579	589	599	609	619	629	639	·
33	l	649	659	669	679	689	699	709	719	729	739	
34 35		749 849	759 859	769 869	779 879	789 889	799 899	809 909	819 919	829 929	939	
36		949	959	969	979	988	998	*008	*018	*028	+038	19
37	64	048	058	o68	078	088	098	108	811	128	137	10.9
38		147	157	167	177	187	197	207	217	227	237	21.8
39	-	246	256	266	276	286	296	306	316	326	335	3 2.7 4 3.6
440		345	355	365 464	375	38 <del>5</del> 483	395	503	513	523	532	54.5
41 42		444 542	454 552	562	473 572	582	493 591	601	611	621	631	65.4 76.3
43		640	650	660	670	680	689	699	709	740		87.2 98.1
44		738	748	758	768	777	787	797	807	816	820	9 8.1
45 46		836 933	846 943	856 953	865 963	875 972	88 <del>5</del> 982	89 <del>5</del> 992	904 *002	914 *011	924 *021	-
47	6r	031	040	050	060	070	079	089	099	108	118	
48	٠,	128	137	147	157	167	176	186	196	205	215	
49		225	234	244	254	263	273	283	292	302	312	
450		321	331	341	350	360	369	379	389	398	408	
N.		•	1	2	3	4	5	6	7	8	9	Prop. Pts.

N.	0	1	2	3	4	5	6	7	8	9	Prop. Pts.
450	65_321	331	341	350	360	369	379	389	398	408	
51	418	427	437	447	456	466	475	485	495	504	
52 53	514 610	523	533	543	552 648	562 658	571 667	581 677	591 686	600	
54	706	715	629 723	639	744	753	763	772	782	702	
55	108	811	820	830	839	849	858	868	877	887	110
56	· 896	906	9#5	925	935	944	954	963	973	982	10
57	992	*001	*011	*020	*030	*039	*049	<b>*</b> 058	*068	*077	$\begin{array}{c c} 1 & 1 & 0 \\ 2 & 2 & 0 \end{array}$
58 59	66 087 181	096 191	106	210	124 219	134 229	143 238	153 247	162 257	172 266	3 3.0
460	276	285	295	304	314	323	332	342	351	361	4 4.0 5 5.0
61	370	380	389	398	408	417	427	436	415	453	66.0
62	464	474	483	492	502	511	521	530	539	549	7 7.0
63.	558	567	577	586	596	603	614	624	633	642	8 8.0 9 9.0
64	652	661	671	680	689	699	708	717	727	736	9,0,0
65 66	745 839	75 <u>5</u> 848	764 857	773 867	783 876	792 885	801	904	820	829 922	·
67				1		_	1	1 - 1	*006	-	ł
68	932 67 025	941 934	950 043	960 052	969	978	987 080	997 <b>0</b> 89	099	*015 108	
69	117	127	136	145	154	164	173	182	191	201	
470	210	219	228	237	247	256	265	274	284	293	19
71	302	311	321	330	339	348	357	367	376	385	
72	394	403	413	422	431	440	449	459	468	477	$ \begin{array}{c c} 1 & 0.9 \\ 2 & 1.8 \end{array} $
73	486	495	504	514	523	532	541	550	560	569	$\frac{2}{3}$ 2.7
· 74	<b>578</b> 669	587	596 688	605	614	624	633	642	651	660	43.6
76	761	679 770	779	788	706	715 806	815	73 <u>3</u> 82 <u>5</u>	742 834	752 843	$   \begin{array}{c}     54.5 \\     65.4   \end{array} $
77	852	861	870	879	888	897	906	916	925	934	76.3
78	943	952	961	970	979	988	997	*006	*015	*024	8 7.2
79	68 034	043	052	061	070	079	088	097	106	115	9 8.1
480	124	133	142	151	160	169	178	187	196	205	
81	215	224	233	242	251	260	269	278	287	296	
82 83	30 <u>5</u> 395	314	323 413	332	34I 43I	3 <u>5</u> 0 440	359 449	368 458	377 467	386 476	
84	485	494	502	511	520	529	538	1	556	565	1
85	574	583	592	601	610	619	628	547 637	646	655	ŀ
86	664	673	681	690	699	70 <b>8</b>	717	726	735	744	8
87.	753	762	771	780	789	797	806	815	824	833	1 0.8
88	842	851	860	869	878	886	895	904	913	922	21.6
87 88 89 <b>490</b>	931 69 020	940	949	958	966	975 064	984	993 082	*002	*011	$   \begin{array}{c c}     3 & 2.4 \\     4 & 3.2   \end{array} $
	108		037	046	055		073		090	188	54.0
91 92	197	205	126	135	144 232	152 241	161 249	170 258	179 267	276	$\begin{array}{c} 6 & 4.8 \\ 7 & 5.6 \end{array}$
93	285	294	302	311	320	329	338	346	355	364	8 6.4
94	373	381	390	399	408	417	425	434	443	452	9 7.2
95	461	469	478	487	496	504	513	522	531	539	
96	548	557	566	574	583	592	601	609	618	627	l
97	636	644	653	662	671	679	688	697	705	714 801	
98 99	723 810	732 819	740 827	749 836	758 84 <del>5</del>	767 854	775 862	784 871	793 880	888	1
500	897	906	914	923	932	940	949	958	966	975	·
Ņ,	0	1	2	3	4	5	6	7	.8	9 :	Prop. Pts.

N.	==	0	1	2	3	4	5	6	7	8	9	Prop. Pts.
500	60	897	906	914	923	932	940	949	958	966	975	
01	- ,_	984	992	*001	*010	*018	<b>*</b> 027	*036	*044	*053	*062	
02 03	70	070	079 165	088 174	096 183	10 <u>5</u>	114 200	122	131	140 226	148	
04		157 243	252	260	269	278	286	295	<b>2</b> 17	312	234 321	
05		329	338	346	355	364	372	381	389	398	406	
06		415	424	432	441	449	458	467	475	484	492	10.9
07 08		501 586	50 <u>9</u>	518 603	526 612	535 621	544 629	552 638	561 646	569 655	578 663	2 1.8
09		672	595 680	689	697	706	714	723	731	740	749	3 2.7 4 3.6
510	-	757	766	774	783	791	800	808	817	825	834	5 4.5
11 12		842 927	851 935	859 944	868 952	876 961	88 <del>5</del> 969	893 978	902 986	910	919 *003	6 5.4 7 6.3
13	71	012	020	029	037	<b>ó</b> 46	054	<b>ó</b> 63	071	<b>6</b> 79	<b>088</b>	87.2
14 15		181	10 <u>5</u> 189	113	122 206	130	139	147	155	164	172	9 8.1
16		265	273	282	290	214 299	223 307	231 315	240 324	248 332	257 341	
17		349	357	366	374	383	391	399 483	408	416	425	
18 19		433 517	441 525	4 <u>5</u> 0	458 542	466 550	475 559	483 567	492 575	500 584	508 592	
520	-	600	609	617	625	634	642	650	659	667	675	
21	-	684	692	700	709	717	725	734	742	750	759	8
22 23		767 850	775 858	784 867	792 875	800 883	809 892	817	825 908	834	842 925	1 0.8 2 1.6
24		933	941	930	958	966	973	983	991	999	*oo8	32.4
25	72	016	024	032	041	049	057	066	074	082	090	43.2 54.0
26		099	107	115	123	132	140	148	156	163	173	6 4.8 7 5.6
27 28		181 263	189 272	198 280	206 288	214	222 304	230 313	239 321	247 329	255 337	86.4
29		346	354	362	370	378	387	395	403	411	419	9 7.2
580	-	428	436	444	452	460	469	477	485	493	501	
31 32		509 591	518 599	526 607	534 616	542 624	550 632	558 640	567 648	575 656	58 <u>3</u>	
33		673	599 681	689	697	705	713	722	730	738	746	}
34 35		754 835	762 843	770 852	779 860	787 868	795 876	803 884	811	819	827 908	
36		916	925	933	941	949	957	965	973	981	989	17
37		997	*006	*014	*022	*030	<b>*</b> 038	*046	*054	*062	*070	10.7
38 39	73	078 159	086	175	183	111	119	207	215	143	151 231	2 1.4 3 2.1
540	١ .	239	247	255	.263	272	280	288	296	304	312	4 2.8 5 3.5
41	•	320	328	336	344	352	360	368	376	384	392	64.2
42 43	ŀ	400 480	408 488	416	424 504	432 512	440 520	448 528	456 536	464 544	472 552	7 4.9 8 5.6
44		560	568	576	584	592	600	608	616	624	632	963
45	ļ	640	648	656	664	672	679	687	695	703	711	
46		719	727	735	743 823	751 830	759 838	767 846	775	783 862	791 870	
47 48		799 878	807 886	894	902	910	918	926	933	941	949	
49	. ا	957	965	973	981	989	997	*005	*013	*020	*028	
550	74	036	044	Ò52	060	068	076	084	092	099	107	
N.	<u> </u>	0	1	9	3	4	5	6	7	8	9	Prop. Pts.

N.	0	1	2	3	4	5	6	7	8	.9	Prop. Pts.
550	74 036	044	052	060	068	076	084	092	099	107	
51	115	123	131	139	147	153	162	170	178	186	
52 53	194 273	202 280	288	218 296	225 304	233 312	241 320	249 327	257 335	26 <del>5</del> 343	·
54	351	359	367	374	382	390	398	406	414	421	
55	429	437	445	453	461	468	476	484	492	300	
56	507 586	515	523	531	539	547	554	562	570	578	
57 58	663	593 671	601 679	609 687	617 695	624 702	632 710	640 718	648 726	656 733	
59	741	749	757	764	772	780	788	796	803	811	
560	819	827	834	842	850	858	865	873	188	889	18
61 62	896 974	904 981	912 989	920 997	927 <b>*0</b> 05	93 <del>3</del> *012	943 *020	950 *028	958 *035	966 *043	1 0.8
63	75 OSI	059	<b>o</b> 66	991	082	089	097	105	113	120	2 1.6
64	128	136	143	151	159	166	174	182	189	197	3 2.4 4 3.2
65 66	20 <u>5</u> 282	213 289	220 297	228 305	236	243 320	251 328	259	266	274	54.0
67	358	366	374	381	312	397	404	335 412	343 420	351 427	64.8 75.6
68	435	442	450	458	465	473	481	488	496	504	8 6.4
69	511	519	526	534	542	549	557	565	572	580	9 7.2
570	587 664	595	603	686	618	626	633	641	648	656	
71 72	740	67 I 747	67 <u>9</u> 755	762	694 770	702 778	709 785	717	724 800	732 808	
73	815	823	831	838	846	853	86ī	793 868	876	884	Ï
74	891	899	906	914	921	929	937	944	952	959	
75 76	967 76 042	974 050	982 057	989 965	997 072	*003 080	*012 087	*020 095	*027 103	*035 110	
77	118	125	1.33	140	148	155	163	170	178	185	
78	193 268	200	208	215	223	230	238	245	253	260	
79 <b>580</b>	343	275 350	283 358	365	298	305 380	313	320	328	335	
81	418	425	433	440	373 448	455	462	395 470	403 477	485	7
82	492	500	507	515	522	530	537	545	552	559	1 0.7
83	567.	574	582	589	597	604	612	619	626	634	$\begin{array}{c c} 2 & 1.4 \\ 3 & 2.1 \end{array}$
84 85	641 716	649 723	656 730	664 738	671 745	678 753	686 760	693 768	701	708 782	42.8
86	790	797	805	812	618	827	834	842	849	856	5 3.5 6 4.2
87	864	871	879	886	893	901	908	916	923	930	7 4.9
88 89	938 77 OI2	945 019	953 026	960 034	967 041	975 048	982 056	989 063	997	*004 078	8 5.6 9 6.3
590	085	093	100	107	115	122	129	137	144	151	0,0.0
91	159	166	173	181	188	195	203	210	217	225	
92 93	232 305	240 313	247 320	254 327	262 33 <del>5</del>	269 342	276 349	283 357	291 364	298 371	
94	379	386		327 401	408	415	422	430	437	444	
95	452	459	393 466	474	481	488	495	503	510	517	
96	525	532	539	546	554	561	568	576	583	590	
97 98	597 670	603	612 685	619 692	627 699	634 706	641 714	648 721	656 728	663	
99	743	750	757	764	772	779	786	793	801	735 808	
600	815	822	830	837	844	851	859	866	873	880	
N.	0	1	2	8	4	5	6	7	8	9	Prop. Pts.

. N.	0	1	2	3	4	5	6	7	8	9	Prop. Pts.
600	77 815	822	830	837	844	851	859	866	873	880	
01	887	893	902	909	916	924	931	938	945	952	
02 03	960 78 032	967 039	974 046	981 053	988	996 068	*003 075	*010 082	*017 089	*023 097	
10	104	111	118	125	132	140	147	154	161	168	
05 06	176 247	183 254	190 262	197 269	204 276	211 283	219 290	226 297	23 <u>3</u> 30 <u>5</u>	240 312	8
07 08	319 390	326 398	33 <u>3</u> 405	340 412	347 419	35 <u>5</u> 426	362 433	369 440	376 447	38 <u>3</u> 45 <u>5</u>	$ \begin{array}{c c} 1 & 0.8 \\ 2 & 1.6 \\ 3 & 2.4 \end{array} $
00	462	469	476	483	490 561	497 569	504 576	512	519	526	43.2
610 11	533 604	540	547 618	554 625	633	640	647	654	590 661	<u>597</u> 668	54.0 64.8
12 13	675 746	68 <sub>2</sub> 753	689 760	696	704 774	711 781	718	725 796	732	739 810	75.6 86.4
14	817	824	831	838	845	852	859	866	873	880	9 7.2
15 16	888 958	893 965	902 972	909 979	916 <b>98</b> 6	923 993	930 <b>*000</b>	937 <b>*007</b>	944 *014	951 <b>*</b> 021	
17	79 029	036	043	050	057	064	071	078	085	092	
18 19	099 169	106	113 183	120	127	1 34 204	211	148 218	225	162 232	
620	239	246	253	260	267	274	281	288	295	302	
21	309	316	323	330	337	344	351	358	36 <u>5</u>	372	7
22 23	379 449	386 456	393 463	470	407 477	414 484	42I 49I	428 498	43 <u>5</u> 505	442 511	1 0.7 2 1.4
24 25	518 588	52 <u>5</u> 595	532 602	539 609	546 616	553 623	560 630	567 637	574 644	581 650	3 2.1 4 2.8
26	657	664	671	678	685	692	699	706	713	720	5 3.5 6 4.2
27 28	727 796	734 803	741 810	748 817	754 824	761 831	768 ·   837	775 844	782 851	789 858	7 4.9 8 5.6
29	865	872	879	886	893	900	900	913	920	927	9 6.3
630	934	941	948	955	952	969	975	982	989	996	}
31 32	80 003 072	010 079	οι7 <b>ο</b> 8 <b>5</b>	024	030	037 106	044	120	058 127	063 134	
33	140	147	<b>#</b> 54	161	168	175	183	188	195	202	
34 35	209 277	216 284	223 291	229	236 305	243 312	318	257 325	264 332	271 339	,
36	346	353	359	366	373	380	387	393	400	407	16
37	414	421 489	·428	434	441	448 516	45 <del>5</del> 523	462	468 536	475	10.6
- 38 39	482 550	557	496 564	502 570	509 577	584	591	530 598	604	543 611	2 1.2 3 1.8
640	618	625	632	638	645	652	659	665	672	679	42.4
41 42	686	693	699 767	706 774	713 781	720 787	726	733	740 808	747 814	5 3.0 6 3.6
43	754 821	828	835	841	848	855	794 862	868	875	882	7 4.2 8 4.8
44	889	895	902 969	909 976	916 983	922	929 996	936 *003	943 *010	949 *017	9 5.4
45 46	956 81 023	963 <b>03</b> 0	037	043	050	990 057	064	070	077	084	
47	090	097 164	104	111	117 184	124	131	137	144 211	151 218	
48 49	158 224	231	171 238	245	251	191 258	265	204	278	283	
650	291	298	305	311	318	325	331	338	343	351	
N.	.0	1	,2	3	4	. 5	6	7	8	.9	Prop Pts.

N.	•	1	2	3	4	5	6	7	8	9	Prop. Pts.
650	81 291	298	303	311	318	325	331	338	345	351	
51 52	358 425	36 <del>5</del> 431	371 438	378 445	38 <u>5</u> 451	391 458	398 463	403 471	411 478	418 485	
53	491	498	503	511	518	525	531	538	544	551	
54	558	564	571	578	584	591	598	604	611	617	
55 56	624 690	697	637 704	710	651 717	657 723	664 730	671 737	677 743	684 750	
57	757	763	770	776	783	790	796	803	809	816	
58 59	823 889	829 895	836 902	908	84 <u>9</u> 915	856 921	862 928	86 <u>9</u> 935	875 941	.948	
660	954	96ī	968	974	981	987	994	*000	*007	*014	
61 62	82 020 086	027	033	040	046	053	060	066	073	079	7
63	151	158	099 164	105	112	119 184	125	132	138 204	145 210	$   \begin{array}{c c}     1 & 0.7 \\     2 & 1.4   \end{array} $
64	217	223	230	236	243	249	256	263	269	276	3 2.1 4 2.8
65 66	282 347	289 354	295 360	302 367	308 373	315 380	321 387	328 393	334	341 406	5 3.5
67	413	419	426	432	439	445	452	458	465	471	64.2 74.9
68 69	478 543	48 <sub>4</sub> 549	491 556	497 562	504 569	575	517 582	523 588	530 595	536 601	8 5.6 9 <b>6.3</b>
670	607	614	620	627	633	640	646	653	659	666	٥,٥,٥
71	672	679	685	692	698	70 <u>5</u> 769	711	718	724	730	
72 73	737 802	743 808	750 814	756 821	763 827	834	776 840	782 847	789 853	795 860	
74	<b>8</b> 66	872	879	885	892	898	903	911	918	924	
.75 76	930 995	937 * <b>001</b>	943 *008	9 <u>5</u> 0 *014	956 <b>*0</b> 20	963 * <b>02</b> 7	969 *033	975 <b>*04</b> 0	982 *046	988 *052	
77	83 059	065	072	078	o8 <del>5</del>	091	097	104	110	117	
78 79	123 187	129	136	142	149 213	219	161 225	168	174 238	181 245	
680	251	257	264	270	276	283	289	296	302	308	
81 82	31 <u>5</u> 378	321 385	327	334 398	340 404	347 410	353	359	366	372	6
83	442	448	391 455	461	467	474	417 480	423 487	429 493	436 499	$   \begin{array}{c c}     10.6 \\     21.2   \end{array} $
84	506 569	512	518	525	531	537 601	544	550	556	563	3 1.8 4 2.4
· 85 86	632	575 639	582 645	588 651	594 658	664	607 670	613	620	626. 689	53.0 63.6
87	696	702	708	715	721	727	734	740	746	753	7 4.2
88 89	759 822	765 828	771 835	778 841	784 847	790 853	797 860	803 866	809 872	816 879	8 4.8 9 5.4
690	883	891	897	904	910	916	923	929	935	942	
91 92	948	954 017	960 023	967 029	973 036	979 042	985 048	992 055	998 <b>9</b> 61	*004 067	
93	073	080	086	092	098	105	111	117	123	130	
94 95	136	143	148	153	161	167	173	180	186	192	
95 96	198 261	205 267	211 273	217 280	223 286	230 292	236 298	242 305	248 311	25 <del>5</del> 317	
97	323	330	336	342	348	354	361	367	373	379	
98 99	<b>38</b> 6 <b>44</b> 8	392 454	398 460	404 466	473	417 479	42 <u>3</u> 48 <u>5</u>	429 491	435 497	442 504	
700	510	516	522	528	535	541	547	553	559	566	
N.	0	ı	2	3	4	5	6	7	8	9	Prop. Pts.

N.	0	1	2	3	4	5	6	7	8	9	Prop. Pts.
700	84 510	516	522	528	535	541	547	553	559	566	
01	572	578	584	590	597	603	609	615	621	628	
02 03	634 696	640 702	646 708	652 714	658 7 <b>2</b> 0	66 <u>5</u> 726	733	677	68 <u>3</u>	689 751	İ
04		763	770	776	782	788	794	739 800	807	813	
05	757 819	825	831	837	844	830	856	862	868	874	
06	880	887	893	899	905	911	917	924	930	936	7
07 08	942 85 003	948 009	954 016	960	967 028	973 034	979	98 <u>5</u> 946	991 052	997 058	$   \begin{array}{c c}     10.7 \\     21.4   \end{array} $
09	065	071	077	083	089	095	101	107	114	120	3 2.1
710	126	132	138	144	150	156	163	169	175	181	42.8 53.5
11	187	193	199	205	211	217	224	230	236	242	64.2
12 13	248 309	254 315	260 321	266 327	272 333	278 339	28 <del>5</del> 345	29I 352	297 358	303 364	74.9 85.6
14	370	376	382	388	394	400	406	412	418	425	96.3
15	431	437	443	449	455	461	467	473	479	485	·
16	491	497	503	509	516	522	528	534	540	546	
17 18	552 612	558 618	564 625	570 631	576 637	582 643	588 649	59 <u>4</u> 655	661	606	
19	673	679	685	691	697	703	709	715	721	727	
720	733	739	745	751	757	763	769	775	781	788	
21 22	794 854	800 860	806 866	812 872	818 878	824 884	830 890	836 896	842 902	848 908	6
23	914	920	926	932	938	944	950	956	962	968	$ \begin{array}{c c} 1 & 0.6 \\ 2 & 1.2 \end{array} $
24	974	980	986	992	998	*004	*010	*016	*022	*028	3 1.8
25 26	86 ó34 094	040 100	046 106	052	058	064 124	070 130	136	082 141	088	42.4 53.0
27	153	159	165	171	177	183	189	195	201	207	63.6
28	213	219	225	231	237	243	249	255	261	267	7 4.2 8 4.8
29	273	279	285	291	297	303	308	314	320	326	9 5.4
780	332	338	344	350	356	362	368	374	380	386	
31 32	392 451	398 457	<b>404</b> <b>463</b>	410	41 <u>5</u> 475	421 481	427 487	433 493	439 499	445°	
33	510	516	522	528	534	540	546	552	558	564	
34	570	576	581	587	593	599	605	611	617.	623	
35 36	6 <b>29</b> 6 <b>88</b>	63 <del>5</del> 694	641 700	646 705	652 711	658 717	664 723	670 729	676 735	682 741	15
37		753	759	764	770	776	782	788	794	800	10.5
38	747 806	812	817	823 882	829	835	841	847	853	859	2 1.0
39 7 <b>4</b> 0	864	870	876	941	888	894	958	906	911	917	3 1.5 4 2.0
41	923	929 988	93 <del>5</del> 994	999	947 *005	953°	*017	*023	*029	*03 <del>5</del>	52.5
42	87 040	046	052	058	064	070	075	180	087	093	63.0 73.5
43	099	105	III	116	122	128	134	140	146	151	84.0 94.5
44 45	157 216	, 163 221	169 227	17 <del>5</del> 233	181 239	186 245	192 251	198 256	204 262	210 268	9 4.5
46	274	280	286	291	297	303	309	315	320	326	
47	332	338	344	349	355	361	36 <u>7</u>	373	379	384	]
48 49	390 448	396 454	402 460	408 466	413 471	419 477	42 <u>5</u> 483	431 489	43 <u>7</u> 49 <u>5</u>	443 500	
750	506	512	518	523	529	535	541	547	552	558	
N.	0	1	2	3	4	5	6	7	8	9	Prop. Pts.

N.	0	1	2	3	4	5	6	7	8	9	Prop. Pts.
750	87 506	512	518	523	529	535	541	547	552	558	
51	564	570	576	581	587	593	599	604	610	616	
52	622	628	633	639	645	651	656	662	668	674	į į
53	679	685	691	697	703	708	714	720	726	731	
54 55	737	743	749	754	760	766	772	777	783	789	
56	793 <b>85</b> 2	800 858	806 864	812 869	818 875	823 881	829 887	835	841	846	
57	910	915	921	927	1	938	944	950	955	961	İ
58	967	973	978	984	933	996	*001	*007	*013	*018	
59	88 024	030	<b>6</b> 36	041	047	053	058	064	070	076	
760	081	087	093	098	101	110	116	121	127	133	
61	138	144	150	156	161	167	173	178	184	190	6
62 63	195	201 258	207 264	213	218	224 281	230 287	235	241	247	1 0.6 2 1.2
64	252			270	275			292	ı	360	2 1.2 3 1.8
65	309 366	315 372	321 377	326 383	332 389	338 395	343 400	349 406	355	417	42.4
66	423	429	434	440	446	451	457	463	468	474	53.0 63.6
67	480	485	491	497	502	508	513	519	523	530	74.2
68	536	542	547	553	559	564	570	576	581	587	84.8
69	593	598	604	610	615	621	627	632	638	643	9 5.4
770	649	653	660	666	672	677	683	689	694	700	
71 72	705 762	767	717	722	728 784	734	739	74 <u>5</u> 801	750 807	756 812	
73	818	824	773 829	77 <u>9</u> 835	840	790 846	795 852	857	863	868	
74	874	880	885	891	897	902	908	913	919	925	
75	930	936	941	947	953	958	964	969	975	981	
76	930 986	992	997	<b>*</b> 003	*009	*014	*020	*025	*031	*037	
77	89 042	048	053	059	064	070	076	180	087	092	
78 79	098	104	109 16 <u>5</u>	115	120	126	131	137	143	148	
780	154	215	221	226	176			193 248	254	260	
81	209	271	276	282	232	<sup>237</sup> <sup>293</sup>	243 298		310	315	15
82	. 321	326	332	337	343	348	354	304 360	365	371	10.5
83	376	382	387	393	398	404	409	415	421	426	2 1.0
84	432	437	443	448	454	459	463	470	476	481	3 1.5
85 96	487	492	498	504	509	513	520	526	531	537	$\begin{array}{c c} & 4 2.0 \\ & 5 2.5 \end{array}$
86	542	548	553	559	564	570	575	581	586	592	63.0
87 88	597 653	658	609 664	669	620 675	625 680	631 686	636 691	642	702	7 3.5
89	653 708	713	719	724	730	735	741	746	752	757	84.0 94.5
790	763	768	774	779	785	790	796	801	807	812	,
. 51	818,	823	829	834	840	845	851	856	862	867	,
92	873	878	883	889	894	900	905	911	916	922	
93 94 95 96	927	933	938	944	949	953	960	1	971	977	
94	982	988	993	998	*004	*009	*015	*020	*026 080	*031 086	
95 96	90 037 091	042	048	. 108	059	064 119	069 124	129	135	140	
97	146	151	157	162	168	173	179	184	189	195	ŀ
98	200	206	211	217	222	227	233	238	244	249	
99	253	260	266	271	276	282.	287	293	298	304	ĺ
800	309	314	320	325	331	336	342	347	352	358	
N.	0	1	2	3	4	5	6	7	8	9	Prop. Pts.

	<b>L</b>										
N.	0	1	2	3	4	5	6	7	8	9	Prop. Pts.
800	90_309	314	320	325	331	336	342	347	352	358	
01 02	363	369	374	380	385	390	396	401	407	412	
03	417 472	423 477	428 482	434 488	439 493	44 <sup>5</sup> 499	450 504	455 509	461 515	466 520	
04	526	531	536	542	547	553	558	563	569	574	• .
05 06	580	585	590	596	601	607 660	612 666	617	623	628 682	
07	634 687	639 693	644 698	650 703	655 7 <b>0</b> 9	714	720	671	677	736	
08	741	747	752 806	757	763	768	773	725 779	730 784	789	
09	793	800		811	816	822	827	832	838	843	
810 11	849	854	859	918	870	875	881	886	891	897	16
12	902 956	907 961	913 966	972	924 977	929 982	934 988	940	945 998	950 *004	10.6
13	91 009	014	020	025	030	036	041	046	052	057	2 1.2 3 1.8
14 15	062 116	o68	073	078 132	084 137	089 142	094 148	100	105	110	42.4
16	169	174	180	185	190	196	201	153 206	212	217	53.0 63.6
17	223	228	233	238	243	249	254	259	26 <u>5</u>	270	7 4.2
18 19	275 328	281 334	286 339	291 344	297 350	302 355	307 <b>3</b> 60	312 365	318	323 376	84.8 95.4
820	381	387	392	397	403	408	413	418	424	429	8 U.¥
21	434	440	445	450	455	461	466	471	477	482	
22 23	487	492	498 551	503 556	508 561	514 566	519 572	524	529 582	535 587	
24	540 593	545 598	603	600	614	619	624	577 630	635	640	
25	645	651	656	661	666	672	677	682	687	693	•
26	698	703	709	714	719	724	730	733	740	745	
27 28	751 803	756 808	761 814	7 <b>6</b> 6 819	772 824	777 829	782 834	787 840	79 <u>3</u> 84 <u>5</u>	79 <b>8</b> -	
29	855	861	866	871	876	882	887	892	897	903	
880	908	913	918	924	929	934	939	944	950	955	. 15
31 32	960 92 012	965 018	97 I 023	976 028	981 033	986 038	991 <b>0</b> 44	997 049	*002 054	*007 059	10.5
33	063	070	075	080	085	091	096	101	106	111	2 1.0
34	117	122	127	132	137 189	143	148	153	158	163	31.5 42.0
35 36	169 221	174 226	179 231	184 236	189	19 <del>5</del> 247	200 252	205 257	210	215	52.5
37	· 273	278	283	288	293	298	304	309	314	319	63.0 73.5
38 39	324	330 381	335	340	345	350 402	355	361	366 418	371	84.0
840	376 428	433	387 438	392 443	397 449	454	459	464	469	423 474	9 4.5
41	480	485	490	495	500	505	511	516	521	526	
42	531	536	542	547	552	557	562	567	572	578 629	•
43	583	588	593	598	603	660 660	665	619	624	681	
44 45	<b>634</b> 686	639 691	64 <del>5</del> 696	6 <u>5</u> 0	65 <u>5</u> 706	711	716	670. 722	675 727	732	
46	737	742	747	752	758	763	768	773	778	783	
47 48	788 840	793 845	799 850	804 853	809 860	814 865	819 870	824 875	881	834 886	
49	891	896	901	906	116	916	921	927	932	937	
850	942	947	952	957	962	967	973	978	983	988	
N.	0	1	2	3	4	5	6	7	8	9	Prop. Pts.

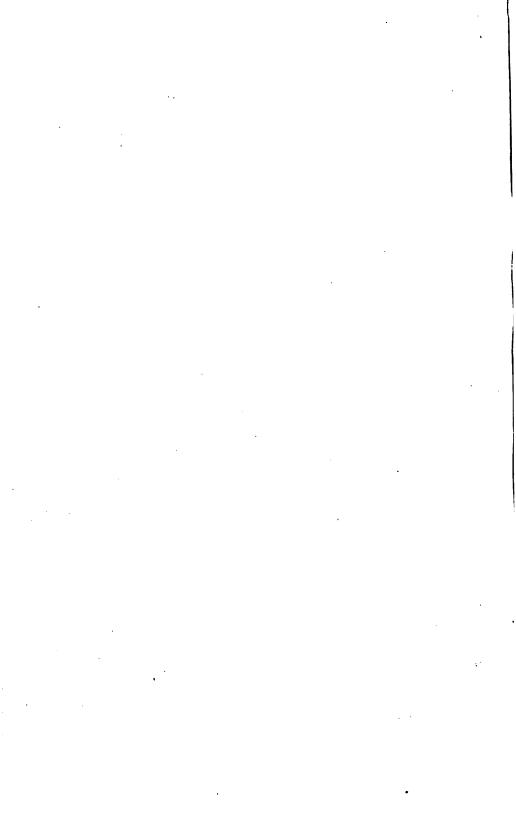
N.	0	· 1	. 3	3	4	5	. 6	7	. 8	9	Prop. Pts.
850	92 942	947	952	957	962	967	973	978	983	988	
51	993	998	*003	*008	*013	*018	*024	*029	*034	*039	,
52	93 044	049	054	059	064	069	075	080	083	090	
53	095	100	105	110	115	120	125	131	136	141	
54 55	146 197	151 202	156 207	161	166	171 222	176	181 232	186 237	192 242	
56	247	252	258	263	268	273	278	283	288	293	6
57	298	303	308	313	318	323	328	334	339	344	1 0.6
58	349	354	359	364	369	374	379	384	389	394	2 1.2 3 1.8
59 <b>860</b>	<u>399</u> 450	404	460	414	470	425	480	435	440	445	42.4
61	500	505	510	515	520	475 526	531	536	541	495 546	5 3.0 6 3.6
62	551	556	561	566	571	576	581	586	591	596	74.2
63	601	606	611	616	621	626	631	636	641	646	84.8
64	651	656	661	666	671	676	682	687	692	697	9 5.4
65 66	702 752	707 757	712	717	722	727 777	732 782	737	742	747 797	
67	802	807	812	817	822	827	832	837	842	847	
68	852	857	862	867	872	877	882	887	892	897	
69	902	907	912	917	922	927	932	937	942	947	
870	952	957	962	967	972	977	982	987	992	997	15.
71 72	94 002 052	007 057	012	017	022	027 077	032	037 086	042	047 096	10.5
73	101	106	111	116	121	126	131	136	141	146	2 1.0
74	151	156	161	166	171	176	181	186	191	196	31.5 42.0
75	201	206	211	216	221	226	231	236	240	245	52.5
76	250	255	260	265	270	275 —	280	285	290	295	63.0
77 78	300 349	30 <u>₹</u>	310 359	31 <del>5</del> 364	320 369	32 <del>5</del> 374	379	33 <del>5</del> 384	340 389	34 <del>5</del> 394	73.5 84.0
79	399	404	409	414	419	424	429	433	438	443	94.5
880	448	453	458	463	468	473	478	483	488	493	
81.	498	503	507	512	517	522	527	532	537	542	
82 83	547 596	552 601	557 606	562 611	567 616	57 I 62 I	576 626	581 630	586 635	591 640	
84	645	650	655	660	663	670	673	680	683	689	
85	694	699	704	709	714	719	724	729	734	738	
86	743	748	753	758	763	768	773	778	783	787	4
87	792	797	802	807	812 861	817 866	822	827 876	832	836 885	1 0.4 2 0.8
88 89	. 841 . 890	846 895	851 900	856 905	910	913	871 919	924	880	934	3 1.2
890	939	944	949	954	959	963	968	973	978	983	4 1.6
91	988	993	998	*002	*007	*012	*017	*022	*027	*032	$\begin{array}{c} 5   2.0 \\ 6   2.4 \end{array}$
92	95 036 085	041	046	051	056	061	066	071	075	080	72.8
93		090	095	100	103	109	114	119	124	129	8 3.2 9 3.6
94 95	134 182	139	143 192	148	153	158 207	163	168	173	177 226	ا 5,5,5
96	231	236	240	245	250	255	260	265	270	274	
97	279	284	289	294	299	303	308	313	318	323	
98	328	332	337 386	342	347	352	357	361	366	371	
99 <b>900</b>	376 424	381 429	434	390 439	395 444	400	405	458	413	468	
N.		1	2	3	4	5	6	7	8	9	Prop. Pts.
	•		1. ~	, ,	*		1	<u> </u>	•	١ ٠	Trop. rus.

						BLE I			-		
N.	0	1	9	3	4	5	6	7	8	9	Prop. Pts.
900	95 424	429	434	439	444	448	453	458	463	468	
01	472	477	482	487	492	497	501	506	511	516	
02	521	525	530	535	540	543	530	554	559	564	
03	569	574	578	583	588	593	598	602	607	612	
04 05	617 663	622 670	626 674	631 679	636 684	641 689	646	650 698	655 703	660 708	
06	713	718	722	727	732	737	742	746	751	756	
07	761	766	770	775	780	783	789	794	799	804	
08	809	813 861	818	823	828	832 880	837 885	842	847	852	
910	856 904	l	I	918	875	928		890	895	899	
11	952	909	914	966	923		933 980	938 985	942	947	1 5
12	999	957 <b>*00</b> 4	*009	*014	971 <b>*</b> 019	976 <b>*02</b> 3	*028	<b>*</b> 033	990 *038	995 *042	10.5
13	96 047	052	057	06 i	066	07 I	076	080	085	090	2 1.0
14	०९इ	099	104	109	114	118	123	128	133	137 185	3 1.5 4 2.0
15 16	I42 I90	147 194	152	156	161 209	166 213	171	175	180		5 2.5
8 1		1	199	1	1	261	265	223	227	232	63.0
17 18	237 284	242	246 294	251 298	256 303	308	313	270 317	275 322	280 327	73.5 84.0
19	332	336	341	346	350	355	360	365	369	374	94.5
920	379	384	388	393	398	402	407	412	417	421	
21	426	431	435	440	445	450	454	459	464	468	
22 23	473 520	478 525	483 530	487 534	492 539	497 544	501 548	506	511	515 562	
24	567	572	577	58r	586	591	595	600	603	609	
25	614	619	624	628	633	638	642	647	652	656	
26	166	666	670	675	680	683	689	694	699	703	
27	708	713	717	722	727	731	736	741	745	750	
28 29	753 802	759 806	764 811	769 816	774 820	778 825	783 830	788 834	792 839	797 844	
980	848	853	858	862	867	872	876	881	886	890	
31	893	900	904	909	914	918	923	928	932	937	4
32	0.12	946	951	956	960	963	970	974	979	984	10.4
33	988	993	997	*002	*007	*011	*016	*021	<b>*02</b> 5	*030	2 0.8 3 1.2
34 35	97 035	039	044	049	053 100	058 104	063	067	072	077 123	41.6
36	128	132	137	142	146	151	155	160	163	169	52.0
37	174	179	183	188	192	197	202	206	211	216	62.4 72.8
38	220	225	230	234	230	243	248	253	257	262	83.2
39	267	271	276	280	285	290	294	299	304	308	9 3.6
940	313	317	368	327	331	336 382	340	345	350	354	
41 42	359 405	410	414	373	377 424	302 428	433	391 437	396 442	400	
43	451	456	460	465	470	474	479	437 483	442 488	493	
44	497	502	506	511	516	520	525	529	534 580	53 <u>9</u> 585	
45 46	543 589	548 594	552 598	557 603	562 607	566 612	571 617	575 621	580 626	58 <u>5</u> 630	
	633	640	644	649	653	658	663	667	672	676	
47 48	681	685	690	695	699	704	708	713	717	722	
49	727	731	736	740	745	749	754	759	763	768	
950	772	777	782	786	791	795	800	804	809	813	
N.	0	1	2	3	4	5	6	7	8	9	Prop. Pts.

N.	0	1	2	3	4	5	6	7	8	9	Prop. Pts.
950	97 772	777	782	786	791	795	800	804	809	813	
51	818	823	827	832	836	841	845	850	853	859	
52 53	864 909	868 914	873 918	877 923	882 928	886 932	891 937	896 941	900	90 <u>3</u> 950	
54	953	959	964	968	973	978	982	987	991	996	·
55 56	98 000 046	050	055	014 059	019	023 068	028	032	037 082	041 087	
57	091	096	100	103	109	114	118	123	127	132	
58	137 182	141	146	150	155	159	164	168	173	177	
59 <b>960</b>	227	232	191 236	195 241	245	204 250	209 254	259	263	268	
61	272	277	281	286	290	295	299	304	308	313	5
62	318	322	327	331	336	340	345	349	354	358	10.5
63	363 408	367 412	372 417	376 421	381 426	385	390	394	399 444	403	2 1.0 3 1.5
64 65		457	462	466	471	430 475	435 480	439 484	489	448 493	42.0
66	453 498	502	507	511	516	520	525	529	534	538	5 2.5 6 3.0
67 68	543 588	547 592	552 597	556 601	561 605	565 610	570 614	574 619	579 623	583 628	73.5 84.0
69	632	637	641	646	650	655	659	664	668	673	94.5
970	677	682	686	691	695	700	704	709	713	717	i
71 72	722 767	726 771	731 776	735 780	740 784	744 789	749 793	753 798	758 802	762 807	
73	811	816	820	823	829	834	838	843	847	851	
74	856	860	863	869	874	878	883	887	892	896	
75 76	900 943	905 949	909 954	914 958	918 963	923 967	927 972	932 976	936 981	941 985	
77	<b>98</b> 9	994	998	*003	*007	*012	<b>*</b> 016	*021	*025	*029	
78 79	99 034 078	038	043 087	047 092	052 096	100	105	109	069 114	074 118	
980	123	127	131	136	140	145	149	154	158	162	
81	167	171	176	180	185	189	193	198	202	207	4
82 83	211 255	216 260	220 264	224 269	229 273	233 277	238 282	242 286	247 291	251 295	1 0.4 2 0.8
84	300	304	308	313	317	322	326	330	335	339	3 1.2
85	344	348	352	357	361	366	370	374	-379	383	4 1.6 5 2.0
86 87	388 432	392 436	396 441	443	405 449	454	414	463	4 <sup>2</sup> 3	427 471	6 2.4 7 2.8
88	476	480	484	489	493	498	502	506	511	515	83.2
89	520 564	524 568	528	533	537 581	542	546	550	555	559	9 3.6
980 91	607	612	572 616	577 621	625	585 629	590 634	594 638	599 642	603 647	
. 22	651 695	656	660	664	669	673	677	682	686	691	
93 94 95 96 97 98		699	704	708	712	717	721	726	730	734	
94 95	739 782	743 787	747 791	752 795	756 800	760 804	76 <u>3</u> 808	769 813	774 817	778 822	!
96	826	830	791 83 <del>5</del>	839	843	848	852	856	861	865	
97 98	870 913	874 917	878 922	883 926	887 930	891 935	896 939	900 944	904 948	909 952	
99	957	961	965	970	974	978	983	987	991	996	
1000	00 000	004	009	013	017	022	026	030	035	039	
N.	0	1	2	3	4	5	6	7	8	9	Prop. Pts.

20						DLE 1	==				
N.	0	1	2	3	4	5	6	7	8	9	Prop. Pts.
1000	000 000	043	087	130	174	217	260	304	347	391	
1001	434	477	521	564	608	651	694	738	781	824	
1002	868 001 301	911 344	954 388	998 431	*041 474	*084 517	*128 561	*171 604	*214 647	*258 690	1 44
1004	734	777	820	863	907	950	993	*036	*o8o	*123	1 4.4
1005	002 166	209	252	296	339	382 814	425	468	512	555	2 8.8
1006	598	641	684	727	771	i	857	900	943	986	3 13.2 4 17.6
1007 1008	003 029 461	504	547	159 590	633	245 676	288 719	331 762	374 805	417 848	5 22.0
1009	891	934	977	*020	*063	*106	*149	*192	*235	*278	6 26.4 7 30.8
1010	004_321	364	407	450	493	536	579	622	665	708	8 35.2
1011 1012	751 005 180	794	837 266	880 309	923 352	966 •395	*009 438	*052 481	*095 524	*138 567	9 39.6
1013	609	652	695	738	781	824	867	909	952	995	
1014	006 038	180	124	166	209	252	295	338	380	423	
1015 1016	466 894	936	552 979	594 *022	637 <b>*</b> 065	680 *107	723 *150	765 *193	808 *236	851 *278	48
1017	007 321	364	406	449	492	534	577	620	662	705	1 4.3 2 8.6
1018	748	790	833	876	918	961	*004	*046	*089	*132	3 12.9
1019	008 174	217	259	302	345	387	430	472	515	558	4 17.2 5 21.5
1020	600	643	685	728	770	813	856	898	941	983 408	6 25.8
1021 1022	009 026 451	068   493	536	153 578	196 621	238 663	281 706	323 748	366 791	833	7 30.1 8 34.4
1023	876	816	961	*003	*045	*o88	*130	*173	*215	*258	9 38.7
1024	010 300	342	385	427	470	512	554	597	639	681	
1025 1026	724 011 147	766	809	274	317	936 359	978	*020 444	*063 486	*105 528	
1027	570	613	655	697	740	782	824	866	909	951	42
1028	993	*035	*078	*120	*162	*204	*247	*289	*331	*373	1 4.2
1029 1080	012 415 837	879	922	542 964	584 *006	626 *048	669 *090	711 *132	753 *174	795 *217	2 8.4 3 12.6
1031	013 259	301	343	385	427	469	511	553	596	638	4 16.8
1032	680	722	764	806	848	890	932	974	*016	*058	$ \begin{array}{c c} 5 & 21.0 \\ 6 & 25.2 \end{array} $
1033	014 100	142	184	226	268	310	352	395	437	479	7 29.4
1034 1035	521 940	982	605 *024	647 *o66	801*	730 *150	772 *192	814 *234	856 *276	898 *318	8 33. <b>6</b> 9 37. <b>8</b>
1036	015 360	402	444	485	527	569	611	653	695	737	0,07.0
1037	779	821	863	904	946	988	*030	*072	*114	<b>*</b> 1 56	•
1038 1039	016 197 616	657	281 699	323 741	365 783	407 824	448 866	490 908	532 950	574 992	! <b>41</b>
1040	017 033	075	117	159	200	242	284	326	367	409	1 4.1
1041	451	492	534	576	618	659	701	743	784	826	2 8.2
1042	868 618 284	909	951 368	993	*034	*076	*118	*159	*201	*243	3 12.3 4 16.4
1043 1044	700	326 742	784	825	451 867	492 908	950	576 992	617 *033	659 <b>*075</b>	5 20.5
1044	019 116	158	199	241	282	324	366	407	449	490	6 24.6 7 28.7
1046	532	573	615	656	698	739	781	822	864	905	8 32.8
1047 1048	947 020 361	988	*030 444	*071 486	*113	*154 568	*195 610	*237 651	*278	*320	9 36.9
1048	775	817	858	900	527 941	982	*024	*065	693 *107	734 *148	
1050	021 189	231	272	313	355	396	437	479	. 520	561	
N.	0	1	2	3	4	. 5	6	7	8	9	Prop. Pts.

N.		0	1	2	3	4	5	6	7	8	9	Prop. Pts.
1050	021		231	272	313	355	396	437	479	520	561	
1051	1	603	644	685	727	768	809	851	892	933	974	
1052	022		057	098	140	181	222	263	305	346	387	
1053		428	470	511	552	593	635	676	717	758	799	42
1054	1	841	882	923	964	<b>*</b> 005	*047	<b>*</b> 088	*129	*170	*211	1 4.2
	023		294	335	376	417	458	499	541	582	623	2 8.4
1056		664	705	746	787	828	870	911	952	993	*034	3 12.6
1057	024		116	157	198	239	280	321	363	404	445	4 16.8 5 21.0
1058 1059		486 896	527	568	<b>*0</b> 19	650 <b>*0</b> 60	*101	732	773 *183	814 *224	855 *265	6 25.2
	025	306	937 347	978 388	429	470	511	*142 552	593	634	674	7 29.4
1061			756		838	879		961			*084	8 33.6
	026	715	165	797 206	247	288	920 329	370	*002 411	*043 452	492	9 37.8
1063		<b>5</b> 33	574	613	656	697	737	778	819	860	901	
1064		942	982	*023	*064	<b>*</b> 105	*146	*186	*227	*268	*309	
	027	350	390	431	472	513	553	594	635	676	716	41
1066	•	757	798	839	879	920	96ĭ	*002	*042	<b>*</b> 083	*124	1 4.1
1067	028	164	205	246	287	327	368	409	449	490	531	2 8.2
1068		571	612	653	693	734	775	815	856	896	937	3 12.3
1069		978	810*	*059	*100	*140	*181	*22Î	*262	*303	*343	4 16.4
1070	029	384	424	465	506	546	587	627	668	708	749	5 20.5
1071	-	789	830	871	911	952	992	<b>*</b> 033	*073	*114	*154	6 24.6 7 28.7
1072	030		235	276	316	357	397	438	478	519	559	832.8
1073		600	640	681	721	762	802	843	883	923	964	9 36.9
1074	031	004	045	085	126	166	206	247	287	328	368	
1075		408	449	489	530	570	610	651	691	732	772	ļ
1076		812	853	893	933	974	*014	*054	*095	*135	*175	
	032		256	296	337	377	417	458	498	538	578	40
1078		619	659	699	740	780	820	860	901	941	981	1 4.0
	033_		062	102	142	182	223	263	303	343	384	2 8.0
1080	-	424	464	504	544	585	625	665	705	745	785	3 12.0 4 16.0
1081		826	866	906	946	986	*027	*067	*107	*147	*187	5 20.0
1082 1083	034	227 628	267 669	308 709	348	388 789	428 829	468   869	508	548	588 989	6 24.0
					749	1		1	909	949	' '	7 28.0
1084 1085	035		069 470	510	149	190	230	670	310	350	390	8 32.0
1086		430 830	870	910	550 950	990	630 *030	*070	710	750 *150	790 *190	9 36.0
			269	1		389		469	l	-		
1088	036	230 629	669	309 709	349 749	789	429 828	868	908	549 948	589 988	
	037	028	068	108	148	187	227	267	307	347	387	89
1090		426	466	506	546	586	626	665	705	745	785	1 3.9
1091	-	825	865	904	944	984	*024	*064	*103	*143	*183	2 7.8
	038		262	302	342	382	42I	461	501	541	580	3 11.7
1093	1	620	660	700	739	779	819	859	898	938	978	4 15.6 5 19.5
1094	039	017	057	097	136	176	216	255	295	335	374	6 23.4
1095		414	454	493	533	573	612	652	692	731	771	7 27.3
1096	1	811	850	890	929	969	*009	*048	*088	*127	*167	8 31.2
	040		246	286	325	365	405	444	484	523	563	9 35.1
1098		602	642	681	721	761	800	840	879	919	958	
1099	·-	998	*037	*077	*116	*156	*195	*235	*274 669	*314	*353	
	041	393	432	472	511	551	590	630	009	708	748	
N.		0	1	2	3	4	5	6	7	8	9	Prop. Pts.



## TABLE II.

## CONSTANTS WITH THEIR LOGARITHMS.

		Number.	Logarithm.
Ratio of circumference	to diameter, $\pi$	3.14159265	0.49714 99
••	π <sup>3</sup>	9.86960440	0-99429 97
••	2π	6.28318531	0.79817 99
•• :•	$$ $\sqrt{\pi}$	1-77245385	0.24857 49
Number of degrees in	circumference,	360 <sup>0</sup>	2.55630 25
minutes	••	21600′	4-33445 38
•• seconds	••	1296000"	6.11260 50
Degrees in arc equal t	o radius,	57°-2957795	1.75812 26
Minutes	••	3437'-74677	3.53 <sup>62</sup> 7 39
Seconds	••	206264".806	5-31442 51
Length of arc of 1 de	egree,	.01745329	8.24187 74—10
ım	inute,	.00029089	6.46372 61-10
I se	cond,	.000004848	4.68557 49—10
Number of hours in 1	day,	24	1.38021 12
minutes	••	1440	3.15836 25
seconds	•	86400	4.93651 37
Number of days in Ju	lian year,	365.25	2.56259 02
Naperian base,		2.718281828	0-43429 45
Modulus of common	logarithms,	0.434294482	9.63778 43—10
Hours in which earth	•	<b>1</b>	
arc equal to radius	·	3.8197186	0.58203 14
Minutes of time .	• •• ••	229.18312	1 ,
Seconds of time .	• •• ••	13750.987	4-13833 39

log of log e = 9.637794 = log M

### TABLE III.

FOR

## SINES AND TANGENTS OF SMALL ANGLES.

#### TO FIND THE SINE OR TANGENT:

Log sin  $\alpha = \log \alpha$  (in seconds) + S.

Log tan  $\alpha = \log \alpha$  (in seconds) + T.

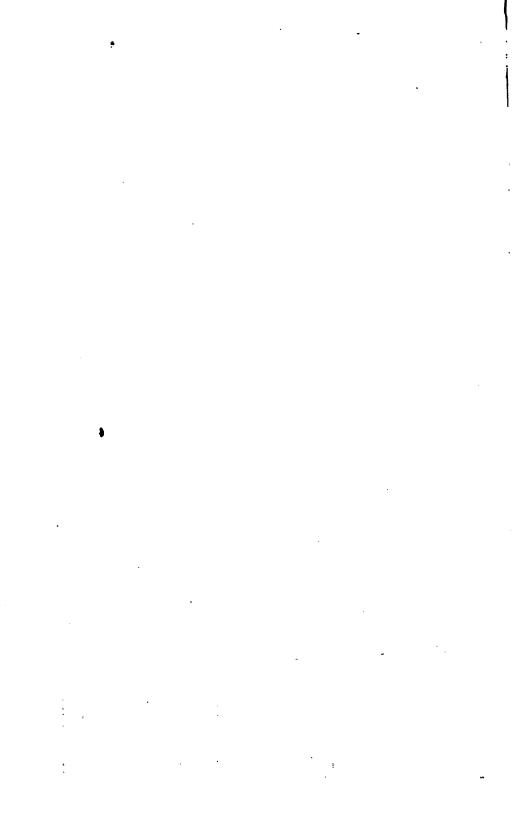
#### TO FIND A SMALL ANGLE FROM ITS SINE OR TANGENT:

Log  $\alpha$  (in seconds) = log sin  $\alpha + S'$ .

Log  $\alpha$  (in seconds) = log tan  $\alpha + T'$ .

			. O	)		
"	,	L. Sin.	8	T	8'	T'
0 60 120	0 1 2	6.46373 .76476	4.68557 .68557 .68557	4.68557 .68557 .68557	5.31443 .31443	5.31443 .31443
180 240	3 4	. 94085 7.06579	.68557 .68557	.68557 .68558	.31443 .31443 .31443	.31443 .31443 .31442
300 360 420	5 6	7.16270 .24188 .30882	4.68557 .68557 .68557	4.68558 .68558 .68558	5.31443 31443	5.31442 .31442
480 540	7 8 9	.36682	.68557 .68557	.68558 .68558	.31443 .31443 .31443	.31442 .31442 .31442
600 660 720	10 11 12	7.46373 .50512 .54291	4.68557 .68557 .68557	4.68558 .68558 .68558	5.31443 .31443 .31443	5.31442 .31442 .31442
780 840	13 14	.57767 .60985	.68557 .68557	.68558 .68558	.31443	.31442 .31442
900 960 1020	15 16 17	7.63982 .66784 .69417	4.68557 .68557 .68557	4.68558 .68558 .68558	5.31443 .31443 .31443	5.31442 .31442 .31442
1080 1140	17 18 19	. 71900 . 74248	.68557 .68557	.68558 .68558	.31443 .31443	.31442 .31442
1200 1260 1320	20 21 22	7 · 76475 · 78594 · 80615	4.68557 .68557 .68557	4.68558 .68558 .68558	5.31443 .31443 .31443	5.31442 .31442 .31442
1380 1440	23 24	.82545 .84393	.68557 .68557	.68558 .68558	.31443 .31443	.31442 .31442
1500 1560 1620	25 26 27 28	7.86166 .87870 .89509	4.68557 .68557 .68557	4.68558 .68558 .68558	5.31443 .31443 .31443	5.31442 .31442 .31442
1680 1740 1800	29	.91088 .92612	.68557 .68557	.68 <u>55</u> 8 .68559	.31443	.31442 .31441
1860 1920	30 31 32	7.94084 ,95508 .96887	4.68557 .68557 .68557	4.68559 .68559 .68559	5 31443 .31443 .31443	5.31441 .31441 .31441
1980 2040 2100	33 _34	.98223 .99520 8.00779	.68557 .68557 4.68557	.68559 .68559	.31443	.31441
2160 2220	35 36 37 38	.02002 .03192	.68557 .68557	4.68559 .68559 .68559	5.31443 .31443 .31443	5.31441 .31441 .31441
2280 2340 2400	38 39 40	.04350 .05478 8.06578	.68557 .68557 4.68557	.68559 .68559 4.68559	.31443	.31441
2460 2520	41 42	.07650 .0869 <u>5</u>	.68556 .68556	.68560 68560	5.31443 .31444 .31444	5.31441 .31440 .31440
2580 2640 2700	43 44 45	.09718 .10717 8.11693	.68556 .68556 4.68556	.68560 .68560 4.68560	.31444 .31444 5.31444	.31440 .31440 5.31440
2760 2820 2880	46 47	. 12647 . 1358 <b>1</b>	.68556 .685 <b>5</b> 6	.68560 .68560	.31444 .31444	.31440 .31440
2000 2000	48 49 50	. 14495 . 15391 8, 16268	.68556 .68536 4.68556	.68560 .68560 4.68561	.31444 .31444 5.31444	.31440 .31440 5.31439
3060 3120	51 52	. 17128 . 17971	.68556 .68556	.68561 .68561	.31444 .31444	.31439 .31439
3180 3240 3300	53 54 55	.18798 .19610 8.20407	.68556 .68556 4.68556	.68561 .68561 4.68561	. \$1444 .31444 5.31444	.31439 .31439 5.31439
3360 3420	55 56 57 58	.21189 .21958	.68556 .6855 <b>5</b>	.68561 .68561	.31444 .31445	.31439 .31439
3480 3540 3600	58 59 60	.22713 .23456 8.24186	.68555 .68555 4.68555	.68562 .68562 4.68562	.31445 .31445 5.31445	.31438 .31438 5.31438
		1	1 7.5533	1 7.55502	3.3.443	3.3.430

			19	)		
"	•	L. Sin.	8	T	S'	T'
3600 3660 3720 3780 3840	0 1 2 3 4	8.24186 .24903 .25609 .26304 .26988	4.68555 .68555 .68555 .68555 .68555	4.68562 .68562 .68562 .68562 .68563	5.31445 .31445 .31445 .31445 .31445	5.31438 .31438 .31438 .31438 .31437
3900 3960 4020 4080 4140	56 78 9	8.27661 .28324 .28977 .29621 .30255	4.68555 .68555 .68555 .68555 .68555	4.68563 .68563 .68563 .68563 .68563	5.31445 .31445 .31445 .31445 .31445	5-31437 -31437 -31437 -31437 -31437
4200 4260 4320 4380 4440	10 11 12 13 14	8.30879 .31495 .32103 .32702 .33292	4.68554 .68554 .68554 .68554 .68554	4.68563 .68564 .68564 .68564 .68564	5.31446 .31446 .31446 .31446 .31446	5.31437 .31436 .31436 .31436
4500 4560 4620 4680 4740	15 16 17 18 19	8.33 <sup>8</sup> 75 .34450 .35018 .35578 .36131	4.68554 .68554 .68554 .68554	4.68564 .68565 .68565 .68565	5.31446 .31446 .31446 .31446	5.31436 .31435 .31435 .31435
4800 4860 4920 4980 5040	20 21 22 23 24	8.36678 .37217 .37750 38276 .38796	4.68554 .68553 .68553 .68553 .68553	4.68565 .68566 .68566 .68566 .68566	5.31446 .31447 .31447 .31447 .31447	5.31435 .31434 .31434 .31434
5100 5160 5220 5280 5340	25 26 27 28 29	8.39310 .39818 .40320 .40816 .41307	4.68553 .68553 .68553 .68553 .68553	4.68566 .68567 .68567 .68567 .68567	5.31447 .31447 .31447 .31447 .31447	5.31434 .31433 .31433 .31433
5400 5460 5520 5580 5640	30 31 32 33 34	8 41792 .42272 42746 .43216 .43680	4.68553 .68552 .68552 .68552 .68552	4.68567 .68568 .68568 .68568 .68568	5.31447 .31448 .31448 .31448 .31448	5·31433 .31432 .31432 .31432
5700 5760 5820 5880 5940	35 36 37 38 39	8.44139 .44594 .45044 .45489 .45930	4.68552 .68552 .68552 .68552 .68551	4.68569 .68569 .68569 .68569 .68569	5.31448 .31448 .31448 .31448 .31449	5.31431 .31431 .31431 .31431
6000 6060 6120 6180 6240	40 41 42 43 44	8.46366 .46799 .47226 .47650 .48069	4.68551 .68551 .68551 .68551 .68551	4.68570 .68570 .68570 .68570 .68571	5.31449 .31449 .31449 .31449 .31449	5.31430 .31430 .31430 .31430 .31429
6300 6360 6420 6480 6540	45 46 47 48 49	8.48485 .48896 .49304 .49708 .50108	4.68551 .68551 .68550 .68550 .68550	4.68571 .68571 .68572 .68572 .68572	5.31449 .31449 .31450 .31450 .31450	5.31429 .31429 .31428 .31428 .31428
6600 6660 6720 6780 6840	50 51 52 53 54	8 50504 .50897 .51287 .51673 .52055	4.68550 .68550 .68550 .68550 .68550	4.68572 .68573 .68573 .68573 .68573	5.31450 .31450 .31450 .31450 .31450	5.31428 .31427 .31427 .31427 .31427
6900 6960 7020 7080 7140	55 56 57 58 59	8.52434 .52810 .53183 .53552 .53919	4.68549 .68549 .68549 .68549 .68549	4.68574 .68574 .68574 .68575 .68575	5.31451 .31451 .31451 .31451 .31451	5.31426 .31426 .31426 .31425 .31425
7200	60	8.54282	4.68549	4.68575	5.31451	5.31425



### TABLE IV.

# LOGARITHMS

OF THE

SINE, COSINE, TANGENT AND COTANGENT

FOR

EACH MINUTE OF THE QUADRANT.

		****			<b>0</b> °			
,	L. Sin.	d.	L. Tang.	c. d.	L. Cotg.	L. Cos.		Prop. Pts.
U			<del></del>			0.∞∞	60	
1 2	6.46 373 6.76 476	30103	6.46 373 6.76 476	30103	3.53 627 3.23 524	0.00000	59 58	3476 3218 2997 .1 348 322 300
3	6.94 083	17609 12494	6.94 083	17609 12494	3.05 915	0.00 000	57	.2 695 644 599
1 4	7.06 579	9691	7.06 579	9691	2.93 421	0.00 000	56	.3 2043 965 899
5	7.16 270 7.24 188	7918	7.16 270 7.24 188	7918	2.83 730 2.75 812	0.00000	55 54	.4 1390 1287 1199 .5 1738 1609 1498
8	7.30 882	6694 5800	7.30 882	6694 5800	2.69 118	0.00 000	53	
9	7.36 682 7.41 797	5115	7.36 682 7.41 797	5115	2.63 318	0.00 000	52 51	2892 2633 2483 .7 280 263 248
10	7.46 373	4576	7.46 373	4576	2.53 627	0.00000	50	.2 560 527 497
11	7.50 512	4139 3779	7.50 512	4139 3779	2.49 488	0.00 000	49 48	.3 841 790 745 .4 2323 2053 993
12 13	7.54 291 7.57 767	3476	7.54 291 7.57 767	3476	2.45 709	0.00 000	48	.5 1401 1316 1242
14	7.60 985	3218 2997	7.60 986	3219 2996	2.39 014	0.00 000	46	2227  2021  1848
15 16	7.63 982	2802	7.63 982	2803	2.36 018	0.00 000	45	.1 223 202 185
17	7.66 784 7.69 417	2633	7.66 78 <del>5</del> 7.69 418	2633	2.33 215 2.30 582	9.99 999	44	.2 445 404 370
18	7.71 900	2483 2348	7.71 900	2482 2348	2.28 100	9.99 999	42	.3 668 606 554 .4 891 808 739
19 20	7.74 248	2227	7.74 248	2228	2.25 752	9.99 999	41	.5 1113 1010 924
21	7.78 594	2119	7.78 595	2119	2.23 524 2.21 405	9.99 999 9.99 999		1704  1579  1472
22	7.78 594 7.80 615	2021 1930	7.80 615	2020 1931	2.19 383	9.99 999	39 38	.3 170 158 147
23 24	7.82 545 7.84 393	1848	7.82 546 7.84 394	1848	2.17 454 2.15 606	9.99 999	37 36	.2 341 316 294 .3 511 474 442
25	7.86 166	1773	7.86 167	1773	2.13 833	9.99 999	35	.3 511 474 442 .4 682 632 589
26	7.87 870	1704 1639	7.87 871	1704 1639	2.12 129	9.99 999	34	.5 852 789 736
27 28	7.89 509 2 91 088	1579	7.89 510 7.91 089	1579	2.10 490 2.08 911	9 99 999	33 32	1379  1297  1223
29	7.92 612	1524 1472	7.92 613	1524 1473	2.07 387	9.99 998	31	.1 138 130 122
80	7.94 084	1424	7.94 086	1424	2.05 914	9.99 998	80	.2 276 259 245 .3 414 389 367
31 32	7.95 508 7.96 887	1379	7.95 510	1379	2.04 490 2.03 111	9.99 998 9.99 998	. 29 28	.4 552 519 489
33	7.98 223	1336 1297	7.98 225	1336 1297	2.01 775	9.99 998	27	.5  690  649  612
34	7.99 520 8.00 779	1259	7.99 522 8.00 781	1259	1.99 219	9.99 998	26 25	1158 1100 1046
35 36	8.02 002	1223	8.02 004	1223	1.97 996	9.99 998	24	.1 116 110 105
37 38	8.03 192 8.04 350	1190	8.03 194 8.04 353	1190	1.96 806	9.99 997	23	.2 232 220 209 .3 347 330 314
39	8.05 478	1128	8.05 481	1128	1.95 647 1.94 519	9·99 997 9·99 997	22 21	.4 463 440 418
40	8.06 578	1100	8.06 581	1100	1.93 419	9.99 997	20	·5  579  550  523
41 42	8.07 6 <u>3</u> 0 8.08 696	1072 1046	8.07 653 8.08 700	3047	1.92 347	9.99 997	19 18	999 954 914
43	8.09 718	1022	8.09 722	1022	1.90 278	9.99 997 9.99 997	17	.1 100 95 91 .2 200 191 183
44	8.10 717	999 976	8.10 720	976	1.89 280	9 99 996	16	.3 300 286 274
45 46	8.11 693 8.12 647	954	8.11 696 8.12 651	955	1.88 304 1.87 349	9.99 996 9.99 996	15 14	.4 400 382 366 .5 500 477 457
47 48	8.13 581	934	8.13 585	934	1.86 415	9.99 996	13	.,
48 49	8.14 495 8.15 391	914 896	8.14 500 8.15 395	915 895	1.85 500 1.84 603	9.99 996 9.99 996	12 11	.1 88 84 81
50	8.16 268	877	8.16 273	878	1.83 727	9.99 995	10	.2 175 169 162
51	8.17 128	860 842	8.17 133	860 842	1.82 867	9.99 995	9	.3 263 253 244
52 53	8.17 971 8.18 798	843 827	8.17 976 8.18 804	843 828	1.82 024 1.81 196	9.99 99 <u>5</u> 9.99 99 <u>5</u>	8	-4 351 337 325 -5 438 422 406
54	8.19610	812	8.19616	812	1.80 384	9.99.995	7	, , ,
55 56	8.20 407	797 782	8.20 413	797 782	1.79 587	9.99 994	5	.1 78 75 730 .1 78 75 73
50 57	8.21 189 8.21 958	769	8.21 195 8.21 964	769	1.78 803	9.99 994 9.99 994	4	.2 156 151 146
57 58 59	8.22 713	755 743	8.22 720	756	1.77 280	9.99 994	3 2	.3 235 226 219 .4 313 302 293
<u>59</u>	8.23 456 8.24 186	.743	8.23 462	742 730	1.76 538	9.99 994	- <u>1</u>	·5 391 377 365
						9·99 993	_	The Pite
<u> </u>	L. Cos.	d.	L. Cotg.	c. d.	L. Tang.	L. Sin.	,	Prop. Pts.
					89°			

					1°			-			
,	L. Sin.	d.	L. Tang.	c. d.	L. Cotg.	L. Cos.			Prop	. Pts	
0	8.24 186	717	8.24 192	718	1.75 808	9.99 993	60				· ·
1 2	8.24 903 8.25 609	706	8.24 910 8.25 616	706	1.75 090	9.99 993	59 58		717	695	673
3	8.26 304	695	8.26 312	696	I.74 384 I.73 688	9.99 993 9 99 993	50 57	.1 .2	71.7	69.5 139.0	67.3
4	8.26 588	684	8.26 996	684	1.73 004	9.99 992	56	.3	215.1	208.5	201.9
5	8.27 651	673 663	8.27 669	663	1.72 331	9.99 992	55	-4	286.8	278.0	269.2
	8.28 324	653	8.28 332	654	1.71 668	9.99 992	54	-5	358.5	347 - 5	336.5
7 8	8.28 977 8.29 621	644	8.28 986 8.29 629	643	1.71 014	9.99 992	53	١,	653	634	616
9	8.30 255	634	8.30 263	634	1.70 371	9.99 992 9.99 991	52 51	.1	65.3	63.4	61.6
10	8.30 879	624	8.30 888	625	1.69 112	9.99 991	50	.2	130.6	126.8	123.2
11	8 31 495	616 608	8.31 505	617	1.68 495	9.99 991	40	-3	195.9	190.2	184.8
12	8.32 103	599	8.32 112	599	1.67 888	9.99 990	48	·4 ·5	261.2 326.5	253.6	246.4 308.0
13 14	8.32 702 8.33 292	590	8.32 711 8.33 302	59I	1.66 698	9.99 990	47		3-5.31	3-7.01	302.1
	8.33 875	583	8.33 886	584	1.66 114	9.99 990	40		599	583	568
15 16	8.34 450	575	8.34 461	575	1.65 539	9.99 990 9.99 989	45 44	.1	59.9	58.3	56.8
17.	8.35 018	568 560	8.35 029	568	1.64 971	9.99 989	43	.2 .3	179.7	116.6	113.6
18	8 35 578	553	8.35 590	561 553	1.64 410	9.99 989	42	.4	239.6	233.2	227.2
<u>19</u>	8.36 131	547	8.36 143	546	1.63 857	9.99 989	41	.5	299.5	291.5	284.0
2U 2I	8.36 678 8.37 217	539	8.36 689 8.37 229	540	1.63 311	9.99 988	40			1	
22	8.37 750	533	8.37 762	533	1.62 771	9.99 988 9.99 988	39 38	.1	553	539	526 52.6
23	8.37 750 8.38 276	526	8.37 762 8.38 289	527	1.61 711	9.99 987	37	.2	55·3 110.6	53·9 107.8	105.2
24	0.30 790	520 514	8.38 809	529 514	1.61 191	9.99 987	36	.3	165.9	161.7	157.8
25	8.39 310	508	8 39 323	509	1.60 677	9 99 987	35	-4	221.2	215.6	210.4
26	8.39 818	502	8.39 832	502	1.60 168	9.99 986	34	-5	276.5	269.5	263.0
27 28	8.40 320 8.40 816	496	8.40 334 8.40 830	496	1.59 666	9.99 986 9.99 986	33 32		514	502	490
29	8.41 307	491	8.41 321	491	1.58 679	9.99 985	31	. 1	51.4	50.2	49
80	8.41 792	485	8.41 807	486	1.58 193	9.99 985	30	.2	102.8	100.4	98
31	8.42 272	480	8.42 287	480	1.57 713	9.99 983	29	-3	154.2	150.6	147
32	8.42 746	474 470	8.42 762	475 470	1.57 238	9.99 984	28	.4	205.6	200.8	196
33 34	8.43 216 8.43 680	464	8.43 232 8.43 696	464	1.56 768	9.99 984	27 26	.5	-37.0	251.0	245
35	8.44 139	459	8.44 156	460	1.55 844	9.99 984	25		480	470	460
36	8.44 594	455	8.44 611	455	1.55 389	9.99 983	24	.1	48	47	46
37 38	8.45 044	450	8.45 061	450	1.54 939	9.99 983	23	.2	96	94	92
38	8.45 489	445 441	8.45 507	446 441	1.54 493	9.99 982	22	·3	144	141	138
39 <b>40</b>	8.45 930	436	8.45 948	437	1.54 052	9.99 982	21	.5	240	235	230
4I	8.46 366 8.46 799	433	8.46 38 <del>3</del> 8.46 817	432	1.53 615	9.99 982 9.99 981	20 19	١.			400
42	8.47 226	427	8.47 245	428	1.52 755	9.99 981	18	١.١	450	440	430
43	8.47 650	424	8.47 669	424	1.52 331	9.99 981	17	.I	45 90	44 83	43 86
44	8.48 069	419	8 48 089	420 416	1.51 911	9.99 980	16	٠3	135	132	129
45 46	8.48 485	411	8.48 505	412	1.51 495	9.99 980	15	-4	180	176	172
47	8.48 896 8.49 304	408	8.48 917 8.49 325	408	1.51 083	9.99 979 9.99 979	14	.5	225	220	215
47 48	8.49 708	404	8.49 729	404	1.50 271	9.99 979	12		420	410	400
49	8.50 108	400	8 50 130	401	1.49 870	9.99 978	11	.1	42	41	40.
50	8.50 504	396	8.50 527	397	1.49 473	9.99 978	10	.2	84	82	8o
51	8 50 897	393 390	8 50 920	393	1.49 080	9.99 977	8	.3	126 168	164	120 160
52 53	8.51 287 8.51 673	386	8.51 310 8.51 696	386	1.48 690	9.99 977 9.99 977	8	·4 ·5		205	200
54	8.52 055	382	8.52 079	383	1.47 921	9.99 976	7 6				l
	8.52 434	379	8.52 459	380	1.47 541	9.99 976	-5		390	360	370
55 56	8.52 810	376	8.52 83 <del>5</del> 8.53 208	376	1.47 165	9.99 97 <u>5</u>	4	Ι.	39	38	37
1 57	8.53 183	373 369	8.53 208	373 370	1.46 792	9 99 975	3 2	.2	78	76 114	74
58 59	8.53 552 8.53 919	367	8.53 578 8.53 94 <b>3</b>	367	1.46 422	9.99 974	2 I	.4	156	152	148
60	8.54 282	363	8.54 308	363	1.45 692	9.99 974	- <del>i</del>	-5	195	190	185
		-		-					70	. TD4	
<u> </u>	L. Cos.	d.	L. Cotg.	c. a.	L. Tang.	L. Sin.	′		rro	. Pts	<u> </u>
					88°						k.

	2°											
	L. Sin.	d.	L. Tang.	c. d.	L. Cotg.	L. Cos.		]	Pro	p. Pts		
0	8.54 282 8.54 642	360	8.54 308 8.54 669	361	1.45 692	9.99 974	60					
2	8.54 999	357	8.55 027	358	1.45 331	9.99 9 <b>73</b> 9.99 9 <b>73</b>	59 58	.1	3 <b>5</b> 5	<b>35</b> 0 35	3 <b>40</b> 34	
3	8.55 354	355 351	8.55 382	355 352	1.44 618	9.99 972	57	.2	72	70	68	
-	8.55 705 8.56 054	349	8.55 734 8.56 083	349	1.44 266	9.99 972	56	.3	308 144	105 140	102 136	
5 6	8.56 400	346	8.56 429	346	I.43 917 I.43 571	9.99 971 9.99 971	55 54	·4 ·5	180	175	170	
7	8.56 743	343 341	8.56 773	344 341	1.43 227	9.99 970	53	.6	316	210	204	
9	8.57 084 8.57 421	337	8.57 114 8.57 452	338	1.42 886 1.42 548	9.99 970	52 51	·7	252 288	245 280	238 272	
10	8 57 757	336	8 57 788	336	1.42 212	9.99 969	50	.9	324	3×5	306	
11	8.58 089	332	8.58 121	333	1.41 879	9.99 968	49	l	330	320	320	
13	8.58 419 8.58 747	328	8 58 451 8.58 779	328	1.41 549 1.41 221	9.99 968 9.99 967	48 47	.I	33 66	32 64	31 62	
14	8.59 072	325 323	8 59 105	326	1.40 893	9.99 967	46	.3	99	96	93	
15	8.59 395	320	8.59 428	321	1.40 572	9.99 967	45	-4	132	128	124	
16 17	8.59 715 8.60 033	318	8 59 749 8 60 068	319	1.40 251	9.99 966 9.99 966	44 43	.5 .6	165 178	160 192	155 186	
17 18	8.60 349	316	8.60 384	316	1.39 616	9.99 963	42	.7	231	224	217	
19	8.60 662	313	8.60 698	314	1.39 302	9.99 964	41	.8 .9	264 297	256 288	248 279	
20 21	8.60 973 8.61 282	309	8.61 009 8.61 319	310	1.38 991	9.99 964 9.99 963	40	.,	1 300	290	285	
22	8.61 589	307	8.61 626	307	1.38 374	9.99 963	39 38	.1	30	29	28.5	
23	8.61 894 8.62 196	302	8.61 931 8.62 234	303	1.38 069	9.99 962	37	.2	60	58	57.0	
24	8.62 497	301	8.62 535	301	1.37 766	9.99 962	36	·3	120	87 316	85.5 114.0	
26	8.62 793	298	8.62 834	299	1.37 465	9.99 961 9.99 961	35 34	.5	150	<b>14</b> 5	142.5	
27 28	8.63 091	296 294	8.63 131	297 295	1 J6 869	9.99 960	33	.6 .7	180 210	174 203	171.0	
20 29	8.63 385 8.63 678	293	8.63 426 8.63 718	292	1.36 574 1.36 282	9.99 960 9.99 959	32 31	.8	240	232	228.0	
80	8.63 968	290	8.64 009	29 I	1.35 991	9.99.959	80	٠9	270	261	256.5	
31	8.64 256	288 287	8 64 298	289	1.35 702	9.99 958	29	ŀ	280	275	270	
32 33	8.64 543 8.64 827	284	8.64 585 8.64 870	285	1.35 415	9.99 958 9.99 957	28 27	.1	28.0 56.0	27.5 55.0	27.0 54.0	
34	8.65 110	283 281	8.65 154	284 281	1.34 846	9.99 956	26	.3	84.0	82.5	81.0	
35	8.65 391	279	8.65 435	280	1.34 563	9.99 956	25	·4 ·5	112.0	137.5	108.0 135.0	
36 37	8.65 670 8.65 947	277	8.65 715 8.65 993	278	1.34 285	9·99 95 <u>5</u> 9·99 955	24 23	.6	168.0	165.0	162.0	
37 38	8.66 223	276	8.66 269	276	1.33 731	9.99 954	22	.7	196.0	192.5	189.0	
39	8.66 497	274 272	8.66 543	274 273	1.33 457	9.99 954	21	8. و.	224.0 252.0		1	
40 41	8.66 769 8.67 039	270	8.66 816 8.67 087	271	1.33 184	9.99 953	20	١	265	250	255	
42	8.67 308	269 267	8.67 356	269	1.32 644	9.99 952 9.99 952	18	.1	.26.5	.26.0	.25.5	
43	8.67 575 8.67 841	266	8.67 624 8.67 890	268 266	1.32 376	9.99 951	17	.2	.53.0 .79.5	.52.0	.51.0 .76.5	
44 45	8.68 104	263	8.68 154	264	1.32 110	9.99.951	16	·3	106.0	104.0	102.0	
46	8.68 367	263	8 68 417	263	1.31 583	9.99 950	15 14	.5	132.5	130.0	127.5	
47 48	8.68 627 8.68 886	260 259	8.68 678 8.68 938	261 260	1.31 322	9.99 949	13	.6 ∙7	159.0 185.5	156.0	153.0 178.5	
49	8.69 144	258	8.69 196	258	1.31 062	9.99 948 9.99 948	12 11	.8	212.0	208.0	204.0	
50	8.69 400	256	8.69 453	257	1 30 547	9.99.947	10	.9	238.5	234.0	229.5	
51	8.69 654 8.69 907	254 253	8.69 708 8.69 962	255 254	1.30 292	9.99 946	9	.1	.25.0	.24.5	240 .24.0	
52 53	8.70 159	252	8.70 214	252	1.30 038	9.99 946 9.99 94 <del>5</del>		.2	.50.0	.49.0	.48.0	
_54	8.70 409	250 249	8.70 465	251 249	1.29 535	9.99.944	7 6	-3	.75.0	.73.5		
55	8.70 658 8.70 90 <del>5</del>	247	8.70 714	248	1.29 286	9 99 944	5	.5	100.0	198.0	.96.0 120.0	
57	8.71 151	246	8.70 962 8.71 208	246	1.29 038	9.99 943 9.99 942	4	.6	150.0	147.0	144.0	
58	8.71 395	244 243	8.71 453	245	1.28 547	9.99 942	3 2	·7 .8	175.0 200.0	171.5	168.0	
55 56 57 58 59 <b>60</b>	8.71 638 8.71 880	242	8.71 697	243	1.28 303	9.99 94:		.9		220.5		
~			8.71 940		1.28 060	9.99 940	0	<u> </u>				
	L. Cos.	d.	L. Cotg.	c. d.	L. Tang.   87°	L. Sin.	'	<u> </u>	Pro	p. Pts		
					(170					-		

					<b>3</b> °						
,	L. Sin.	d.	L. Tang.	c. d.	L. Cotg.	L. Cos.			Prop	. Pts	
0	8.71 880	240	8.71 940	241	1.28 060	9.99 940	60				
1 2	8.72 120 8.72 359	239	8.72 181 8.72 420	239	1.27 819	9.99 940 9.99 939	59 58		235	234	229
3	8.72 597	238 237	8.72 659	239	1.27 341	9.99 938	57	.1 .2	23.8 47.6	23.4 46.8	22.9 45.8
4	8.72 834	235	8.71 896	237 236	1.27 104	9.99 938	56	•3	71.4	70.2	68.7
5	8.73 o69 8.73 303	234	8.73 132 8.73 366	234	1.26 868 1.26 634	9.99 937	55	·4 ·5	95.2	93.6	91.6 214.5
7 8	8.73 535	232 232	8.73 600	234	1.26 400	9.99 936 9.99 936	54 53	.6	142.8	140.4	137.4
<b>E</b> ! 1	8.73 707	230	8.73 832	232	1 .26 168	9 99 935	52	·7 .8	166.6	163.8	160.3
9 10	8.73 997 8.74 226	229	8.74 063	229	1.25 937	9.99 934	51 50	.9		187.2 210.6	
11	8.74 454	228 226	8.74 521	229	1.25 708	9·99 934 9·99 933			225	220 j	216
12	8.74 680	226	8.74.748	227 226	1.25 252	9.99 932	49 48	.1	22.5	22.0	21.6
13 14	8.74 906 8.75 130	224	8.74 974 8.75 199	225	1.25 026	9.99 932 9.99 931	47 46	.2	45.0 67.5	44.0 66.0	43.2 64.8
15	8.75 353	223	8.75 423	224	1.24 577	9.99 930	45	.4	90.0	88.0	86.4
16	8.75 575	220	8.75 645	222	1.24 355	9 99 929	44	.5	1	110.0	108.o
17	8.75 795 8.76 015	220	8.75 867 8.76 087	220	1.24 133	9.99 929	43	.6 ·7	135.0	132.0	129.6
19	8.76 234	219	8.76 306	219	1 23 913	9.99 928 9.99 927	42 41	.8	180.0	176.0	172.8
20	8.76 451	217	8 76 525	219	1.23 475	9.99 926	40	.9		198.0	• • •
2I 22	8.76 667 8.76 883	216	8.76 742 8.76 958	217	1.23 258	9.99 926	39		212	20.8	204
23	8.77 097	214	8.77 173	215	1.23 042	9.99 92 <del>5</del> 9.99 924	38 37	.I	42.4	41.6	20.4 40.8
24	8.77 310	213	8.77 387	214	1.22 613	9 99 923	36	.3	63.6	62.4	61.2
25	8.77 522	211	8.77 600	213	1.22 400	9 99 923	35	·4 ·5	84.8 206.0	83.2	81.6 102.0
26 27	8.77 733 8.77 943	210	8.77 SII 8:78 022	211	1.22 189	9.99 922 9.99 921	34	.6		124.8	122.4
27 28	8.78 152	209	8.78 232	210	1.21 768	9 99 920	33 32	.7		145.6	142.8
29	8.78 360	208	8.78 441	209	1.21 559	9.99 920	31	.8		166.4 187.2	163.2
30 34	8.78 568 8.78 774	206	8.78 649 8.78 855	206	1.21 351 1 21 145	9.99 919	30		20I	197	193
32	8.78 979	205 204	8.79 061	205	1.20 939	9.99 917	29 28	.1	20.1	19.7	19.3
33	8.79 183	203	8.79 266	205	I .20 734	9 99 917	27	.2	40.2 60.3	39 4	38.6
34	8.79 386	202	8.79 470	203	1.20 530	9.99 916	26	·3	80.4	59.1 78.8	57·9 77·2
36	8.79 789	201	8 79 875	202	1.20 327	9.99 915	25 24	-5	100.5	98.5	96.5
37 38	8.79 990 8.80 189	199	8 %o o 76	201 201	1.19 924	9.99 913	23	.6 .7		118.2	115.8
39	8.80 388	199	8 80 277 8 80 476	199	I . 19 723 I . 19 524	9.99 913	22 21	.8	160.8	157.6	154.4
40	8.80 585	197	8.80 674	198	1.19 326	9.99 911	20	.9		±77·3	173.7
41	8.80 782 8.80 978	197 196	8.80 872	198 196	1.19 128	9:99 910	19		18.9	185	181
42 43	8.81 173	195	8.81 068 8.81 264	196	1.18 932 1.18 736	9.99 909	18	.1	37.8	37.0	36.2
44	8.81 367	194	8.81 459	195	1.18 541	9.99 909	17	-3	56.7	55 - 5	54 - 3
45	8.81 560	193	8.81 653	194	1.18 347	9 99 907	15	·4 ·5	75.6 94.5	74.0	72·4 90·5
46 47	8.81 752 8.81 944	192	8 81 846 8 82 038	193 192	1.18 154	9.99 906 9.99 905	14	.6	113.4	111.0	108.6
48	8.82 134	190	8.82 230	192	1.17 770	9.99 904	13 12	.7		129.5 148.0	126.7
49	8 82 324	189	8.82 420	190	1.17 580	9 99 904	11	.9		166.5	
50 51	8.82 513 8.82 701	188	8.82 610 8.82 799	189	1.17 390	9.99 903	10			3   2	
52	8.82 888	187	8.82 987	188	1.17 201	9.99 902 9.99 901	9	,1	0.4 0	.з о.	
53	8.83 075	187 186	8.83 175	188	1.16 825	9.99 900	7 6	.2 .3		.6 o. .9 o.	
54	8.83 261 8.83 446	185	8.83 361 8.83 547	186	1.16 639	9.99 899		.4	1 .1	.2 0.	- 1
55 56	8.83 630	184	8.83 732	185	1.16 268	9.99 898	5	-5		.5 1.	
57 58	8.83 813	183 183	8.83 916	184 184	1.16 084	9.99 897	3	.6 •7	1 1	.8 I.	
58 59	8.83 996 8.84 177	181	8.84 100 8.84 282	182	1.15 900	9.99 896 9.99 89 <del>5</del>	2 I	.8	3.2 2	.4 1.	6 0.8
60	8.84 358	181	8.84 464	182	1.15 536	9.99 894	Û	.9	3.6 2	.7 1.	<b>8 0</b> .9
	L. Cos.	d.		c. d.		L. Sin.	<u> </u>	_	Prop	Die	
II—	, ,		5000	, J. W.	86°	D. But.		<u> </u>	I FUP	18	<u> </u>
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,	L. Sin.	d.	L. Tang.	c. d.	L. Cotg.	L. Cos.			Prop	. Pts	
0	8.84 358	181	8.84 464	182	1.15 536	9.99 894	60				
1 2	8.84 539	179	8.84 646 8.84 826	180	1.15 554	9.99 893 9.99 892	59 58		181	179	177
3	8.84 718 8.84 897	179	8.85 006	180	I . I 5 I 74 I . I 4 994	9.99.891	57	.I	18.1 36.2	35.8	17.7 35.4
4	8.85 075	178 177	8.85 183	179	1.14 815	9.99891	56	.3	54.3	53.7	53.1
5	8.85 252	177	8.85 363	177	1.14 637	0.00 800	55	-4	72.4	71.6	70.8
	8.85 429 8.85 605	176	8.85 540 8.85 717	177	1.14 460	9.99 889	54	.5 .6	108.6	89.5	88.5 106.2
7 8	8.85 780	175	8.85 893	176	I.14 283 I.14 107	9.99 888 9.99 887	53 52	.7		125.3	123.9
9	8.85 953	175	8.86 069	176	1.13 931	9.99 886	51	.8		143.2	141.6
10	8.86 128	173 173	8.86 243	174	1.13 757	9.99 885	50	.9	• •:	161.1	
II I2	8.86 301 8.86 474	173	8.86 417	174	1.13 583	9.99 884	49		175	173	171
13	8.86 645	171	8.86 591 8.86 763	172	1.13 409 1.13 23 <u>7</u>	9.99 883 9.99 882	48 47	.I .2	17.5 35.0	17.3 34.6	17.1 34.2
14	8.86 816	171	8.86 935	172	1.13 065	9.99 881	46	.3	52.5	51.9	51.3
15	8.86 987	171	8.87 106	171	1.12 894	9.99 880	45	-4	70.0	69.2	68.4
16	8.87 156	169	8 87 277	171	1.12 723	9 99 879	44	.5	87.5	86.5	85.5
17	8.87 325 8.87 494	169	8.87 447 8.87 616	169	1.12 553	9 99 879	43	.6	105.0	103.8	102.6
19	8.87 661	167	8.87 783	169	1.12 384	9.99 878 9.99 877	42 41	.8		138.4	136.8
20	8.87 829	168	8.87 953	168	1.12 047	9.99 876	40	.9	157.5	₹55.7	153.9
21	8.87 995	166 166	8.88 120	167	1.11 880	9.99 875			168	x66	164
22	8.88 161	165	8 88 287	167 166	1.11 713	9 99 874	39 38	.1	.16.8	16.6	16.4
23 24	8.88 326 8.88 490	164	8.88 453 8.88 618	165	1.11 547	9.99 873 9.99 872	37	.2	33.6 50.4	33.2 49.8	32.8 49.2
	8.88 654	164	8.88 783	165	1.11 217	9.99.871	36	4	67.2	66.4	65.6
25 26	8.88 817	163	8.88 948	165	1.11 052	9.99.870	35 34	٠5	84.0	83.0	82 o
27 28	8.88 980	163 162	111 08.8	163	1.10 889	9.99.869	33	.6	100.8	99.6	98.4
28 29	8 89 142	162	8.89 274	163 163	1.10 726	9.99 868	32	·7 .8	117.6	116.2	114.8
80	8.89 304 8.89 464	160	8.89 437	161	1.10 563	9.99.867	31	.9	151.2	149.4	147.6
31	8.89 625	161	8 89 598 8 89 760	162	1.10 402 1.10 240	9.99 866 9.99 863	<b>80</b> 29		162	159	157
32	8.89 784	159	8.89 920	160	1.10 080	9.99 864	28	. т	16.2	15.9	15.7
33	8.89 943	159	8.90 080	160 160	1.09 920	9.99 863	27	.2	32.4	31.8	3= -4
34	8.90 102	158	8.90 240	159	1.09 760	9.99 862	26	·3	48.6 64.8	47·7 63.6	47.1 62.8
35 36	8.90 260 8.90 417	157	8.90 399 8.90 557	158	1.09 601	9.99 861 9.99 860	25	-5	81.0	79.5	78.5
37	8.90 574	157	8.90 715	158	1.09 285	9.99 859	24 23	.6	97.2	95-4	94.2
37 38	8.90 730 8.90 885	156 155	8.90 872	157	1.09 128	9.99 858	22	.7 .8	113.4	111.3	109.9
39		155	8.91 029	157	1.08 971	. 9 . 99 857	21	.9	129.6	143.1	125.6 141.3
40 41	8.91 040 8.91 19 <del>5</del>	155	8.91 183	155	1.08 815	9.99 856	20	,	155	153	151
42	8.91 349	154	8.91 340 8.91 495	155	1.08 503	9.99 855	19	. 1	15.5	15.3	15.1
43	8.91 502	153	8.91 630	155	1.08 350	9.99 853	17	.2	31.0	30.6	30.2
44	8.91 655	153	8.91 803	153 154	1.08 197	9.99 852	16	.3	46.5	45.9	45.3
45 46	8.91 807	152	8.91 957	153	1.08 043	9.99 851	15	·4 ·5	77·5	61.2 76.5	60.4 75.5
	8.91 959 8.92 110	151	8.92 110 8.92 262	152	1.07 890 1.07 738	9.99 850 9.99 848	14	.6	93.0	91.8	90.6
47 48	8.92 261	151	8.92 414	152	1.07 586	9.99 847	13	.7		107.1	105.7
49	8.92 411	150 150	8.92 563	151	1.07 435	9.99 846	11	.8	124.0	122.4	120.8
50	8.92 561	149	8.92 716 8.92 866	151	1.07 284	9.99 845	10	.9		137 - 7	
51 52	8.92 710 8.92 859	149	8.92.866	150 150	1.07 134 1.06 984	9.99 844	9	.1	149 14.9	147	I 0.1
53	8.93 007	148	8.93 016 8.93 163	149	1.06 835	9.99 843 9.99 842	8	.2	29.8	14.7 29.4	0.2
54	8.93 154	147	8.93 313	148	1.06 687	9.99 841	7 6	.3	44.7	44.I	0.3
	8.93 301	147	8.93 462	149	1.06 538	9.99 840		-4	59.6	58.8	0 4
55 56 57 58 59	8.93 448	147	8 93 609	147	1.06 391	9.99 839	5 4	.5 .6	74·5 89·4	73·5 88.2	o.5 o.6
5%	8.93 594 8.93 740	146	8.93 756 8.93 903	147	I.06 244 I.06 097	9.99 838	3	.7	104.3	102.9	0.7
59	8.93 885	145	8.94 049	146	1.05 951	9.99 837 9.99 836	3 2 1	.8	119.2	117.6	0.8
60	8.94 030	145	8.94 195	146	1.05 805	9.99 834	<u> </u>	.9	134.1	132.3	0.9
	L. Cos.	d.		c. d.	L. Tang.	L. Sin.	<u>,</u>	<u> </u>	Prop	D4-	
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,	L. Sin.	d.	L. Tang.	c. d.	L. Cotg.	L. Cos.			Pro	p. Pts	3.
0	8.94 030	144 .	8.94 195	145	1.05 803	9.99 834	60				
I 2	8.94 174 8.94 317	143	8.94 340 8.94 485	145	1.05 660	9.99 833 9.99 832	59 58		145	143	141
3	8.94 461	144	8.94 630	145	1.05 370	9.99831	57	.I	#4.5 #9.0	14.3 28.6	14.1 28.2
4	8.94 603	142	8.94 773	143 144	1.05 227	9.99 830	57 56	-3	43.5	42.9	42.3
5	8.94 746 8.94 887	141	8.94 917 8.95 060	143	1.05 083	9.99 829	55	·4 ·5	58.0 72.5	57.2 71.5	56.4 70. <b>5</b>
7 8	8.95 029	142	8.95 202	142	1.04 940	9.99 828 9.99 827	54 53	.6	87.0	85.8	84.6
	8.95 170	141	8.95 344	142	1.04.656	9.99 825	52	.7	101.5	100.1	98.9
9 10	8.95 310	140	8.95 486	141	1.04 514	9.99 824	51	.8	116.0 130.5	114.4	112.8
11	8.95 4 <u>5</u> 0 8.95 589	139	8.95 627 8.95 767	140	I.04 373 I.04 233	9.99 823 9.99 822	<b>50</b> 49	ĺ .	339	138	136
12	8.95 728	139	8.95 908	141	1.04 092	9.99 821	48	.1	13.9	13.8	13.6
13	8.95 867 8.96 005	138	8.96 047 8.96 187	139	1.03 953	9.99 820	47	.2	27.8	27.6	27.2
14	8.96 143	138	8.96 325	138	1.03 813	9.99 819	46	·3	41.7 55.6	41.4 55.2	40.8 54·4
16	8.96 280	137	8.96 464	139	1.03 536	9.99 816	45 44	∙5	69.5	69.0	68.o
17 18	8.96 417	137 136	8.96 602	138	1.03 398	9.99 815	43	.6	83.4	82.8 96.6	81.6
18	8.96 553 8.96 689	136	8.96 739 8.96 877	138	1.03 261	9.99 814 9.99 813	42 41	.7 .8	97·3	110.4	95.2 108.8
20	8.96 825	136	8.97 013	136	1.02 987	9.99 812	40	.9	125.1	: 24 . 2	122.4
21	8.96 960	135 135	8.97 130	137	1.02 850	9.99810	39 38		135	133	131
22 23	8.97 09 <del>5</del> 8.97 229	134	8.97 285 8.97 421	136	1.02 715	9.99 809 9.99 808	38	.1	13.5 27.0	13.3 26.6	13.1 26.2
24	8.97 363	134	8.97 556	135	1.02 444	9.99 807	37 36	.3	40.5	39.9	39.3
25	8.97 496	133	8.97 691	135	1.02 309	9.99 806	35	-4	54.0	53.2	52.4
26	8.97 629	133	8.97 825	134	1.02 175	9.99 804	34	.5 .6	67.5 81.0	66.5 79.8	65.5 78.6
27	8.97 762 8.97 894	132	8.97 959 8.98 092	133	1.02 041	9.99 803 9.99 802	33 32	.7	94.5	93.1	91.7
29	8.98 026	132	8.98 225	133	1.01 773	9.99801	31	.8	108.0	ro6.4	104.8
80	8.98 157	131	8.98 358	133	1.01 642	9.99 800	80	.9	121.5	128	117.9
31 32	8.98 288 8.98 419	131	8.98 490 8.98 622	132	1.01 510	9.99 798 9.99 797	29 28	.1	129	12.8	12.6
33	8.98 549	130	8.98 753 8.98 884	131	I.OI 247	9.99 796	27	.2	25.8	25.6	25.2
34	8 98 679	130		131	1.01 116	9.99 795	26	.3	38.7 51.6	38.4 51.2	37.8 50.4
35 36	8.98 808 8.98 937	129	8.99 01 <del>5</del> 8.99 145	130	1.00 985	9.99 793	25	·4 ·5	64.5	64.0	63.0
37	8.99 066	129	8.99 275	130	1.00 725	9.99 792 9.99 791	24 23	.6	77 - 4	76.8	75.6
37 38	8.99 194	128	8.99 405	130	1.00 595	9.99 790	22	·7 .8	90.3 103.2	89.6 :02.4	88.9
39 40	8.99 322	128	8.99 534	128	1.00 466	9.99 788	21	.9	116.1	:15.2	113.4
41	8.99 4 <del>5</del> 0 8.99 577	127	8.99 662 8.99 791	129	1.00 338	9.99 787 9.99 786	20 19		125	123	122
42	8.99 704	127 126	8.99 919	128	1.00 081	9.99 783	18	.ı	12.5	12.3	12.2
43	8.99 830 8.99 956	126	9.00 046	127	0.99 954	9.99 783	17 16	.2	25.0 37.5	24.6 36.9	24.4 36.6
44 45	9.90 082	126	9.00 174	127	0.99 699	9.99 782	15	.4	50.0	49.2	48.8
46	9.00 207	125	9.00 327	126	0.99 573	9.99 780	14	.5 .6	62.5	61.5	61.0
47 48	9.00 332	125	9.00 553	126 126	0.99 447	9.99 778	13	.7	75.0 87.5	73.8 86.1	73.2 85.4
46 49	9.00 456 9.00 581	125	9.00 679 9.00 80 <u>5</u>	126	0.99 321	9·99·777 9·99·776	I2 II	.8	100.0	98.4	97.6
50	9.00 704	123	9.00 930	125	0.99 070	9.99 775	10	.9	112.5	-10.7	109.8
51	9.00 828	124	9.01.055	125	0.98 945	9.99 773	9		121	120	0.1
52 52	9.00 951 9.01 074	123	9.01 179 9.01 303	124	0.98 821	9.99 772 9.99 771	8	.I .2	24.2	24.0	0.2
52 53 <u>54</u>	9.01 196	122	9.01 427	124	0.98 573	9.99 769	7 6	-3	36.3	36.0	0.3
55	9.01 318	122	9.01 550	123	0.98 450	9.99 768	5	·4 ·5	48.4 60.5	48.0 60.0	0.4
56	9.01 440 9.01 561	121	9.01 673	123	0.98 327	9.99 767	4 3 2	.6	72.6	72.0	0.6
55 56 57 58	9.01 682	121	9.01 796 9.01 918	122	0.98 204	9 99 765 9 99 764	3	.7	84.7	84.0	0.7
59	9.01 803	121	9.02 040	122	0.97 960	9.99 763	1	.8 .9	96.8 108.9	96.0	0.8
60	9.01 923		9.02 162		0.97 838	9.99 761	9		. /		
	L. Cos.	d.	L. Cotg.	c. d.		L. Sin.	,		Pro	. Pts	•
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<b>_</b>	L. Sin.	d.	L. Tang.	c. d.	L. Cotg.	L. Cos.			Prop	• Pts	
0	9.01 923	120	9.02 162	121	0.97 838	9.99 761	60				
I 2	9.02 043 9.02 163	120	9.02 283 9.02 404	121	0.97 717	9.99 760 9.99 759	59 58		121	12.0	11.9
3	9.02 283	120	9.02 525	121	0.97 475	9.99 757	57	.2	24.2	24.0	23.8
4	9.02 402	119	9 02 645	131	0.97 355	9.99 756	56	-3	36.3	36.0	35.7
5	9.02 520	119	9.02 766 9.02 885	119	0.97 234	9.99 755	55	·4 ·5	48.4 60.5	48.0 60.0	47.6 59·5
7 8	9.02 639	118	9.03 005	120	0.97 115	9·99 753 9·99 752	54 53	.6	72.6	72.0	71.4
	9.02 874	117	9.03 124	119	0.96 876	9.99 751	52	.7	84.7	84.0	83.3
9 10	9.02 992	217	9.03 242	119	0.96 758	9.99 749	51	.8 .9	96.8 108.9	96.0 108.0	95.2 107.1
111	9.03 109 9.03 226	117	9.03 361 9.03 479	118	0.96 639 0.96 521	9.99 748     9.99 747	50 40	ĺ	118	117	116
12	9.03 342	116	9.03 597	118	0.96 403	9.99 745	49 48	.x	11.8	11.7	<b>fi</b> .6
13	9.03 458	116	9.03 714	118	0.96 286	9.99 744	47	.8	23.6	23.4	23.2
14	9.03 574	116	9.03 832	116	0.96 168	9.99 742 9.99 741	46 45	·3	35·4 47·2	35.1 46.8	34.8 46.4
16	9.03 805	115	9.03 940	117	0.95 935	9.99 740	44	.5	59.0	58.5	58.o
17 18	9.03 920	115	9.04 181	116	0.95 819	9.99 738	43	.6	70.8 82.6	70.2	69.6
18	9.04.034 9.04.149	115	9.04 297 9.04 413	116	0.95 703	9.99.737	42 41	·7	94.4	81.9 93.6	81.2 92.8
20	9.04.262	113	9.04 528	115	0.95 472	9.99 736 9.99 734	40	.9	206.2	105.3	104.4
21	9.04 376	114	9.04 643	115	0.95 357	9.99 733	39 38	1	115	114	113
22	9.04.490	114	9.04 758	115	0.95 242	9.99 731		.1	11.5	22.8	11.3 22.6
23 24	9.04.603	112	9.04.873 9.04.987	114	0.95 127	9.99 730 9.99 728	37 36	.2 .3	23.0 34.5	34.2	33.9
25	9.04 828	113	9.05 101	114	0.94 899	9.99 727	35	-4	46.0	45.6	45.2
26	9.04.940	112	9.05 214	113	0.94 786	9.99 726	34	.5 .6	57·5 69.0	57.0 68.4	56.5 67.8
27 28	9.05 052 9.05 164	112	9.05 328	113	0.94 672	9.99 724	33	.7	80.5	79.8	79.1
29	9.05 275	222	9.05 44 <b>1</b> 9.05 553	112	0.94 447	9.99 723 9.99 721	32 31	.8	92.0	91.2	90.4
80	9.05 386	111	9.05 666	113	0.94 334	9.99 720	80	.9	103.5	103.6	101.7
31	9.05 497	111	9.05 778	112	0.94 222	9.99 718	29 28	.1	112	111	110 11.0
32 33	9.05 607	110	9.05 890 9.06 002	112	0.94 110	9.99 717 9.99 716	20 27	.2	22.4	22.2	22.0
34	9.05 827	110	9.06 113	111	0.93 887	9.99 714	26	٠3	33.6	33.3	33.0
35 36	9.05 937	110	9.06 224	111	0.93 776	9.99 713	25	-4	44.8 56.0	44·4 55·5	44.0 55.0
36	9.06 046	109	9.06 33 <del>5</del> 9.06 445	110	0.93 665	9.99 711	24	.5 .6	67.2	66.6	66'.o
37 38	9.06 264	109	9.06 556	111	0.93 555	9.99 710 9.99 708	22	.7	78.4	77.7	77.0
39	9.06 372	108	9.06 666	100	0.93 334	9.99 707	21	.8 .9	89.6 100.8	88.8 99.9	88.a 99.a
40	9.06 481	108	9.06 775 9.06 883	110	0.93 225	9.99 705	20		109	108 I	107
4I 42	9.06 589	107	9.00 885	109	0.93 115	9 99 704 9 99 702	19 18	.1	10.9	8.or	10.7
43	9.06 804	108	9.07 103	109	0 92 897	9.99 701	17	.2	21.8	21.6	21.4
44	9.06 911	107	9.07 211	100	0.92 789	9.99 699	16	·3 ·4	32.7 43.6	32.4 43.2	32.1 42.8
45 46	9.07 018	106	9.07 320	108	0.92 680	9.99 698 9.99 696	15 14	٠5	54 - 5	54.0	53.5
47 48	9.07 231	107	9.07 536	108	0.92 464	9.99 693	13	.6	65.4 76.3	64.8	64.2
	9.07 337	106	9.07 643	107	0.92 357	9.99 693	12	·7 .8	87.2	75.6 86.4	74·9 85.6
49 <b>50</b>	9.07 442	106	9.07 751	107	0.92 249	9.99 692	10	و.	98.1	97.2	96.3
51	9.07 548	105	9.07.964	106	0.92 142	9.99 690 9.99 689	ര	1	106	105	204
52	9 07 653 9 07 758 9 07 863	105	9.08 071	107	0.91 929	9.99 687	8	.1	10.6	10.5	
53	9.07 863 9.07 968	105	9.08 177 9.08 283	106	0.91 823	9.99 686 9.99 684	7 6	.2 .3	21.2 31.8	21.0 31.5	90.8 31.2
54	9.07 908	104	9.08 283	106	0.91 717	9.99 683		-4	42.4	42.0	41.6
56	9.08 176	104	9.08 493	106	0.91 505	9.99 681	5 4	.5 .6	53.0 63.6	52.5 63.0	52.0 62.4
57	9.08 280	104	9 08 600	105	0.91 400	9 99 680	3 2	.7	74.2	73.5	72.8
55 56 57 58 59	9.08 383 9.08 486	103	9.08 705	105	0.91 295	9.99 678	2   I	.8	84.8		83.2
60	9.08 589	103	9.08 914	104	0.91 086	9.99 675	0	.9	95.4	94-5	93.6
	L. Cos.	d.	L. Cotg.	c. d.			7	<b> </b>	Pro	p. Pts	
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					<b>7</b> °			
	L. Sin.	d.	L. Tang.	e. d.	L. Cotg.	L. Cos.		Prop. Pts.
0	9.08 589	103	9.08 914	105	0.91 086	9.99 675	60	
1 2	9.08 692 9.08 795	103	9.09 019 9.09 123	104	0.90 981 0.90 877	9.99 674 9.99 672	59 58	.I 10.5 10.4 10.3
3	9.08 897	103	9.09 227	104	0.90 773	9.99670	57	.2 21.0 20.8 20.6
4	9 08 999	109	9.09 330	104	0.90 670	9.99 669	56	-3 31.5 31.2 30.9
5	9.09 IOI 9.09 202	101	9.09 434 9.09 537	103	0.90 566	9.99 667 9.99 666	55 54	.4 42.0 41.6 41.2 .5 52.5 52.0 51.5
7 8	9.09 304	102	9.09 640	103	0.90 360	9.99 664	53	.6 63.0 62.4 61.8
9	9.09 403	101	9.09.742 9.09.843	103	0.90 258	9.99 663 9.99 661	52	7 73.5 72.8 72.1 .8 84.0 83.2 82.4
10	9.09 506	100	9.09.043	102	0.90 053	9.99 659	50	.9 94.5 93.6 92.7
31	9.09 707	101	9.10 049	101	0.89 951	9.99 658	49 48	103 101 100
12 13	9.09.807	100	9.10 150	102	0.89 850	9.99 656 9.99 653		.1 10.2 10.1 10.0
14	9.10 006	.99	9.10 252 9.10 353	101	0.89 647	9.99 653	47 46	.2 20.4 20.2 20.0 .3 30.6 30.3 30.0
15	9.10 106	100	9.10454	101	0.89 546	9.99 651	45	.4 40.8 40.4 40.0
16	9.10 205	99 99	9.10 555	101	0.89 445	9 99 650	44	.5 51.0 50.5 50.0 .6 61.2 60.6 60.0
17 18	9.10 304 9.10 402	98	9.10 656 9.10 756	100	0.89 344	9.99 648 9.99 647	43 42	.7 71.4 70.7 70.0
19	9.10 501	99 98	9.10856	100	0.89 144	9.99 643	41	.8 81.6 80.8 80.0
20	9. 10 599	98	9.10956	100	0.89 044	9.99 643	40	.9  91.8  90.9  90.0
2I 22	9.10 697 9.10 795	98	9.11 056 9.11 155	99	0.88 944	9.99 642 9.99 640	39 38	.I 9.9 98
23	9.10893	98 97	9.11 254	99	0.88 746	9.99638	37	.2 19.8 19.6
24	9.10 990	97	9.11 353	.99	0.88 647	9 99 637	36	.3 29.7 29.4 .4 39.6 39.2
25 26	9.11 087 9.11 184	97	9.11 452 9.11 551	99	0.88 548	9.99 635	35	.5140.5140.0
27	9.11 281	97 96	9.11 649	98	0.88 351	9.99 632	34 33	.6  59.4  58.8
28	9.11 377	97	9.11 747	98 98	0.88 253	9 99 630	32	.7 69.3 68.6 .8 79.2 78.4
29 <b>80</b>	9.11 474 9.11 570	96	9.11 845	98	0.88 155	9.99.629	$\frac{31}{80}$	.9 89.1 88.2
31	9.11 666	96	9.11 543	97	0.87 960	9.99 625	29	97   96   95
32	9.11 761	95 96	9.12 138	98	0.87862	9 99 624	28	.I 9.7 9.6 9.5
33 34	9.11 857 9.11 952	95	9.12 23 <del>5</del> 9.12 332	97	0.87 765	9.99 622 9.99 620	27 26	.2 19.4 19.2 19.0 .3 29.1 28.8 28.5
35	9.12 047	95	9.12 428	96	0 87 572	9.99 618	25	.4 38.8 38.4 38.0
36	9.12 142	95 94	9.12.525	97 96	0.87 475	9.99617	24	.5 48.5 48.0 47.5 .6 58.2 57.6 57.0
37 38	9.12 236 9.12 331	95	9.12 621 9.12 717	96	0.87 379	9.99 615	23 22	.7 67.9 67.2 66.5
39	9.12 425	94	9.12 813	96	0.87 187	9.99 612	21	.8  77.6  76.8  76.0
40	9.12 519	94 93	9.12 909	96	0.87 091	9.99 610	20	.9  87.3  86.4  85.5
41 42	9.12 612 9.12 706	94	9.13 004	95 95	o.86 996 o.86 901	9.99 608 9.99 607	19 18	.I 9.4 9.3 9.2
43	9.12 799	93	9.13 <b>099</b> 9.13 194	95	0.86 806	9.99.605	17	.2 18.8 18.6 18.4
44	9.12 892	93 93	9 13 289	95 95	0.86 711	9.99 603	16	.3 28.2 27.9 27.6 .4 37.6 37.2 36.8
45 46	9.12.985 9.13.078	93	9.13 384	94	0.86 616	9.99 601	15	.5 47.0 46.5 46.0
	9.13 171	93	9 13 478 9 13 573	95	0.86 522	9.99 600	14 13	.6 56.4 55.8 55.2
47 48	9.13 263	92 92	9.13667	94	0.86 333	9.99 596	12	.7 65.8 65.1 64.4 .8 75.2 74.4 73.6
49 <b>50</b>	9.13 355	92	9.13 761	93	0.86 239	9.99 595	11	.8 75.2 74.4 73.6 .9 84.6 83.7 82.8
51	9.13 447 9.13 539	92	9.13 854 9.13 948	94	0.86 052	9.99 593 9.99 591	10	91   90   2
52	9.13 630	91 92	9.14 041	93	0.85 959	9.99 589	9 8	.1 9.1 9.0 0.2 .2 18.2 18.0 0.4
53 54	9.13 722 9.13 813	91	9.14.134 9.14.227	93 93	0.85 866 0.85 773	9.99 588 9.99 586	7 6	.3 27.3 27.0 0.6
	9.13 904	91	9.14.320	93	0.85 680	9.99 584	5	. A 36. A 36.0 0.8
55 56	9.13 994	90 91	9.14.412	92 92	0.85 588	9.99 582	4	.4 36.4 36.0 0.8 .5 45.5 45.0 1.0 .6 54.6 54.0 1.2 .7 63.7 63.0 1.4 .8 72.8 72.0 1.6
57 58	9.14 085 9.14 175	90	9.14.504	93	0.85 496	9.99 581	4 3 2	.6 54.6 54.0 I.2 .7 63.7 63.0 I.4 .8 72.8 72.0 I.6
59	9.14 266	91	9.14 597 9.14 688	91	0.85 403	9.99 579 9.99 577	1	.8 72.8 72.0 1.6 .9 81.9 81.0 1.8
60	9.14 356	90	9.14 780	92	0.85 220	9.99 575	0	.9  81.9  81.0  1.8
	L. Cos.	d.	L. Cotg.	c. d.	L. Tang.	L. Sin.	<b>—</b>	Prop. Pts.
					82°			
L					04			

30	<u> </u>				8°			
,	L. Sin.	d.	L. Tang.	c <b>. d.</b>	L. Cotg.	L. Cos.		Prop. Pts.
0	9.14 356	89	9.14.780 9.14.872	92	0.85 220 0.85 128	9.99 575	60	l an i ar l m
1 2	9. 14 44 <u>5</u> 9. 14 535	90	9.14.6/2 9.14.963	91	0.85 037	9.99 574 9.99 572	59 58	92 91 90 .1 9.2 9.1 9.0
3	9.14 624	89 90	9.15 054	91 91	0.84 946	9.99 570	57	.2 18.4 18.2 18.0
4	9.14 714	89	9.15 145	91	0.84 853	9.99 568	<u>56</u> 55	.3 27.6 27.3 27.0 .4 36.8 36.4 36.0
5	9.14 891	88 89	9.15 327	91 90	0.84 673	9.99 565	54	.5 46 0 45.5 45.0
8	9.14 980 9.15 069	89	9.15 417 9.15 508	91	0.84 583	9.99 563 9.99 561	53 52	.6 55.2 54.6 54.0     .7 64.4 63.7 63.0
9	9.15 157	88 88	9.15 598	90	0.84 402	9 99 559	51	8 73.6 72.8 72.0
10	9.15 245	88	9.15 688	89	0.84 312	9 99 557	50	9 82.8 81.9 81.0   89 88
11	9.15 333 9.15 421	88 87	9.15 777 9.15 867	90	0.84 133	9.99 556 9.99 554	49 48	.1 8.9 8.8
13	9.15 508	88	9.15 956 9.16 046	90	0.84 044	9.99 552	47	.2 17.8 17.6 .3 26 7 26.4
14	9.15 596	87	9.16 135	89	0.83 865	9.99 550	46 45	.4 35.6 35.2
15 16	9.15 770	87 87	9.16 224	89	0.83 776	9.99 546	44	.5 44.5 44.0 .6 53.4 52.8
17	9.15 857 9.15 944	87	9.16 312 9.16 401	89	0.83 688	9·99 54 <del>5</del> 9·99 543	43 42	.6 53.4 52.8 .7 62.3 61.6 .8 71.2 70.4
19	9.16 030	86 86	9.16 489	88 88	0.83 511	9.99 541	41	8 71.2 70.4 .9 80.1 79.2
29	9.16 116	87	9.16 577 9.16 665	88	0.83 423 0.83 335	9.99 539	40	87   86
22	9.16.289	86 85	9.16 753 9.16 841	88 88	0.83 247	9 99 537 9 99 535	<b>3</b> 9 38	.1 8.7 8.6
23 24	9.16 374 9 16 460	86	9.16 841 9.16 928	87	0.83 159	9: 99 533	37 36	.2 17.4 17.2 .3 26.1 25.8
25	9.16 545	85	9.17 016	88	0.82 984	9.99 532	35	.4 34.8 34.4
26	9.16 631	86 8 <sub>5</sub>	9.17 103	8 <sub>7</sub>	0.82 897	9.99 528	34	.5 43.5 43.0 .6 52.2 51.6
27 28	9.16 716 9.16 801	85	9.17 190 9.17 277	87	0.82 810	9.99 <b>526</b> 9.99 <b>524</b>	33 32	7 60.9 60.2
29	9.16 886	85 84	9.17 363	86 8 <sub>7</sub>	0.82 637	9.99 522	31	.8 69.6 68.8 .9 78.3 77.4
80 31	9.16 970 9.17 055	85	9.17 430 9.17 536	86	0.82 550 0.82 464	9.99 520 9.99 518	<b>80</b> <b>2</b> 9	85   84
32	9.17 139	84 84	9.17622	86 86	0.82 378	9.99 517	28	.1 8.5 8.4
33 34	9.17 223 9.17 307	84	9.17 708 9.17 794	86	0.82 292	9.99 515	27 26	.2 17.0 16.8 .3 25.5 25.2
	9.17 391	84	9.17 880	86	0.82 120	9 99 513	25	.4 34.0 33.6
35 36	9.17 474	83 84	9.17 965 9.18 051	8 <sub>5</sub> 86	0.82 035	9.99 509	24	.5 42:5 42.0 .6 51.0 50.4
37 38	9.17 558 9.17 641	83	9.18 136	85	0.81 949 0.81 864	9.99 507 9.99 505	23 22	. 7 59.5 58.8
39	9.17 724	83 83	9.18 221	8 <sub>5</sub>	0.81 779	9.99 503	21	.8 68.0 67.2 .9 76.5 75.6
40 41	9.17 807 9.17 890	83	9.18 306 9.18 391	85	0.81 694 0.81 609	9.99 501 9.99 499	20	83   82
42	9.17 973	83 82	9.18 475	84 85	0.81 525	9.99 497	18	.1 8.3 8.2
43 44	9.18 055 9.18 137	82	9.18 560 9.18 644	84	0.81 440	9 99 495 9 99 494	17	.2 16.6 16.4 .3 24.9 24.6
45 46	9.18 220	83 82	9.18 728	84	0.81 272	9.99 492	15	.4 33.2 32.8
46	9.18 302 9.18 383	81	9.18 812 9.18 896	84 84	0.81 188	9.99.490 9.99.488	14 13	.5 41.5 41.0 .6 49.8 49.2
47 48	9.18465	82 82	9.18 979	83 84	0.81 021	9.99486	12	.7 58.1 57.4 .8 66.4 65.6
49 <b>50</b>	9.18 547 9.18 628	81	9.19 063	84 83	0.80 937	9.99 484	11	.9 74.7 73.8
51	9.18 028	81	9.19146 9.19229	83	0.80 854	9.99.482 9.99.480	10	81   80   2
51 52	9. 18 790 9. 18 871	81 81	9.19 312	83 83	0.80688	9.99 478	8	.1 8.1 8.0 0.2 .2 16.2 16.0 0.4
54	9.18 952	81	9.19 395 9.19 478	83	0.80 603	9.99 476 9.99 474	7 6	.3 24.3 24.0 0.6
53 54 55 56 57 58 59 <b>60</b>	9.19 033	81 80	9.19 561	83 82	0.80 439	9 99 472	5	.4 32.4 32.0 0.8
57	9.19 113 9.19 193	80	9.19 643 9.19 725	82	0.80 357	9 99 470 9 99 <b>4</b> 68	4	.6 48.6 48.0 I.2
58	9.19 273	80 80	9 19 807	82 82	0.80 193	9.99 466	3 2	.7 56.7 56.0 1.4 .8 64.8 64.0 1.6
60	9. 19 353 9. 19 433	80	9.19889	82	0.80 029	9.99 464	<u>1</u>	.9 72.9 72.0 1.8
	L. Cos.	d.		c. d.	L. Tang.	9.99 462 <b>L. Sin.</b>	Ļ	Duon Die
				-U- U-	81°	т. ош.	, ,	Prop. Pts.
					01			

					9°			
,	L. Sin.	d.	L. Tang.	c. d.	L. Cotg.	L. Cos.		Prop. Pts.
0	9.19 433	80	9.19971	82	0.80 029	9.99 462	60	
1 2	9.19 513 9.19 592	79	9.20 053 9.20 134	8z	0.79 947 0.79 866	9.99 460 9.99 458	59 58	82 81 80 .1 8.2 8.1 8.0
3	9.19672	80 79	9.20 216	82	0.79 784	9.99 456	57	2 16.4 16.2 16.0
4	9.19 751	79	9.20 297	81 81	0.79 703	9.99 454	56	.3 24.6 24.3 24.0
5	9.19830	79	9.20 378 9.20 459	8z	0.79 622 0.79 541	9.99 4 <u>5</u> 2 9.99 4 <u>5</u> 0	55	.4 32.8 32.4 32.0 .5 41.0 40.5 40.0
7 8	9.19 988	79	9.20 540	8z	0.79 460	9.99 448	54 53	.6 49 2 48.6 48.0
	9 20 067	79 78	9.20 621	81 80	0.79 379	9.99 446	52	.7 57.4 56.7 56.0 .8 65.6 64.8 64.0
9 10	9.20 145	78	9.20 701	8z	0.79 299	9.99 444	51 50	9 73.8 72.9 72.0
111	9.20 302	79	9.20 862	80	0.79 138	9.99 440	40	79   78
12	9.20 380	78 78	9.20 942	80 80	0.79 058 0.78 978	9.99 438	48	.1 7.9 7.8 .2 15.8 15.6
13 14	9.20 458 9.20 535	77	9.21 022 9.21 102	80	0.78 898	9.99 436 9.99 434	47 46	.2 15.8 15.6 .3 23.7 23.4
15	9.20 613	78	9.21 182	80	0.78 818	9.99 432	45	4 31.6 31.2
16	9.20 691	78 77	9.21 261	79 8o	0.78 739	9.99 429	44	5 39.5 39.0 6 47.4 46.8
17 18	9.20 768 9.20 845	77	9.21 341 9.21 420	79	0.78 659 0.78 580	9.99 427 9.99 425	43 42	
19	9.20 922	77	9.21 499	79	0.78 501	9.99 423	41	
20	9.20 999	77 77	9.21 578	79 79	0.78 422	9.99 421	40	.9  71.1  70.2
2I 22	9.21 076 9.21 153	77	9.21 657 9.21 736	79	0.78 343 0.78 264	9.99 419 9.99 417	39 38	77 76 .1 7.7 7.6
23	9.21 229	76	9.21 814	78	0.78 186	9.99 415	37	.2 15.4 15.2
24	9.21 306	77 76	9.21 893	79 78	0.78 107	9.99 413	36	.3 23.1 22.8 .4 30.8 30.4
25 26	9.21 382 9.21 458	76	9.21 971 9.22 049	78	0.78 029 0.77 951	9.99 411 9.99 409	35 34	.4 30.8 30.4 .5 38.5 38.0
27 28	9.21 534	76	9.22 127	78	0.77 873	9.99 407	33	.6 46.2 45.6
	9.21 610 9.21 685	76 75	9.22 205	78 78	0.77 795	9.99 404	32	.7 53 9 53.2 .8 61.6 60.8
29 80	9.21 761	76	9.22 283	78	0.77 717	9.99 402	31 80	9 69.3 68.4
31	9.21 836	75	9 22 438	77	0.77 562	9.99 398	29	75 74
32	9.21 912	76 75	9.22 516	78 77	0.77 484	9.99 396	28	.I 7.5 7.4 .2 15.0 14.8
33 34	9.21 987	75	9.22 593	77	0.77 407	9.99 394 9.99 392	27 26	.2 15.0 14.8 .3 22.5 22.2
	9.22 137	75	9.22 747	77	0.77 253	9 99 390	25	.4 30.0 29.6
35 36	9.22 211	74 75	9 22 824	77	0.77 176	9.99 388	24	.5 37.5 37.0 .6 45.0 44.4
37 38	9.22 286 9.22 361	75	9.22 901 9.22 977	76	0.77 099	9.99 385 9.99 383	23	.7 52.5 51.8
39_	9.22 435	74	9.23 054	77 76	0.76 946	9.99 381	21	.8 60.0 59.2 .9 67.5 66.6
40	9.22 509	74 74	9.23 130	76	0.76 870	9 99 379	20	73   72
41 42	9.22 583 9.22 657	74	9.23 206 9.23 283	77	0.76 794	9·99 37 <u>7</u> 9·99 375	18	.1 7.3 7.2
43	9.22 731	74	9 23 359	76 76	0.76 641	9 99 372	17	.2 14.6 14.4
44	9.22 805	74 73	9 23 435	76 75	0.76 565	9 99 370	16	.3 21.9 21.6 4 29.2 28.8
45 46	9.22 878 9.22 952	74	9.23 510 9.23 586	76	0.76 490	9.99 368 9.99 366	15 14	5 36.5 36.0
47 48	9.23 025	73	9.23 661	75 76	0.76 339	9.99 364	13	
48 49	9.23 098 9.23 171	73 73	9.23 737 9.23 812	76 75	0.76 263 0.76 188	9.99 362 9.99 359	I2 II	.8 58.4 57.6
50	9.23 244	73	9.23 887	75	0.76 113	9.99 357	10	
51	9.23 317	73	9.23 962	75	0.76 038	9.99 355	9	71 3 2
52 53	9.23 390 9.23 462	73 72	9.24 037 9.24 112	75 75	0.75 963 0.75 888	9.99 353 9.99 351	8	.I 7.I 0.3 0.2 .2 I4.2 0.6 0.4
53 54	9.23 535	73	9.24 186	74	0.75 814	9.99 348	7 6	[ .3  21.3  0.9  0.6
55	9.23 607	72	9.24 261	75	0.75 739	9.99 346	5	.4 28.4 I.2 0.8 .5 35.5 I.5 I.0
55 56 57 58 59	9.23 679	72 73	9.24 335 9.24 410	74 75	0.75 66 <del>3</del> 0.75 590	9.99 344 9.99 342	4	.6 42.6   I.8   I.2
58	9.23 752 9.23 823	71	9.24 484	74	0.75 516	9.99 342	3 2	.7 49 7 2.1 1.4 .8 56.8 2.4 1.6
59	9.23 895	72 72	9.24 558	74 74	0.75 442	9.99 337	1	9 63.9 2.7 1.8
60	9.23 967		9.24 632		0.75 368	9.99 335	0	
<u> </u>	L. Cos.	d.	L. Cotg.	ic. d.		L. Sin.	,	Prop. Pts.
					80°			

	10°											
•	L. Sin.	d.	L. Tang.	c. d.	L. Cotg.	L. Cos.		Prop. Pts.				
ि	9.23 967	72	9.24 632	74	0.75 368	9.99 335	60					
1 2	9.24 039 9.24 IIO	71	9.24 706 9.24 779	73	0.75 294 0.75 221	9.99 333 9.99 331	59 58	74 73				
3	9.24 181	71 72	9.24 853	74	0.75 147	9.99 334	57 57	.1 7.4 7.3 .2 14.8 14.6				
4	9.24 253	71	9.24 926	73 74	0.75 074	9.99 326	56	.3 22.2 21.9				
5	9.24 324 9.24 395	71	9.25 000	73	0.75 000	9.99 324	55	.4 29.6 29.2 5 27 0 26 5				
7 8	9.24 466	71	9.25 146	73	0.74 927 0.74 854	9.99 <b>322</b> 9.99 319	54 53	.5 37.0 36.5 .6 44.4 43.8				
	9.24 536	70 71	9.25 219	73 73	0.74 781	9.99 317	52	.7 51.8 51.1				
9 10	9.24 607	70	9.25 292	73	0.74 708	9.99 315	51	.8 59.2 58.4 .9 66.6 65.7				
111	9.24 677 9.24 748	72	9.25 365	72	0.74 635 0.74 563	9.99 313 9.99 310	<b>50</b>	72   71				
12	9.24 818	70 70	9.25 510	73 72	0.74 490	9.99 308	49 48	.1 7.2 7.1				
13 14	9.24 888 9.24 958	70	9.25 582 9.25 653	73	0.74 418	9.99 306	47	.2 14.4 14.2				
15	9.25 028	70	9.25 727	72	0.74 345	9.99 304 9.99 301	46	.3 21.6 21.3 .4 28.8 28.4				
16	9.25 098	70	9.25 799	72	0.74 201	9.99.299	44	.5 36.0 35.5				
17	9.25 168	7°	9.25 871	72 72	0.74 129	9.99 297	43	.6 43.2 42.6				
19	9.25 237 9.25 307	70	9.25 943 9.26 015	72	0.74 057	9.99 294 9.99 292	42 41	.7 50.4 49.7 .8 57.6 56.8				
20	9.25 376	69	9.26 086	7º	0.73 914	9.99 290	40	.9  64.8  63.9				
21	9.25 445	69 69	9.26 158	72 71	0.73 842	9.99 288	39 38	70 69				
22 23	9.25 514 9.25 583	69	9.26 229 9.26 301	72	0.73 771 c 73 699	9.99 285 9.99 283	38	.1 7.0 6.9 .2 14.0 13.8				
24	9.25 652	69	9.26 372	71	0.73 628	9.99 281	37 36	.3 21.0 20.7				
25 26	9.25 721	69 69	9.26 443	71 71	0.73 557	9.99 278	35	.4 28.0 27.6				
	9.25 790 9.25 858	68	9.26 514 9.26 58 <del>5</del>	771	0.73 486	9.99 276	34	.5 35.0 34.5 .6 42.0 41.4				
27 28	9.25 927	69	9.26 655	70	0.73 415	9.99 274 9.99 271	33 32	.7 49.0 48.3				
29	9.25 995	68 68	9.26 726	71	0.73 274	9.99 269	31					
80	9.26 063	68	9.26 797 9.26 867	70	0.73 203	9.99 267	80	.9   63   62   I   68   67				
31 32	9.26 131 9.26 199	68	9.26 937	70	0.73 133	9.99 264 9.99 262	29 28	.1 6.8 6.7				
33	9.26 267	68 68	9.27 008	7 <sup>1</sup>	0.72 992	9.99 260	27	.2 13.6 13.4				
34	9.26 335	68	9.27 078	70	0.72 922	9.99 257	26	.3 20.4 20.1 .4 27.2 26.8				
35 36	9.26 403 9.26 470	67	9.27 148 9.27 218	70	0.72 852	9.99 255 9.99 252	25 24					
37 38	9 26 538	68 67	9.27 288	70	0.72 712	9.99 250	23	.5 34.0 33.5 .6 40.8 40.2				
38	9.26 605 9.26 672	67	9.27 357	70	0.72 643	9.99 248	22	.7 47.6 46.9 .8 54.4 53.6				
39 40		67	9.27 427	69	0.72 573	9.99 245	21 20	.9 61.2 60.3				
41	9.26 739 9.26 806	67	9.27 566	70	0.72 434	9.99.241	19	66   65				
42	9.26 873	67	9.27 635	69 69	0.72 365	9 99 238	18	.1 6.6 6.5				
43 44	9.26 940	67	9.27 704 9.27 773	69	0.72 296	9.99 236 9.99 233	17 16	.2 13.2 13.0 .3 19.8 19.5				
45 46	9.27 073	66	9.27 842	69	0.72 158	9.99 231	15	.4 26.4 26.0				
46	9.27 140	66	9.27 911	69	0.72 089	9.99 229	14	.5 33.0 32.5 .6 39.6 39.0				
47 48	9.27 206 9.27 273	67	9.27 980	69	0.72 020 0.71 951	9.99 226 9.99 224	13	.7 46.2 45.5				
49	9.27 339	66 66	9.28 117	68 69	0.71 883	9.99 221	11					
50	9.27 403	66	9.28 186	68	0.71 814	9.99 219	10	.9  59.4  58.5   3   2				
51 52	9.27 471 9.27 537	66	9.28 254 9.28 323	69	0.71 746 0.71 677	9.99 217 9.99 214	8					
53	9.27 602	65 66	9.28 391	68	0.71 609	9.99 212	7 6	.2 0.6 0.4				
51	9.27 668	66 66	9.28 459	68 68	0.71 541	9.99 209		.3 0.9 0.6 .4 1.2 0.8				
55 56	9.27 734 9.27 799	65	9.28 527 9.28 595	68	0.71 473 0.71 405	9.99 207	5	.5 I.5 I.0 .6 I.8 I.2				
57	9.27 864	65	9.28 662	67	0.71 338	9.99 204 9.99 202	4	.6 1.8 1.2				
57 58	9.27 930	66 65	9.28 730	68 68	0.71 270	9.99 200	2	.4 I.2 0.8 .5 I.5 I.0 .6 I.8 I.2 .7 2.1 I.4 .8 2.4 I.6				
<u>59</u> <b>60</b>	9.27 995	65	9.28 798	67	0.71 202	9.99 197	1 0	.9 2.7 1.8				
	L. Cos.					9.99 195		Davis TV				
	110 UUS0	d.	L. Cotg.	c. d.	L. Tang.	L. Sin.		Prop. Pts.				
I					79°			-				

	11°											
,	L. Sin.	d.	L. Tang.	c. d.	L. Cotg.	L. Cos.		Prop. Pts.				
0	9.28 060	65	9.28 865	68	0.71 135	9.99 195	60					
I 2	9.28 123	65	9.28 933	67	0.71 067	9.99 192	59 58	.1 6.8 6.7				
3	9.28 254	64 65	9.29 067	67	0.70.933	9.99 187	57	.2 13.6 13.4				
4	9.28 319	65	9.29 134	67	0.70 866	9.99 185	56	.3 20.4 20.1				
5	9.28 384 9.28 448	64	9.29 201 9.29 268	67	0.70 799 0.70 732	9.99 182 9.99 180	55 54	.4 27.2 26.8 .5 34.0 33.5				
7 8	9.28 512	64 65	9.29 335	67	0.70665	9.99 177	53	.6 40.8 40.2				
8	9.28 577 9.28 641	64	9.29 402 9.29 468	66	0.70 598 0.70 532	9.99 175	52 51	.7 47.6 46.9 .8 54.4 53.6				
10	9.28 705	64	9.29 535	67	0.70 465	9.99 172	50	.9 61.2 60.3				
11	9.28 769	64 64	9.29 601	66	0.70 399	9.99 167	49 48	66 65				
12	9.28 833 9.28 896	63	9.29 668	66	0.70 332	9.99 165		.1 6.6 6.5				
14	9.28 960	64	9.29 734 9.29 800	66	0.70 200	9.99 162 9.99 160	47 46	.2 13.2 13.0 .3 19.8 19.5				
15	9.29 024	64 63	9.29 866	66	0.70 134	9.99 157	45	.4 26.4 26.0				
16 17	9.29 087	63	9.29 932	66	0.70 068	9.99 155	44	.5 33.0 32.5 .6 39.6 39.0				
18	9.29 150 9.29 214	64	9.29 998	66	0.69 936	9.99 152 9.99 150	43 42	.7 46.2 45.5				
19.	9.29 277	63 63	9.30 130	66 65	0.69870	9.99 147	41					
20	9.29 340	63	9.30 195	66	0.69 803	9.99 145	40	.9  59.4  58. <b>5</b>   <b>64   63</b>				
2I 22	9.29 403 9.29 466	63	9.30 261 9.30 326	65	0.69 739	9.99 <b>142</b> .9.99 <b>14</b> 0	39 38					
23	9.29 529	63 62	9.30 391	65	0.69 609	9.99 137	37	2 12.8 12.6				
24	9.29 591	63	9.30 457	65	0.69 543	9.99 135	36	3 19.2 18.9 4 25.6 25.2				
25 26	9.29 654 9.29 716	62	9.30 522 9.30 587	65	0.69 478	9.99 132 9.99 130	35 34					
27 28	9.29 779	63 62	9.30 652	65	0.69 348	9.99 127	33	6 38.4 37.8				
28 29	9.29 841	62	9.30 717	65	0.69 283	9.99 124	32	.7 44.8 44.1 .8 51.2 50.4				
80	9.29 903	63	9.30 782 9.30 846	64	0.69 218	9.99 122	31 30	.9 57.6 56.7				
31	9.30 028	.6a	9.30 040	65	0.69 089	9.99 119	29	6a 61				
32	9.30 090	62 -61	9.30 975	64	0.69 025	9.99 114	28	.I 6.2 6.I .2 I2.4 I2.2				
33 34	9.30 151 9.30 213	62	9.31 040 9.31 104	64	o.68 960 o.68 896	9.99 II2 9.99 IO9	27 26	.2 12.4 12.2 .3 18.6 18.3				
35	9.30 275	62	9.31 168	64	0.68 832	9.99 106	25	.4 24.8 24.4				
36	9.30 336	61 62	9.31 233	64	0.68 767	9.99 104	24	.5 31.0 30.5 .6 37.2 36.6				
37 38	9.30 398 9.30 459	бı	9.31 297 9.31 361	64	o.68 703 o.68 639	9.99 101 9.99 099	23 22	.7 43.4 42.7				
39	9.30 521	62 61	9.31 425	64	0.68 575	9.99 096	21					
40	9.30 582	6r	9.31 489	63	0.68 511	9.99 093	20	.9 55.8 54.9   <b>6</b> 0  <b>59</b>				
4I 42	9.30 643 9.30 704	6 <b>1</b>	9.31 552 9.31 616	64	0.68 448	9.99 ogi 9.99 o88	18	1 60 50				
43	9.30 765	6r	9.31 679	63	0.68 321	9.99 086	17	.2 12.0 11.8				
44	9.30 826	61 61	9.31 743	64	0.68 257	9.99 083	16	.3 18.0 17.7 .4 24.0 23.6				
45 46	9.30 887 9.30 947	60	9.31 806 9.31 870	64	0.68 194	9.99 080	15	.5 30.0 29.5				
47 48	9.31 008	6r	9 31 933	63	0.68 067	9.99 078 9.99 075	14 13	.6  36.0  35.4				
	9.31 068	60 61	9.31 996	63	0.68 004	9.99 072	12	.7 42.0 41.3 .8 48.0 47.2				
49 <b>50</b>	9.31 129	60	9.32 059	63	0.67 941	9.99 070	10	.9  54.0  53.1				
51	9.31 250	61 6-	9.32 185	63	0.67813	9.99 007	9	3 3				
52	9.31 310	6e 6o	9.32 248	63 63	0.67 752	9.99 062	8	.1 0.3 0.2 .2 0.6 0.4				
53 54	9.31 370 9.31 430	60	9.32 311 9.32 373	62	0.67 689	9.99 059 9.99 056	7 6	.3 0.9 0.6				
55 56	9.31 490	60	9.32 436	63	0.67 564	9.99 054	5	.4 1.2 0.8				
56	9.31 549	59 <b>6</b> 9	9.32 498	62	0.67 502	9.99 051	4	.5 I.5 I.0 .6 I.8 I.2				
57 58	9.31.609 9.31.669	60	9.32 561 9.32 623	62	0.67 439	9.99 048 9.99 046	3 2	.7 2.1 I.4				
H 59 I	9.31 728	59 60	9.32 685	62	0.67 315	9.99 043	1	.8 2.4 1.6 .9 2.7 1.8				
60	9 31 788		9.32 747	62	0.67 253	9.99 040	0	12/ 21/1 210				
	L. Cos.	d.	L. Cotg.	c. d.	L. Tang.	L. Sin.	•	Prop. Pts.				
					78°							
J												

	12°											
1	L. Sin.	d.	L. Tang.	c. d.	L. Cotg.	L. Cos.		Prep. Pts.				
0	9.31 788 9.31 847	59	9.32 747 9.32 810	63	0.67 253	9.99 040	60					
2	9.31 907	60	9.32 872	62 61	0.67 190	9.99 038 9.99 035	59 58	.1 6.3 6.2				
3	9.31 966	59 59	9.32 933	62	0.67 067	9.99 032	57	.2 12.6 12 4				
4	9.32 025	59	9.32 995 9.33 057	62	0.66 943	9.99 030	56	.3 18.9 18.6 .4 25.2 24.8				
5	9.32 143	59 59	9.33 119	62	0.66 881	9.99 024	55 54	.5 31.5 31.0 .6 37.8 37.2				
8	9.32 202 9.32 261	59	9.33 180 9.33 242	62	0.66 820	9.99 022	53	.6 37.8 37.2 .7 44.1 43.4				
9	9.32 319	58	9.33 303	62	0.66 697	9.99 016	52 51	.8 50.4 49.6				
10	9.32 378	59 59	9.33 365	61	0.66 635	9.99 013	50	.9  56.7  55.8				
11 12	9.32 437 9.32 495	58	9.33 426 9.33 487	6z	0.66 574	9.99 008	49 48	.1 6.1 6.0				
13	9.32 553	58 59	9.33 548	62	0.66 452	9.99 005	47	.2 12.2 12.0				
14	9.32 612	58	9.33 609	62	0.66 391	9.99 002	46	.3 18.3 18.0				
15 16	9.32 670 9.32 728	58	9.33 670 9.33 731	6x	0.66 330	9.99 000	45 44	.4 24.4 24.0 .5 30.5 30.0 .6 36.6 36.0				
17	9.32 786	58 58	9.33 792	62 61	0.66 208	9.98 994	43					
18	9.32 844 9.32 902	58	9.33 853 9.33 913	60	0.66 147	9.98 991 9.98 989	42 41	.7 42.7 42.0 .8 48.8 48.0				
20	9.32 960	5 <b>8</b>	9.33 974	61	0.66 026	9.98 986	40	.9 54.9 54.0				
2I 22	9.33 018	58 57	9.34 034	60 61	0.65 966	9.68 983	39 38	59				
23	9.33.075	58	9.34 095	60	0.65 905	9.98 980	38 37	.1 5.9 .2 11.8				
24	9.33 190	57 58	9.34 215	60 63	0.65 783	9.98 975	36	.3 17.7				
25 26	9.33.248 9.33.305	57	9.34 276	60	0.65 724	9.98 972 9.98 969	35	r .441 23.0				
27 28	9.33 362	57	9 34 336 9 34 396	60	0.65 604	9.98 967	34 33	.6 35.4				
	9.33 420	58 57	9.34 456	60 60	0.65 544	9.98 964	32	.7 41.3 .8 47.2				
29 80	9 33 477	57	9.34 516	60-	0.65 484	9.98.961	31	.9 53.1				
31	9 33 591	57	9.34.635	59	0.65.365	9.98 955	29	52 57				
32	9.33 647 9.33 704	56 57	9.34 695	60 60	0.65 305 0.65 245	9.98.953	28	.3 5.8 5.7 .2 11.6 11.4				
33 34	9.33 761	57	9·34·755 9·34·814	59	0.65 186	9.989 <del>3</del> 0 9.98947	27 26	.3 17.4 17.1				
35 36	9.33818	57 56	9.34.874	<b>6</b> 0-	0.65 126	9.98 944	25	.at 23.21 22.8				
36	9.33 874 9.33 931	57	9·34·933 9·34·992	59	0.65 067	9.98941 9.98938	24	.6 34.8 34.2				
37 38	9.33 987	56	9.35 051	59 60	0.64,949	9.98 936	23 22	7 40.6 39.9				
39	9.34 043	56 57	9.35 111	572	0.64 889	9.98 933	21	.8 46.4 45.6				
40 41	9.34 100 9.34 156	56	9.35 170 9.35 229	59	0.64 830	9.98930	20 19	56 55				
42	9.34 212	5 <b>6</b> 56	9.35 288	59 59	0.64 712	9 98 924	18	.1 5.6 5.5 .2 11.2 11.0				
43 44	9.34 268 9.34 324	56	9.35 347 9.35 405	58	0.64 653 0.64 595	9.98 921 9.98 919	17	.2 11.2 11.0 .3 16.8 16.5				
45	9.34 380	56	9.35 464	59	0.64 536	9.98 916	15	.4 22.4 22.0				
46	9 34 436	56 55	9.35 523	59 58	0.64 477	9.98 913	14	.5 28.0 27.5 .6 33.6 33.0				
47 48	9.34 491 9.34 547	56	9.35 581 9.35 640	59	0.64 419	9.98 910 9.98 907	. 13 12	.7 39.2 38.5				
49	9.34 602	55 56	9.35 698	58 59	0.64 302	9.98 904	ш	.8 44.8 44.0 .9 50.4 49.5				
50 51	9.34 658	55	9.35 757	58	0.64 243 0.64 185	9.98 901	10	3 2				
52	9.34 713 9.34 769	56	9.35 873	58	0.64 127	9.98 898 9.98 896	8	.1 0.3 0.2				
53	9.34 824	55 55	9.35 931	58 58	0.64 069	9.98 893	7 6	.2 0.6 0.4 .3 0.9 0.6				
<u>54</u>	9.34 879 9.34 934	55	9.35 989	58	0.64 011	9.98 890	5	1.4 1.2 0.0				
55 56	9.34 989	55	9.36 105	58	0.63 895	9.98 884	4 3	.5 1.5 1.0 .6 1.8 1.2				
57 58	9.35 044 9.35 099	55 <sub>.</sub>	9.36 153 9.36 221	58 58	0.63 837 0.63 779	9.98 881 9.98 878	3	.7 2.1 1.4				
59	9.35 154	55	9.36 279	58	0.63 721	9.98 875	1	.8 2.4 1.6 .9 2.7 1.8				
60	9.35 209	55	9.36 336	57	0.63 664	9.98 872	0	-781				
	L. Cos.	d.	L. Cotg.	c. d.		L. Sin.	,	Prop. Pts.				
					77°							

					13°			
,	L. Sin.	d.	L. Tang.	c. d.	L. Cotg.	L. Cos.		Prop. Pts.
0	9.35 209	54	9.36 336	58	0.63 664	9.98 872	60	
1 2	9.35 263 9.35 318	55	9.36 394 9.36 452	58	o 63 606 o 63 548	9.98 869 9.98 867	59 58	. I 5.8 5.7
3	9.35 373	55 54	9.36 509	57 57	0.63 491	9.98 864	57	.2 11.6 11.4
4	9.35 427	54	9.36 566	58	0.63 434	9.98 861	56	·3 17.4 17.1
5	9.35 481 9.35 536	55	9.36 624 9.36 681	57	0.63 376 0.63 319	9.98 858 9.98 85 <b>5</b>	55 54	.4 23.2 22.8 .5 29.0 28.5
7	9.35 590	54 54	9.36 738	57 57	0.63 262	9.98 852	-53	6 34.8 34.2
8 9	9.35 644 9.35 698	54	9.36 795 9.36 852	57	0.63 205	9.98 849 9.98 846	52 51	. 7 40.6 39.9 .8 46.4 45.6
10	9.35 752	54	9.36 909	57	0.63 091	9.98 843	50	.9 52.2 51.3
11	9.35 752 9.35 806	54 54	9.36 966	57 57	0.63 034	9.98 840	49 48	55 55
12 13	9.35 860 9.35 914	54	9.37 023 9.37 080	57.	0.62 977	9.98 837 9.98 834		.1 5.6 5.5 .2 11.2 11.0
14	9.35 968	54	9.37 137	57	0.62 863	9.98 831	47 46	.3 16.8 16.5
15	9.36 022	54	9.37 193	56	0.62 807	9.98 828	45	.4 22.4 22.0
16 17	9.36 075 9.36 129	53 54	9.37 250	57 56	0.62 750	9.98 825 9.98 822	44	.5 28.0 27.5 .6 33.6 33.0
18	9.36 182	53	9.37 306 9.37 363	57	0.02 637	9.98 819	43 42	.7 39.2 38.5
19	9.36 236	54 53	9.37 419	56 57	0.62 581	9.98 816	41	.8 44.8 44.0
20 21	9.36 289	53	9.37 476	56	0.62 524	9.98 813 9.98 810	40	.9  50.4  49.5   54
22	9.36 342 9.36 395	53	9.37 532 9.37 588	56	0.62 412	9.98 807	39 38	
23	9.36 449	54 53	9.37644	56 56	0.62 356	9.98 804	37	.2 10.8
24	9.36 502	53	9.37 700	56	0.62 300	9.98 801 9.98 798	36	.3 16.2 .4 21.6
25 26	9.36 553 9.36 608	53	9.37 756 9.37 812	56	0.62 244 0.62 188	9.98 795	35 34	.5 27.0
27 28	9.36 660	52 53	9.37 808	56 56	0.62 132	9.98 792	33	.6 32.4 .7 37.8
28	9.36 713 9.36 766	53	9.37 924 9.37 980	56	0.62 076	9.98 789 9.98 786	32 31	.8 43.2
80	9.36 819	53	9.38 035	55	0.61 965	9.98 783	80	.9  48.6
31	9.36871	52 53	9.38 091	56 56	0.61 909	9.58 780	29	53 52
32 33	9.36 924 9.36 976	52	9.38 147 9.38 202	55	0.61 853 0.61 798	9.98 777 9.98 774	28 27	.1 5.3 5.2 .2 10.6 10.4
34	9.37 028	52	9.38 257	55	0.61 743	9.98 771	26	.3 15.9 15.6
35 36	9.37 081	53 52	9.38 313	56 55	0.61 687	9.98 768	25	.4 21.2 20.8 .5 26.5 26.0
30	9.37 133 9.37 185	52	9.38 368 9.38 423	55	0.61 632 0.61 577	9.98 76 <del>3</del> 9.98 762	24 23	6 31 8 31.2
37 38	9.37 237	52	9.38 479	36	0.61 521	9.98 759	22	.7 37.1 36.4 .8 42.4 41.6
39	9.37 289	52 52	9.38 534	55 55	0.61.466	9.98 756	21	.8 42.4 41.6 .9 47.7 46.8
40 41	9.37 341 9.37 393	52	9.38 589 9.38 644	55	0.61 411	9.98 753 9.98 750	20	51 4
42	9.37 445	52	9.38 699	55	0.61 301	9.98 746	18	.1 5.1 0.4
43	9 37 497	52 52	9.38 754 9.38 808	55 54	0.61 246 0.61 192	9.98 743	17 16	.2 IO.2 O.8 .3 I5.3 I.2
44	9.37 549	51 °	9.38 863	55	0.01 137	9.98 740	15	.4 20.4 1.6
45 46	9.37 652	52	9.38 918	55	0.61 082	9.98 734	14	.5 25.5 2.0 .6 30.6 2.4
47 48	9.37 703	51 52	9.38 972	54 55	0.61 028	9.98 731 9.98 728	13	.7 35.7 2.8
49	9·37 755 9·37 806	5x	9.39 027 9.39 082	55	0.60 9/3	9.98 725	12 11	.8 40.8 3.2
50	9.37 858	52	9.39 136	54	0.60 864	9.98 722	10	.9 45.9 3.6
51	9.37 909	51 51	9.39 190	54 55	0.60810	9.98 719	9	.1 0.3 0.2
52 53 54	9.37 960 9.38 OII	5 <b>x</b>	9.39 245 9.39 299	54	0.60 755	9.98 715	7	.2 0.6 0.4
54	9.38 062	51 51	9.39 353	54 54	0.60 647	9.98 709	7 6	.3 0.9 0.6 .4 1.2 0.8
55 56 57 58 59	9.38 113 9.38 164	51 51	9.39 407	54 54	0.60 593 0.60 539	9.98 706	. 5	.5 1.5 1.0
57	9.38 215	5 <b>1</b>	9.39 461 9.39 515	54	0.60 485	9.98 703 9.98 700	4	.6 I.8 I.2 .7 2.1 I.4
58	9.38 266	51 51	9.39 569	54	0.60 431	9.98697	3 2	8 2.4 1.6
59 <b>60</b>	9.38 317	51	9.39 623	54 54	0.60 377	9.98 694	-1	.9 2.7 1.8
							_	Dron Di-
H	L. Cos.	d.	L. Cotg.	c. a.		L. Sin.	,	Prop. Pts.
					76°			

44	14°										
,	L. Sin.	d.	L. Tang.	c. d.	L. Cotg.	L. Cos.	d.		Prop. Pts.		
0	9.38 368	50	9.39 677	54	0.60 323	9.98 690		60			
I 2	9.38 418 9.38 469	51	9.39 731 9.39 785	54	0.60 269	9.98 687 9.98 684	3	59 58			
3	9.38 519	50	9.39 838	53	0.60 162	9.98 681	3	50 57	54 53		
4_	9.38 570	51 50	9.39 892	54 53	0.60 108	9.98 678	3	56	.1 5.4 5.3 .2 10.8 10.6		
5	9.38 620 9.38 670	50	9.39 945	54	0.60 053	9.98 673 9.98 671	4	55	.3 16.2 15.9		
	9.38 721	51	9.39 999 9.40 052	53	0.59 948	9.98 668	3	54 53	.4 21.6 21.2		
8	0.38 771	50 50	9.40 106	54 53	0.59 894	9.98 665	3	52	.5 27.0 26.5 .6 32.4 31.8		
9 10	9.38 821	50	9.40 159	53	0.59 841	9.98 662	3	51	.7 37.8 37.1		
11	9.38 921	50	9.40 212 9.40 266	54	0.59 788 0.59 734	9.98 659 9.98 656	3	50	.8 43.2 42.4 .9 48.6 47.7		
12	9.38 971	50 50	9.40 319	53 53	0.59 681	9.98 652	4	49 48	.9140.0147.7		
13	9.39 021	50	9.40 372	53	0.59 628	9.98 649	3	47	1 1		
14	9.39 071	50	9.40 425	53	0.59 575	9.98 646	3	46	.1 5.2 5.1		
15 16	9.39 170	49	9.40 531	53	0.59 469	9.98 640	3	45 44	.2 10.4 10.2		
17 18	9.39 220	50 50	9.40 584	53 52	0.59 416	9.98 636	4	43	.3 15.6 15.3 .4 20.8 20.4		
19	9.39 270 9.39 319	49	9.40 636 9.40 689	53	0.59 364	9.98 633 9.98 630	3	42 41			
20	9.39 369	50	9.40 742	53	0.59 258	9.98 627	3	40	6 31.2 30.6		
21	9.39 418	49 49	9 40 793	53 52	0.59 205	9.98 623	4	39 38	.7 36.4 35.7 .8 41.6 40.8		
22 23	9 39 467 9 39 517	50	9.40 847	53	0.59 153	9.98620 9.98617	3	38 37	.9 46.8 45.9		
24	9.39 566	49	9.40 952	52	0.59 048	9.98 614	3	36			
25	9.39 613	49	9.41 ∞5	53 52	0.58 995	9.98 610	4	35	50   49		
26 27	9.39 664	49	9.41 057 9.41 109	52	0.58 943 0.58 891	9.98 607 9.98 604	3	34	1.1 5.0 4.0		
28	9.39 762	49	9.41 161	52	0.58 839	9.98 601	3	33 32	.2 10.0 9.8		
29	9.39 811	49 49	9.41 214	53 52	0.58 786	9.93 597	4	31	.3 15.0 14.7 .4 20.0 19.6		
80	9.39 860	49	9.41 266	52	0.58 734 0.58 682	9.93 594	3	80	.4 20.0 19.0 .5 25.0 24.5 .6 30.0 29.4		
31 32	9.39 909 9.39 958	49	9.41 318 9.41 370	52	0.58 630	9.98 591 9.98 588	3	29 28			
33	9.40 006	48 49	9.41 422	52 52	0.58 578	9.98 584	4	27	.7 35.0 34.3 .8 40.0 39.2		
34	9.40 055	48	9.41 474	52	0.58 526	9.98 581	3	26	.9 45.0 44.1		
35 36	9.40 I03 9.40 I52	49	9.41 526 9.41 578	52	0.58 474 0.58 422	9 98 578 9 98 574	4	25 24			
37 38	9:40 200	48 49	9.41 629	51 52	0.58 371	9.98 571	3	23	1 48 1 47		
38	9.40 249 9.40 297	48	9.41 681	52	0.58 319 0.58 267	9 98 568	3	22	.1 4.8 4.7		
40	9.40 346	49	9.41 733	51	0.58 207	9.98 563	4	21 20	.2 9.6 9.4		
41	9.40 394	48 48	9.41 836	52	0.58 164	9.98 558	3	19	.3 14.4 14.1 .4 19.2 18.8		
42	9.40 442	48	9.41 887	51 52	0.58 113	9.98 555	3	18	.5 24.0 23.5		
43 44	9.40 490 9.40 538	#8	9.41 939 9.41 990	5 I	0.58 o61 0.58 o10	9.98 551 9.98 548	3	17 16	.6 28.8 28.2		
45 46	9.40 586	48 48	9.42 041	51	0.57 959	9.98 545	3	15	.7 33.6 32.9 .8 38.4 37.6		
46	9.40 634	48 48	9.42 093	52 51	0.57 907	9.98 541	4	14	.9 43 2 42 3		
47 48	9.40 682 9.40 730	48	9.42 I44 9.42 I95	51	0.57 856 0.57 803	9.98 538 9.98 535	3	13			
49	9.40 778	48 47	9.42 246	51 51	0.57 754	9.98 531	4	11	1413		
50	9.40 825	48	9.42 297	51	0.57 703	9.98 528	3	10	.1 0.4 0.3		
51 52	9.40 873	48	9.42 348 9.42 399	51	0.57 652 0.57 601	9.98 52 <del>5</del> 9.98 521	4	98 76	.2 0.8 0.6 .3 1.2 0.9		
53	9 4c 968	47 48	9.42 450	51 51	0.57 550	9.98 518	3	7	.4 1.6 1.2		
54	9.41 016	47	9.42 501	51 51	0.57 499	9.98 513	3 4		.4 1.6 1.2 .5 2.0 1.5 .6 2.4 1.8 .7 2.8 2.1 .8 3.2 2.4 .9 3.6 2.7		
55 56	9.41 063 9.41 111	48	9.42 552 9.42 603	51	0.57 448	9.98 511 9.98 508	3	5 4 3 2	.6 2.4 I.8 .7 2.8 2.1		
57 58	9.41 158	47	9.42 653	50	0.57 347	9.98 505	3	3	.8 3.2 2.4		
58 59	9.41 205 D.41 252	47	9.42 704	51 51	0.57 296	9.98 501	4 3	2 I	.9 3.6 2.7		
60	9.41 252	48	9.42 755	50	0.57 245	9.98 498	4	-			
	L. Cos.	d.	L. Cotg.	c. A		L. Sin.	d.	Ť	Dron Die		
	1 20 0000	, u.	n nong.	10. <b>u</b> .		II. DIN.	(le		Prop. Pts.		
<b>!</b>					75°						

	15°										
,	L. Sin.	d.	L. Tang.	c. d.	L. Cotg.	L. Cos.	d.		Prop. Pts.		
0	9.41 300	47	9.42 805	51	0.57 195	9.98 494	3	60			
I 2	9.41 347 9.41 394	47	9.42 856 9.42 906	50	0.57 144	9.98 491 9.98 488	3	59 58	l/		
3	9.41 441	47 47	9 42 957	51 50	0.57 043	9.98 484	4	57	51 50 V		
4	9.41 488	47	9.43 ∞7	50	0.56 993	9.98 481	3	56	.2 10.2 10.0		
5	9.41 53 <del>5</del> 9.41 582	47	9.43 057 9.43 108	51	0.56 943	9.98 477 9.98 474	3	55 54	.3 15.3 15.0		
7 8	9.41 628	46 47	9.43 158	50 50	0.56 842	9.98 471	3 4	53	.4 20.4 20.0 .5 25.5 25.0		
9	9.41 675 9.41 722 .	47	9.43 208 9.43 258	50	0.56 792	9.98 467 9.98 464	3	52	.6 30.6 30.0		
10	9.41 768	46	9.43 308	50	0.56 692	9.98 460	4	51 50	.7 35.7 35.0 8 40.8 40.0		
11	9.41 813	47	9.43 358	50 50	0.56 642	9.98 457	3	49 48	.9 45.9 45.0		
12	9.41 861 9.41 908	47	9.43 408 9.43 458	50	0.56 592	9.98 453	3	48 47	l		
14	9.41 954	46 47	9.43 508	50 50	0.56 492	9.98 447	3	46	49   48		
15	9.42 001	46	9.43 558	49	0.56 442	9.98 443	4	45	.1 4.9 4.8 .2 9.8 9.6		
16 17	9.42 047 9.42 093	46	9.43 607	50	0.56 393 0.56 343	9.98 440 9.98 436	4	44 43	.2 9.8 9.6 .3 14.7 14.4		
17 18	9.42 140	47 46	9 43 707	50 49	0.56 293	9.98 433	3	42	.4 19.6 19.2		
19 <b>20</b>	9.42 186	46	9.43 756	50	0.56 244	9.98 429	4	41	.5 24.5 24.0 .6 29.4 28.8		
2U 2I	9.42 232 9.42 278	46	9.43 806 9.43 855	49	0.56 194	9.98 426 9.98 422	4	40	7 34.3 33.6		
22	9.42 324	46 46	9.43 903	50 49	0.56 095	9.98419	3	39 38	.8 39.2 38.4 .9 44.1 43.2		
23 24	9.42 370 9.42 416	46	9 · 43 954 9 · 44 004	50	0.56 046	9.98 415 9.98 412	4	37	.91 44.11 43.2		
	9.42 461	45	9.44 053	49	0.55 947	9.98 409	3	36 35			
25 26	9.42 507	46 46	9.44 102	49 49	0.55 898	9.98 405	4	34	.I 4.7 4.6		
27 28	9.42 553 9.42 599	46	9.44 151 9.44 201	50	0.55 849	9.98 402 9.98 398	3	33	.2 9.4 9.2		
29	9.42 644	45 46	9.44 250	49	0.55 750	9.98 395	.3	32 31	.3 14.1 13.8		
80	9.42 690	45	9.44 299	49 49	0.55 701	9.98 391	4	30			
31 32	9.42 735 9.42 781	46	9.44 348 9.44 397	49	0.55 652	9.98 388 9.98 384	3	29 28	.6 28.2 27.6		
33	9.42 826	45 46	9.44 446	49	0.55 554	9.98 381	3	27	.7 32.9 32.2 .8 37.6 36.8		
34	9.42 872	45	9.44 493	49 49	0.55 505	9.98 377	4	26	.9 42.3 41.4		
35 36	9.42 917 9.42 962	45	9 · 44 · 544 9 · 44 · 592	48	0.55 456 0.55 408	9.98 373 9.98 370	3	25 24	1		
37 38	9.43 008	46 45	9.44 641	49	0.55 359	9.98 366	4	23	45   44		
38 39	9.43 053 9.43 098	45	9.44.690	49 48	0.55 310	9.98 363 9.98 359	3	22			
40	9.43 143	45	9.44 738 9.44 787	49	0.55 262	9.98 356	3	21	. <b>2</b>   9.0  8.8		
41	9.43 188	45	9.44 836	49 48	0.55 164	9.98 352	4	19	.3 13.5 13.2 .4 18.0 17.6		
42. 43	9.43 233 9.43 278	45 45	9.44 884	49	0.55 116	9.98 349	3	18	.5 22.5 22.0		
44	9.43 278	45	9.44 933 9.44 981	48	0.55 067	9.98 345 9.98 342	3	17 16			
45	9.43 367	44 45	9.45 029	48	0.54 971	9.98 338	4	15	.8 36.0 35.2		
46 47	9.43 412 9.43 457	45	9.45 078 9.45 126	49 48	0.54 922	9.98 334 9.98 331	4	14	.9 40.5 39.6		
47 48	9.43 502	45	9.45 174	48	0.54 826	9.98 327	4.	13 12			
49	9.43 546	44 45	9.45 222	48 49	0.54 778	9.98 324	3 4	11	4   3		
50 51	9.43 591 9.43 635	44	9.45 271 9.45 319	48	0.54 729	9.98 320	3	10	.I 0.4 0.3 .2 0.8 0.6		
52	9.43 680	45	9.45 367	48	0.54 633	9.98 313	4	8			
53 54	9.43 724	44 45		48 48	0.54 585	9.98 309	4	7 6	.4 1.6 1.2		
	9.43 769	44	9.45 463	48	0.54 537	9.98 306	4	-	.3 1.2 0.9 .4 1.6 1.2 .5 2.0 1.5 .6 2.4 1.8		
56	9.43 857	44	0.45 550	48	0.54 441	9.98 299	3	5 4 3 2	7 2.8 2.1		
57	9.43 901 9.43 946	44 45	9.45 666 9.45 654	47 48	0.54 394	9.98 295	4	3	.8 3.2 2.4 .9 3.6 2.7		
55 56 57 58 59	9.43 990	44	9.45 054	48	0.54 346 0.54 298	9.98 291 9.98 288	3	2 1			
60	9.44 034	44	9.45 750	48	0.54 250	9.98 284	4	0			
	L. Cos.	d.	L. Cotg.	c. d.	L. Tang.	L. Sin.	d.	,	Prep. P'		
	74°										
<u> </u>	14										

					16°				
,	L. Sin.	d.	L. Tang.	c.d.	L. Cotg.	L. Cos.	d.		Prop. Pts.
0	9.44 034	44	9.45 750	47	0.54 250	9.98 284	3	60	
I 2	9.44 078 9.44 122	44	9.45 79 <u>7</u> 9.45 845	48	0.54 203 0.54 155	9.98 281 9.98 277	4	59 58	
3	9.44 166	44	9.45 892	47 48	0.54 108	9.98 273	4	57	.1 4.8 4.7
4	9.44 210	43	9.45 940	47	0.54 060	9.98 270	4	56	2 9.6 9.4
5 6	9.44 253 9.44 297	44	9.45 987 9.46 035	48	0.54 013	9.98 262	4	55 54	.3 14.4 14.1
7 8	9.44 341	44	9:46 082	47 48	0.53 918	9.98 259	3 4	53	.4 19.2 18.8 .5 24.0 23.5
8	9.44 38 <del>3</del> 9.44 428	43	9.46 130 9.46 177	47	0.53 870	9.98 255 9.98 251	4	52	.6 28.8 28.2
10	9.44 472	44	9.46 224	47	0.53 776	9.98 248	3	50	.7 33.6 32.9 .8 38.4 37.6
II	9.44 516	44 43	9.46 271	47 48	0.53 729	9.98 244	4	49 48	9 43 2 42.3
12	9.44 559 9.44 602	43	9.46 319 9.46 366	47	0.53 681	9.98 240 9.98 237	3	48 47	
14	9.44 646	44 43	9.46 413	47	0.53 587	9.98 233	4	46	46   45
15	9.44 689	44	9.46 460	47	0.53 540	9.98 229	4	45	.1 4.6 4.5 .2 9.2 9.0
16 17	9·44 733 9·44 776	43	9.46 507 9.46 554	47	0.53 493	9.98 226 9.98 222	4	44 43	.3 13.8 13.5
18	0.44 810	43 43	9.46 601	47	0.53 399	9.98 218	4	42	.4 18.4 18.0
19 <b>20</b>	9.44 862	43	9.46 648	46	0.53 352	9.98 213	3	41	.5 23.0 22.5 .6 27.6 27.0
2U 2I	9.44 905 9.44 948	43	9.46 741	47	0.53 306	9.98 211	4	40	.7 32.2 31.5
22	9.44 992	44 43	9.46 788	47	0.53 212	9.98 204	3	39 38	.8 36.8 36.0 .9 41.4 40.5
23 24	9.45 035 9.45 077	42	9.46 83 <del>5</del> 9.46 881	46	0.53 165	9.98 200 9.98 196	.4	37 36	.9145.4440.5
25	9.45 120	43	9.46 928	47	0.53 072	9.98 192	4	35	
26	9.45 163	43 43	9.46 975	47 46	0.53 025	9.98 189	3	34	.1 4.4 4.3
27 28	9.45 206 9.45 249	43	9.47 021 9.47 068	47	0.52 979 0.52 932	9.98 18 <del>3</del> 9.98 181	4	33 32	.1 4.4 4.3 .2 8.8 8.6
29	9.45 292	43 42	9.47 114	46 46	0.52 886	9.98 177	4	31	.3 13.2 12.9
80	9.45 334	43	9.47 160	47	0.52 840	9.98 174	3 4	80	.4 17.6 17.2 .5 22.0 21.5
31 32	9.45 377 9.45 419	42	9.47 207 9.47 253	46	0.52 793 0.52 747	9.98 170 9.98 166	4	29 28	.6 26.4 25.8
33	9.45 462	43 42	9.47 299	46 47	0.52 701	9.98 162	4	27	.7 30.8 30.1 .8 35.2 34.4
34	9.45 504	43	9.47 346	46	0.52 654	9.98 159	3 4	26	.8 35.2 34.4 .9 39.6 38.7
35 36	9.45 547 9.45 589	42	9.47 392 9.47 438	46	0.52 608 0.52 562	9.98 153	4	25 24	
37 38	9.45 632	43 42	9.47 484	46 46	0.52 516	9.98 147	4	23	1 42 1 41
38 39	9.45 674 9.45 716	42	9.47 530 9.47 576	46	0.52 470	9.98 144 9.98 140	3	22 21	.1 4.2 4.1
40	9.45 758	42	9.47 622	46	0.52 378	9.98 136	4	20	.2 8.4 8.2
41	9.45 801	43 42	9.47 668	46 46	0.52 332	9.98 132	4	19	.3 12.6 12.3 .4 16.8 16.4
42 43	9.45 843 9.45 885	42	9.47 714 9.47 760	46	0.52 286	9.98 129 9.98 125	3	18 17	.5 21.0 20.5
44	9.45 927	42 42	9.47 806	46 46	0.52 194	9.98 121	4	16	.7 20.4 28.7
45	9.45 969	42	9.47 852	45	0.52 148	9.98 117	4	15	.8  33.6  32.8
46 47	9.46 of 1 9.46 of 3	42	9.47 897 9.47 943	46	0.52 103	9.98 113	4	14 13	.9 37.8 36.9
47 48	9.46 095	42 41	9.47 989	46 46	0.52 011	9.98 106	4	12	
49 <b>50</b>	9.46 136	42	9.48 035	45	0.51 965	9.98 102	4	11	4   3
51	9.46 178	42	9.48 080 9.48 126	46	0.51 920 0.51 874	9.98 o98 9.98 o94	4	10	.1 0.4 0.3
52	9.46 262	42 41	9.48 171	45 46	0.51 829	9.98 090	4		.3 1.2 0.9
53 54	9.46 30 <u>3</u> 9.46 34 <del>5</del>	42	9.48 217 9.48 262	45	0.51 783	9.98 087 9.98 083	3	8 7 6	4 1.6 1.2
	9.46 386	4I	9.48 307	45	0.51 738	9.98 079	4		.4 I.6 I.2 .5 2.0 I.5 .6 2.4 I.8
55 56	9.46 428	42 41	9.48 353	46	0.51 647	9.98 075	4	5 4 3 2	.7  2.8  2.I
57 58 59	9.46 469 9.46 511	42	9.48 398 9.48 443	45 45	0.51 602	9.98 071 9.98 067	4	3	.8 3.2 2.4 .9 3.6 2.7
59	9.46 552	41 42	9.48 489	46	0.51 511	9.98 063	4	ī	1 101 0101 -17
60	9.46 594	<u> </u>	9.48 534	45	0.51 466	9.98 060	3	0	
	L. Cos.	d.	L. Cotg.	c. d.	L. Tang.	L. Sin.	d.	,	Prop. Pts.
					73°				
<u> </u>									

	17°											
,	L. Sin.	·d.	L. Tang.	c. d.	L. Cotg.	L. Cos.	d.		Prop. Pts.			
0	9.46 594	41	9.48 534	45	0.51.466	9.98 060	4	60				
1 2	9.46 63 <del>\$</del> 9.46 676	41	9.48 579 9.48 624	45	0.51 421	9.98 056 9.98 052	4	59 58				
3	9 46 717	41	9.48 669	45 45	0.51 331	9.98 048	4	57	·E 4.5 4.4			
4	9.46 758	42	9.48 714 9.48 759	45	0.51 286	9.98 044	4	56	.2 9.č 8.8			
5	9.40 841	41	9.48 804	45	0.51 241	9.98 040 9.98 036	4	55 54	.3 13.5 13.2 .4 18.0 17.6			
7 8	9.46 882	4E	9.48 849	45 45	0.51 151	9.98 032	4	53	.5 22.5 22.0 .6 27.0 26.4			
9	9.46 923 9.46 964	41	9.48 894 9.48 939	45	0.51 106	9.98 029 9.98 025	4	52 51	.6 27.0 26.4			
10	9.47 005	48	9.48 984	45	0.51 016	9.98 021	4	50	.7 31.5 30.8 .8 36.0 35.2			
11	9.47 045	40 41	9.49 029	45 44	0.50 971	9.98017	4	49	.9 40.5 39.6			
12 13	9.47 086 9.47 127	41	9.49.073 9.49.118	45	0.50 927 0.50 882	9.98 org 9.98 oog	4	48	į			
14	9.47 168	4% 4%	9.49 163	45	0.50 837	9.98 005	4	47 46	43   48			
15	9.47 209	49	9.49 207	44 45	0.50 793	9.98 001	4	45	.I 4.3 4.2 .2 8.6 8.4			
16 17	9.47 249 9.47 290	41	9.49 252 9.49 296	44	0.50 748	9 97 997 9 97 993	4	44	.2 8.6 8.4 .3 12.9 12.6			
18	9.47 330	40 41	9.49 341	45	0.50 659	9.97 989	4	43 42	.4 17.2 16.8			
19	9 47 371	40	9.49 385	44 45	0.50 615	9.97 986	3	41	.5 21 .5 21 .0 .6 25 8 25 .2			
20 21	9.47 411 9.47 452	4E	9.49 430 9.49 474	44	0.50 570 0.50 526	9.97.982 9.97.978	4	4()	.7 30 I 29 4 .8 34 4 33 6			
22	9.47 492	40 41	9.49 474	45	0.50 481	9.97 974	4	39 38	.8 34.4 33.6 .9 38.7 37.8			
23 24	9 - 47 533	40	9.49 563	44	0.50 437	9.97.970	4	37	.91 30.71 37.0			
	9.47 573	40	9.49 652	45	0.50 393	9.97.966	4	35				
25 26	9.47 654	4 <sup>I</sup>	9.49 696	44	0.50 304	9.97.958	4	34	41 40			
27 28	9.47 694	40	9.49 740	44	0.50 200	9 97 954	4	33	.I 4.I 4.0 .2 8.2 8.0			
29	9·47 734 9·47 774	40	9.49 784 9.49 828	44	0.50 216	9.97 950 9 97 946	4	32 31	.3 12.3 12.0			
80	9.47 814	40 40	9.49 872	44	0.50 128	9.97 942	4	30	.4 16.4 16.0 .5 20.5 20.0			
31	9.47 854	40	9.49 916	44	0.50 084	9.97 938	4	29	6 24.6 24.0			
32 33	9.47 894 9.47 934	40	9.49 900	44	0.50 040	9.97 934 9.97 930	4	28 27	.7 28.7 28.0 .8 32.8 32.0			
34	9.47 974	40 40	9.50 048	44	C.49 952	9.97 926	4	26	.8 32.8 32.0 .9 36.9 36.0			
35 36	9.48 014	40	9.50 092	44	C.49 908	9.97 922	. 4	25				
37	9.48 054 9.48 094	40	9.50 136 9.50 180	44	0.49 804	9.97 918 9.97 914	4	24 23				
37 38	9.48 133	39 40	9.50 223	43 44	0.49 777	9.97910	4	22	39 5 .1 3.9 0.5			
39 40	9.48 173	40	9.50 207	44	0.49 733	9.97 906	4	21	.2 7.8 1.0			
41	9.48 252	39	9.50 311 9.50 355	44	0.49 689	9.97 902 9.97 898	4	20 19	.3 II.7 I.5 .4 I5.6 2.0			
42	9.48 292	49 40	9.50 398	43 44	0.49 602	9 97 894	4	18				
43 44	9.48 332 9.48 371	39	9.50 442 9.50 485	43	0.49 558	9.97 890 9.97 886	4	17 16	.6 23.4 3.0			
45	9.48 411	40	9.50 529	44	0.49 471	9.97 882	4	15	.7 27.3 3.5 .8 31.2 4.0			
46	9.48 450	39 40	9.50 572	43 44	0.49 428	9.97 878	4	14	.9 35.1 4.5			
47 48	9.48 490	39	9.50 616 9.50 659	43	0.49 384	9.97 874 9.97 870	4	13 12				
49	9.48 568	39 39	9.50 703	44	0.49 297	9.97866	4	ii	1413			
50	9.48 607	40	9.50 746	43 43	0.49 254	9.97 861	5 4	10	.1 0.4 0.3			
51 52	9 48 647 9 48 686	39	9.50 789 9.50 833	44	0.49 211	9.97 857 9.97 853	4	8				
53	9.48 725	39 30	9.50876	43	0.49 124	9.97 849	4.	7 6	.4 1.6 1.2			
54	9.48 704	39 39	9.50 919	43 43	0.49 081	9.97 845	4		.5 2.0 1.5			
55 56	9.48 803	39	9.50 962	43	0.49 038	9.97 841 9.97 837	4	5 4	.6 2.4 I.8			
57	9.48 881	39 39	9 51 048	43	0 48 952	9 97 833	4	3 2	.8 3.2 2.4 .9 3.6 2.7			
57 58 59	9.48 920 9.48 959	39	9.51.092	44 43	0.48 908	9.97 829 9.97 825	4	2 I	.9  3.6  2.7			
60	9.48 998	39	9.51 178	43	0.48 822	9.97 821	4	-	į			
	L. Cos.	d.	L. Cotg.	c. d.		L. Sin.	d.	Ť	Prop. Pts.			
i			· · · · · · · · · · · · · · · · · · ·		<b>72°</b>		-					
<u>'</u>					. 4							

	18°										
,	L. Sin.	đ.		c. d.	L. Cotg.	L. Cos.	đ.		Prop. Pts.		
0	9.48 998	39	9.51 178	43	0.48 822	9.97 821	4	60			
I 2	9.49 <b>0</b> 37 9.49 076	39	9.51 221 9.51 264	43	0.48 779	9.97.817 9.97.812	5	59 58			
3	9.49 113	39 38	9.51 306	42	0.48 694	9.97 808	4	57	43   42		
4	9.49 153	39	9.51 349	43° 43	0.48 651	9.97 804	4	56	.1 4.3 4.2 .2 8.6 8.4		
5	9.49 192	39	9.51 392	43	0.48 608	9.97 800	4	55	.3 12.9 12.6		
7	9.49 231 9.49 269	38	9.51 435 9.51 478	43	0.48 565	9.97 796 9.97 792	4	54	.4 17.2 16.8		
7 8	9.49 308	39 39	9.51 520	42 43	0.48 480	9.97 788	4	53 52	.5 21.5 21.0 .6 25.8 25.2		
9	9 49 347	38	9.51 563	43	0.48 437	9.97 784	4 5	51	.7 30.1 29.4		
10	9.49 385 9.49 424	39	9.51 606 9.51 648	42	0.48 394 0.48 352	9 97 779 9 97 775	4	50	.8 34.4 33.6 .9 38.7 37.8		
12	9.49 462	38 38	9.51 691	43	0.48 309	9.97.771	4	49 48	.91 30.71 37.0		
13	9.49 500	39	9.51 734	43 42	0.48 266	9.97 767	4	47			
14	9·49 539 9·49 577	38	9.51 776	43	0.48 224	9.97 763	4	46	.1 4.1		
15 16	9.49 577	38	9.51 861	42	0.48 139	9 97 759 9 97 754	5	45 44	.2 8.2		
17 18	9.49 654	39 3 <b>8</b>	9.51 903	42 43	0.48097	9.97 750	4	43	.3 12.3		
	9.49 692	38	9.51 946	42	0.48 054 0.48 012	9.97 746	4	42	.4 16.4 .5 20.5		
19 20	9.49 730	38	9.52 031	43	0.48 012	9.97 742	4	41 40	.6 24.6		
21	9.49 806	38 38	9.52 673	42	0.47 927	9.97 734	4.		.7   28.7		
22	9.49 844	38	9.52 115	42 42	0.47 885	9.97 729	5 4	39 38	.8 32.8 .9 36.9		
23 24	9.49 882	38	9.52 157 9.52 200	43	0.47 843 0.47 800	9.97 725 9.97 721	4	37 36			
	9.49 958	38	9.52 242	42	0.47 758	9.97 717	4	35			
25 26	9.49 996	38 38	9.52 284	42 42	0.47 716	9.97 713	4	34	.1 3.9 3.8		
27 28	9.50 034	-38	9.52 326 9.52 368	42	0.47 674 0.47 632	9.97 708 9.97 704	5 4	33	.2 7 8 7.6		
29	9.50 110	38 38	9.52 410	42	0.47 590	9.97 700	4.	32 31	.3 11.7 11.4		
80	9.50 148	37	9.52 452	4º 42	0.47 548	9.97696	4	80	.4 15.6 15.2 .5 19.5 19.0		
31	9.50 185	3/ 38	9.52 494	42	0.47 506	9.97 691	5 4	20	.6 23.4 22.8		
32 33	9.50 223 9.50 261	38	9.52 536	42	0.47 464 0.47 422	9.97 687 9.97 683	4	28	7 27.3 26.6 .8 31.2 30.4		
34	9.50 298	37 38	9.52 620	42 41	0.47 380	9.97 679	4	26	.8 31.2 30.4 .9 35.1 34.2		
35 36	9.50 336	38	9.52 661	42	0.47 339	9.97 674	5 #	25	7,00		
30	9.50 374	37	9.52 703 9.52 745	42	0.47 29 <u>7</u> 0.47 25 <u>5</u>	9.97 670 9.97 666	4	24 23			
37 38	9.50 449	38	9.52 787	42 42	0.47 213	9.97 662	4	22	.1 3.7 3.6		
39	9.50 486	37 37	9.52 829	41	0.47 171	9.97657	5 4	21	2 7.4 7.2		
40 41	9.50 523 9.50 561	38	9.52 870 9.52 912	42	0.47 130	9.97 653 9.97 649	4	20	.3 11.1 10.8		
42	9.50 598	37	9.52 953	41	0.47 047	9.97 645	4	18	.4 14.8 14.4 .5 18.5 18.6		
43	9.50 635	37 38	9.52 995	42 42	0.47 005	9.97640	5	17	.6 22.2 21.6		
44	9.50 673	37	9.53 037	41	0.46 963	9.97 636	4	16	7 25.9 25.2		
45 46	9.50 710	37	9.53 078	42	0.46 880	9.97 632 9.97 628	4	15	.8 29.6 28.8 .9 33.3 32.4		
47 48	9.50 784	3 <b>7</b> 37	9.53 161	41 41	0.46 839	9.97 623	5	13	7. 55 5, 5		
48 49	9.50 821 9.50 858	37	9.53 202	42	0.46 798	9.97 619 9.97 615	4	12 11			
50	9.50 896	38	9 53 244 9 53 285	41	0.46 715	9.97 610	5	10	.I 0.5 0.4		
51	9.50 933	37	9.53 327	42	0.46 673	9.97606	4	0	1.0 0.8		
52	9.50'970	37 37	9.53 368	41 41	0.46 632	9.97 602	4 5	8	.3 I.5 I.2 .4 2.0 I.6		
53 54	9.51 ∞7 9.51 043	36	9.53 409 9.53 450	41	0.46 550	9 97 597 9 9 <b>7 593</b>	4	7 6			
55	9.51 080	37	9.53 492	42	0.46 508	9.97 589	4		.6 3.0 2.4		
55 56 57 58 59	9.51 117	37 37	9 53 533	41 41	0.46 467	9.97 584	5 4	5 4 3 2	.7 3.5 2.8 .8 4.0 3.2		
36 58	9.51 154 9.51 191	37	9.53 574 9.53 615	41	0.46 385	9 9 <b>7 580</b> 9 97 576	4	3	.9 4.5 3.6		
59	9.51 227	36 37	9.53 656	41 41	0.46 344	9.97 571	5	1	•		
60	9.51 264		9.53 697		0.46 303	9.97 567	+	0			
	L. Cos.	d.	L. Cotg.	c. d.	L. Tang.	L. Sin.	d.	,	Prop. Pts.		
1					71°						

					19°				
	L. Sin.	d.	L. Tang.	c.d.	L. Cotg.	L. Cos.	d.		Prop. Pts.
0	9.51 264 9.51 301	37	9.53 697	41	0.46 303 0.46 262	9.97 567	4	60	
2	9.51 338	37 36	9.53 738 9.53 779	4 <sup>I</sup>	0.46 221	9.97 563 9.97 558	. 5	59 58	
3	9.51 374	37	9.53 820	41 41	0.46 180	9 97 554	4	57	.I 4.I 4.0
4	9.51 411	36	9.53 861	41	0.46 139	9.97 550	5	56	.2 8.2 8.0
<b>5</b>	9.51 484	37 36	9.53 943	41 41	0.46 057	9 97 545 9 97 541	4	55 54	.3 12.3 12.0 .4 16.4 16.0
7 8	9.51 520 9.51 557	37	9.53 984	4I	0 46 016	9.97 536	5	53	.5 20.5 20.0
9	9.51 593	36 36	9.54 025 9.54 065	40	0.45 975 0.45 935	9 97 532 9 97 528	4	52 51	.6 24.6 24.0 .7 28.7 28.0
10	9.51 629	37	9.54 106	41 41	0.45 894	9.97 523	5	$\frac{50}{50}$	.8 32.8 32.0
11 12	9.51 666 9.51 702	36	9.54 147 9.54 187	40	0.45 853 0.45 813	9.97 519	4	49 48	.9 36.9 36.0
13	9.51 738	36 36	9.54 228	41 41	0.45 772	9.97 513 9.97 510	5	47	
14	9.51 774	37	9.54 269	40	0.45 731	9.97 506	4 5	46	39
15 16	9.51 811 9.51 847	36	9.54 309 9.54 350	41	0.45 691	9.97 501 9.97 497	4	45	.I 3.9 .2 7.8
17 18	9.51 883	36 36	9.54 390	40 41	0.45 610	9 97 492	5	44 43	.3 11.7
18	9.51 919 9.51 955	36	9 54 431	40	0.45 569	9.97 488	4	42	.4 15.6 .5 19.5
20	9.51 991	36	9.54 471	41 41	0.45 529	9.97 484	5	41	.6 23.4
21	9.52 027	36 36	9 54 552	40 41	0.45 448	9.97 475	4	39 38	.7 27.3 .8 31.2
22	9.52 003	36	9·54·593 9·54·633	40	0.45 407	9.97 470 9.97 466	5	38 37	.9 35.1
24	9.52 135	36 36	9.54 673	40 41	0.45 327	9.97 461	5	36	•
25	9.52 171	36	9.54 714	40	0.45 286	9.97 457	4	35	37   36
26 27	9.52 207 9.52 242	35	9·54 754 9·54 794	40	0.45 246 0.45 206	9.97 453 9.97 448	5	34 33	.1 3.7 3.6
27 28	9.52 278	36 36	9.54 835	41 40	0.45 165	9.97 444	4	32	.2 7.4 7.2 .3 II.I 10.8
<b>80</b>	9.52 314	36	9.54 873	40	0.45 125	9.97 439	5. 4	31	.4 14.8 14.4
31	9.52 350 9.52 385	35	9.54 913 9.54 955	40	0.45 085	9.97 435 9.9 <b>7 430</b>	5	80 29	.5 18.5 18.0
32	9.52 421	36 - 35	9.54 995	40 40	0.45 ∞5	9.97 426	4	28	.6 22.2 21.6 .7 25.9 25.2
33 34	9.52 456 9.52 492	36	9.55 035 9.55 075	40	0.44 965	9.97 <b>421</b> 9.97 417	5 4	27 26	.8 29.6 28.8
35	9.52 527	35	9.55 115	40	0.44 885	9.97 412	5	25	.9   33.3   32.4
36	9.52 563 9.52 598	36 35	9.55 155	40	0.44 845	9.97408	4 5	24	
37 38	9.52 634	36	9.55 195 9.55 235	40	0.44 803	9.97 403 9.97 399	4	23	35 34
39	9.52 669	35 36	9.55 275	40	0.44 725	9 97 394	5	21	.1 3.5 3.4 .2 7.0 6.8
40 41	9.52 705 9.52 740	35	9.55 315	40	0.44 685	9.97 390	5	20	.3 10.5 10.2
42	9.52 775	35 36	9·55 355 9·55 395	40	0.44 605	9 97 385 9 97 381	4	19 18	.4 14.0 13.6 .5 17.5 17.0
43 44	9.52 811 9.52 846	35	9.55 434	39 40	0.44 566	9.97 376	5 4	17 16	.6 21.0 20.4
	9.52 881	35	9.55 474 9.55 514	40	0.44 526	9.97 372 9.97 367	5	15	.7 24.5 23.8 .8 28.0 27.2
45 46	9.52 916	35 35	9.55 554	40 39	0.44 446	9.97 363	4	14	.9 31.5 30.6
47 48	9.52 951 9.52 986	35	9·55 593 9·55 633	40	0.44 407 0.44 367	9.97 358 9.97 353	5	13	
49	9.53 021	35 35	9.55 673	40 39	0.44 327	9.97 349	4	11	1514
50	9.53 056	36.	9.55 712	40	0.44 288	9 97 344	5	10	.1 0.5 0.4
51 52	9.53 092 9.53 126	34	9.55 752 9.55 791	39	0.44 248	9.97 340 9.97 335	5	8	.2 I.0 0.8 .3 I.5 I.2
53	9.53 161	35 35	9.55 791 9.55 831 9.55 870	40 39	0.44 169	9.97 331	4	7 6	1.4 2.0 1.6
54	9.53 196	35	9.55 870	40	0.44 130	9.97 326	5		.5 2.5 2.0
56	9.53 266	35	9.55 910 9.55 949	39	0.44 090 0.44 051	9.97 322 9.97 317	5	5 4	.6 3.6 2.4 .7 3.5 2.8 .8 4.0 3.2
57	9.53 301	35 35	9.55 989	40 39	0.44 011	9.97 312	5	3 2	1.0 4.0 3.2
55 56 57 58 59 <b>60</b>	9.53 336 9.53 370	34	9.56 028 9.56 067	39	0.43 972 0.43 933	9.97 308 9.97 303	5	2 I	.9 4.5 3.6
60	9.53 405	35	9.56 107	40	0.43 893	9.97 299	4	0	
	L. Cos.	d.	L. Cotg.	c. d.		L. Sin.	d.	,	Prop. Pts.
					70°				
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		•			20°				
,	L. Sin.	đ.	L. Tang.	c. d.	L. Cotg.	L. Cos.	d.		Prop. Pts.
0	9.53 405	35	9.56 107	39	0.43 893	9.97 299	5	60	
1 2	9·53 440 9·53 473	35	9.56 146 9.56 185	39	0.43 854	9.97 <b>294</b> 9.97 <b>28</b> 9	5	59 58	
3	9.53 509	34 35	9.56 224	39 40	0.43 776	9.97 283	4	57	.I 4.0 3.9
4	9.53 544	34	9.56 264	39	0.43 736	9.97 280	5	57 56	.I 4.0 3.9 .2 8.0 7.8
5	9.53 578 9.53 613	35	9.56 303 9.56 342	39	0.43 697 0.43 658	9.97 276 9.97 271	5	55 54	.3 12.0 11.7
7 8	9.53 647	34 35	9.56 381	39 39	0.43 619	9.97 266	5	53	.4 16.0 15.6 .5 20.0 19.5
8 9	9.53 682 9.53 716	34	9.56 <b>420</b> 9.56 459	39	0.43 580	9.97 262	5	52	.6 24.0 23.4
10	9.53 751	35	9.56 498	39	0.43 541	9.97 257 9.97 252	5	51 50	.7 28.0 27.3 .8 32.0 31.2
11	0.53 785	34 34	9 56 537	39 39	0.43 463	9.97 248	4	49 48	.9  36.0   35.1
12 13	9.53 819 9.53 854	35	9.56 576 9.56 615	39	0.43 424	9.97 243 9.97 238	5	48	
14	9.53 888	34	9.56 654	39	0.43 346	9.97 234	4	47 46	38 37
15 16	9.53 922	34 35	9.56 693	39 39	0.43 307	9.97 229	5	45	.I 3.8 3.7
	9·53 957 9·53 991	34	9.56 732	39	0.43 268	9.97 224	5 4	44	.2 7.6 7.4 .3 II.4 II.I
17 18	9.54 025	34	9.56 771 9.56 810	39	0.43 190	9.97 220 9.97 215	5	43 42	.4 15.2 14.8
19	9.54 059	34 34	9.56 849	39 38	0.43 151	9.97 210	5	41	.5 19.0 18.5 .6 22.8 22.2
20 21	9.54 093 9.54 127	34	9.56 887 9.56 926	39	0.43 113	9.97 206 9.97 201	5	40	.7   26.6   25.9
22	9.54 161	34	9.56 963	39	0.43 074	9.97 196	5	39 38	
23	9.54 195	34 34	9.57 004	39 38	0.42 996	9.97 192	<b>4</b> 5	37 36	.9   34.2   33.3
24	9.54 229 9.54 263	34	9.57.042	39	0.42 958	9.97 187 9.97 182	5		
25 26	9.54 297	34	9.57 120	39 38	0.42 880	9.97 178	4	35 34	35
27 28	9.54 331	34 34	9.57 158	39	0.42 842	9.97 173	5 5	33	.1 3.5 .2 7.0
20	9 · 54 365 9 · 54 399	34	9.57 197 9.57 235	38	0.42 765	9.97 168 9.97 163	5	32 31	.3 10.5
80	9.54 433	34	9.57 274	39 38	0.42 726	9.97 159	4	80	.4 14.0 .5 17.5
31	9.54.466	33 34	9.57 312	39	0.42 688	9.97 154	5	29 28	.6 21.0
32 33	9.54.500 9.54.534	34	9.57 351 9.57 389	38	0.42 649	9.97 14 <u>9</u> 9.97 143	4	20 27	.7 24.5 .8 28.0
34	9.54 567	33 34	9.57 428	39 38	0.42 572	9.97 140	5 5	26	.9 31.5
35 36	9.54 601 9.54 635	34	9.57 466	38	0.42 534	9 97 135	5	25	
37	9.54 668	33	9.57 504 9.57 543	39	0.42 457	9.97 130 9.97 126	4	24 23	34   33
37 38	9.54 702	34 33	9.57 581	38 38	0.42 419	9.97 121	5 5	22	
39 <b>40</b>	9·54 735 9·54 769	34	9.57 619	39	0.42 381	9.97 116	5	$\frac{21}{20}$	
41	9.54 802	33	9.57 696	38	0.42 342	9.97 III 9.97 IO7	4	19	.3 IO.2 9.9 .4 I3.6 I3.2
42 43	9.54 836 9.54 869	34 33	9 . 57 734	38 38	0.42 266	9.97 102	5 5	18	.5 17.0 16.5
44	9.54 903	34	9.57 772 9.57 810	38	0.42 228 0.42 190	9.97.097 9.97.092	5	17 16	
45	9.54 936	33 33	9.57 849	39 . 38	0.42 151	9.97 087	5	15	.8 27.2 26.4
46	9.54 969 9.55 ∞3	34	9.57.887. 9.57.925	38	0.42 113	9.97 083 9.97 078	4	14	.9 30.6 29.7
47 48	9.55 036	33	9.57 963	38 38	0.42 075	9.97 073	5	13 12	
<del>49</del> <b>50</b>	9.55 069	33 33	9.58001	38	0.41 999	9.97 068	5 5	11	5   4
51	9.55 102 9.55 136	34	9.58 039 9.58 077	38	0.41 961 0.41 923	9.97 063 9.97 059	4	10	.1 0.5 0.4
52	9.55 169	33 33	9.58 115	38 38	0.41 885	9.97 054	5	8	.3 1.5 1.2
53 54	9.55 202 9.55 235	33	9.58 153 9.58 191	38	0.41 847 0.41 809	9.97 049	5 5	7 6	.4  2.0  I.0
	9.55 268	33	9.58 229	38	0.41 771	9.97 044 9.97 039	5	5	.5 2.5 2.0 .6 3.0 2.4 .7 3.5 2.8 .8 4.0 3.2
55 56	9.55 301	33 33	9.58 267	38 37	0.41 733	9.97 035	4	4	.7  3.5  2.8
57 58	9 · 55 334 9 · 55 367	33	9.58 304 9.58 342	38	0.41 696 0.41 658	9.97 030 9.97 023	5 5	3 2	.8 4.0 3.2 .9 4.5 3.6
1 59	9.55 400	33 33	9.58 380	38	0.41 620	9.97 025	5	I	71 7731 310
60	9.55 433		9.58 418	38	0.41 582	9.97 015	5.	0	
	L. Cos.	d.	L. Cotg.	c. d.	L. Tang.	L. Sin.	d.	,	Prop. Pts.
					69°				

	21°										
	L. Sin.	d.	L. Tang.	c. d.	L. Cotg.	L. Cos.	d.		Prop. Pts.		
0	9 55 433	33	9.58 418	37	0.41 582	9.97 015	5	60			
1 2	9.55 466 9.55 499	33	9.58 455 9.58 493	38	0.41 545	9.97 010 9.97 005	5	59 58			
3	9.55 532	33 32	9.58 531	38 38	0.41 469	9.97 001	4 5	57	38 37 .1 3.8 3.7		
4	9.55 564	33	9.58 569 9.58 606	37	0.41 431	9.96 996	5	56	2 7.6 7.4		
5	9 55 597 9 55 630	33	9.58644	38	0.41 394	9.96 991 9.96 986	5	55 54	.3 11.4 11.1		
7 8	9.55 663	33 32	0.58 68i	37 38	0.41 319	9.96 981	5 5	53	.4 15.2 14.8 .5 19.0 18.5		
9	9.55 695 9.55 728	33	9.58 719 9.58 757	38	0.41 281	9.96976 9.96971	5	52 51	.6 22.8 22.2		
10	9.55 761	33	0.58 704	37	0.41 206	9.96 966	5	50	.7 26.6 25.9 .8 30 4 29.6		
11	9.55 793	32 33	0.58 832	38 37	0.41 168	9.96 962	4	49 48	.9 34.2 33.3		
12 13	9.55 826 9.55 858	32	9.58 869 9.58 907	38	0.41 131	9.96 957 9.96 952	5 5				
14	9.55 891	33	9.58 944	37	0.41 056	9.96 947	5	47 46	36   33		
15	9.55 923	32 33	9.58 981	37 38	0.41 019	9.96 942	5	45	.1 3.6 3.3		
16	9,55 956	32	9.59 019	37	0.40 981	9.96 937	5 5	44	.2 7.2 6.6 .3 10.8 9.9		
17 18	9.55 988 9.56 021	33	9.59.056 9.59.094	38	0.40 944	9.96 93 <b>2</b> 9.96 927	5	43 42	.4 14.4 13.2		
19	9.56 053	. 32 32	9.59 131	37 37	0.40.869	9.96 922	5 5	41	.5 18.0 16.5 .6 21.6 19.8		
20	9.56 085	33	9.59 168	37	0.40 832	9.96 917	5	40			
2I 22	9.56 118 9.56 150	32	9.59 205 9.59 243	38	0.40 795	9.96 912 9.96 907	5	-39 38	.8 28.8 26.4		
23	9.56 182	32 33	9.59 280	37 37	0.40 720	9.96 903	4	37	·9 32·4 29·7		
24	9.56 213	32	9.59 317	37	0.40 683	9.96 898	5	36			
25 26	9.56 247 9.56 279	32	9·59 354 9·59 391	37	0.40 646	9.96 893 9.96 888	5	35	32		
27 28	9.56 311	32	9.59 429	38	0.40 571	9.96 883	5	34 33	.1 3.2 .2 6.4		
	9.56 343	32 32	9.59 466	37 37	0.40 534	9.96.878	5 5	32	.2 6.4 .3 9.6		
29 <b>80</b>	9.56 375	33	9.59 503	37	0.40 497	9.96 873 9.96 868	5	31 <b>80</b>	.4 12.8		
31	9.56 440	32	9.59 577	37	0.40 423	9.96 863	5	29	.5 16.0 .6 19.2		
32	9.56 472	32 32	9.59 614	37 37	0.40 386	9.96 858	5	28			
33 34	9.56 504 9.56 536	32	9.59 651 9.59 688	37	0.40 349	9.96 853 9.96 848	5	27 26	.8 25.6		
	9.56 568	32	9.59 725	37	0.40 275	9 96 843	5	25	.9 28.8		
35 36	9.56 599	31 32	9.59 762	37 37	0.40 238	9.96 838	5	24			
37 38	9.56 631 9.56 663	32	9 · 59 799 9 · 59 835	36	0.40 201	9.96 833 9.96 828	5	23 22	31   6		
39	9.56 695	32	9.59 872	37	0.40 128	9.96 823	5	21	.I 3.I 0.6 .2 6.2 1.2		
40	9.56 727	32 32	9.59 909	37 37	0.40 091	9.96 818	5	20	.2 6.2 I.2 .3 9.3 I.8		
41 42	9.56 759 9.56 790	31	9.59 946 9.59 983	37	0.40 054	9.96 813 9.96 808	5 5	19 18	.4 12.4 2.4		
43	9 56 822	32	9.59.903	36	0.39 981	9.96 803	5	17	.5 15.5 3.0 .6 18.6 3.6		
44	9 . 56 854	32 32	9.60 056	37 37	0.39 944	9.96 798	5 5	16	.7 21.7 4.2		
45 46	9.56 886 9.56 917	31	9.60 093	37	0.39 907	9.96 793 9.96 788	5	15			
47	9.56 949	32	9.60 130 9.60 166	36	0.39 834	9.96 788 9.96 783	5	14 13	.9127.9 5.4		
47 48	9.56 980	31 32	9.60 203	37 37	0.39 797	9.96 778	5 6	12	.		
49 <b>50</b>	9.57 012	32	9.60 240	36	0.39 760	9.96 772	5	10	5 4		
5I	9.57 044 9.57 075	31	9.60 276 9.60 313	37	0.39 724	9.96 767 9.96 762	5		.I 0.5 0.4 .2 I.0 0.8		
52 53	9.57 107	32 31	9.60 349	36 37	0.39 651	9.96 757	5	8	.3 1.5 1.2		
53 54	9.57 138 9.57 169	31	9.60 386 9.60 422	36	0.39 614	9.96 752	5 5	7 6	.4 2.0 1.6		
	9.57 201	32	9.60 459	37	0.39 5/8	9.96 747	5	$\frac{6}{5}$	.5 2.5 2.0 .6 3.0 2.4		
56	9.57 232	31	9.60 495	36	0.39 505	9.96 737	5	4	.7 3.5 2.8		
57	9.57 264	32 31	9.60 532 9.60 568	37 36	0.39 468	9.96 732 9.96 727	5 5	3 2	.8 4.0 3.2 .9 4.5 3.6		
55 56 57 58 59	9.57 295 9.57 326	31	9.60 605	37	0.39 432	9.96 727	5	1	7.51 3.0		
60	9.57 358	32	9.60 641	36	0.39 359	9.96 717	5	0			
	L. Cos.	d.	L. Cotg.	6. d.		L. Sin.	d.		Prop. Pts.		
					68°						

	22°											
,	L. Sin.	d.	L. Tang.	c. d.	L. Cotg.	L. Cos.	d.		Prop. Pts.			
Ō	9.57 358	31	9.60 641	36	0.39 359	9.96 717	6	60				
1 2	9.57 389 9.57 420	31	9.60 677 9.60 714	37	0.39 323	9.96 711 9.96 706	5	59 58	1 1			
3	9.57 451	31 31	9 60 750	36 36	0.39 250	9.96 701	5 5	57	.1 37 36 .1 3.7 3.6			
4	9.57 482	32	9.60 786	37	0.39 214	9.96 696 9.96 691	5	56	.2 7.4 7.2			
5	9 - 57 543	31	9.60 859	36	0.39 177 0.39 141	9.96 686	5	55 54	.3 11.1 10.8 .4 14.8 14.4			
7 8	9.57 576 9.57 607	31 31	9.60 895	36 36	0.39 105	9.96 681	5 5	53	.5 18.5 18.0			
ا ۋ	9.57 638	31	9.60 931 9.60 967	36	0.39 069	9.96676 9.96670	6	52 51	6 22.2 21.6			
10	9.57 669	31	9.61 004	37 36	0.38 996	9.96 665	5	50	.8 29.6 28.8			
11 12	9.57 700 9.57 73I	31	9.61 040 9.61 076	36	0.38 960 0.38 924	9.96 660	5 5	49 48	.9   33.3   32.4			
13	9.57 762	31	9.61 112	36	0.38 888	9.96 655 9.96 650	5	40				
14	9 - 57 793	31 31	9.61 148	36 36	0.38 852	9 96 643	5	46	35			
15 16	9.57 824 9.57 855	31	9.61 184 9.61 220	36	0.38 816	9.96 640	6	45	.I 3.5 .2 7.0			
17	9.57 885	30	9.61 256	36	0.38 780	9.96 634 9.96 629	5	44 43	.3 10.5			
18	9.57 916	31	9.61 292	36 36	0.38 708	9 96 624	5	42	.4 I4.0 .5 17.5			
19 <b>20</b>	9.57 947	31	9.61 328	36	0.38 672	9.96 619	5	41 40	.6 21.0			
21	9.58 008	30	9.61.304	36	0.38 600	9.96 608	6		.7 24.5 .8 28.0			
22	9.58 039 9.58 070	31 31	9.61 436	36 36	0.38 564	9.96 603	5 5	39 38	9 31.5			
23 24	9.58 101	31	9.61 472 9.61 508	36	0.38 528	9.96 598 9.96 593	5	37 36	3.0			
25 26	9.58 131	30 31	9.61 544	36	0.38 456	9.96 588	5	35	32   31			
	9.58 162 9.58 192	30	9.61 579	35 36	0.38 421	9 96 582	6 5	34	.I 3.2 3.I			
27 28	9.58 223	31	9.61.615	36	0.38 385	9.96 577	5	33 32	.2 6.4 6.2			
29	9.58 253	30 31	9.61 687	36 35	0.38 313	9 96 567	5	31	.3 9.6 9.3 .4 12.8 12.4			
80	9.58 284 9.58 314	30	9 61 722	36	0.38 278	9 96 562	6	80	.5 16.0 15.5			
31 32	9.58 345	31	9.61 758 9.61 794	36	0.38 242	9 96 556 9 96 551	5	29 28	.6 19.2 18.6 .7 22.4 21.7			
33	9.58 375	30 31	9.61 830	36 35	0.38170	9 96 546	5	27	.8 25.6 24.8			
34	9.58 406	30	9.61 865 9.61 901	36	0.38 135	9.96 541	6	26	.9 28.8 27.9			
35 36	9.58 467	31	9.61 936	35	0.38 064	9 96 535 9 96 530	5	25 24				
37 38	9.58 497 9.58 527	30 30	9.61 972	36 36	0.38 028	9.96 523	5	23	30   29			
39	9.58 557	30	9.62 008	35	0.37 992 0.37 957	9.96 520 9.96 514	6	22 21	.I 3.0 2.9 .2 6.0 5.8			
40	9.58 588	31	9.62 079	36	0.37 921	9.96 509	5	20	.2 6.0 5.8 .3 9.0 8.7			
41 42	9.58 618 9.58 648	30 30	9.62 114	35 36	0 37 886	9 96 504	5 6	19	.4 12.0 11.6			
43	9.58 678	30	9.62 185	35	0.37 850	9.96 498 9.96 493	5	18	.5 15.0 14.5 .6 18.0 17.4			
44	9.58 709	31 30	9.62 221	36 35	0.37 779	9 96 488	5 5	16	7 21.0 20.3 8 24.0 23.2			
45 46	9.58 739 9.58 769	30	9.62 256 9.62 292	36	0.37 744	9.96 483	6	15				
47 48	9.58 799	30	9.62 327	35	0.37 708	9 96 477 9 96 472	5	14 13	.9  27.0  26.1			
48 49	9.58 829 9.58 859	30 30	9.62 362	35 36	0.37 638	9.96 467	5	12				
<b>50</b>	9.58 889	30	9.62 398	35	0.37 602	9.96 461	5	10	.I 0.6 0.5			
51	9.58 919	30	9.62 433 9.62 468	35	0.37 532	9.96 451	5	9	.I 0.6 0.5 .2 I.2 I.0			
52 53	9.58 949 9.58 979	30	9.62 504	36 35	0.37 496	9 96 445	6 5	8	.3 1.8 1.5			
54	9.59 009	30	9.62 539 9.62 574	35	0.37 461	9.96 440 9.96 433	5	7 6	.4 2.4 2.0 .5 3.0 2.5			
55	9.59 039	30 30	9.62 600	35	0.37 391	9.96 429			6 3.6 3.0			
55 56 57 58 59	9.59 069 9.59 098	29	9.62 64 <del>5</del> 9.62 680	36 35	0.37 355	9.96 424	5 5	5 4 3 2	.7 4.2 3.5 .8 4.8 4.0			
58	9.59 128	30	9.62 713	35	0.37 320 0.37 285	9 96 419 9 96 413	6	3	.8 4.8 4.0 .9 5.4 4.5			
<u>59</u>	9.59 158	30	9.62 750	35 35	0.37 250	9.96 408	5 5	1	,			
<del> </del>			9.62 785		0.37 215	9.96 403		9				
<u> </u>	L. Cos.	d.	I L. Cotg.	c. d.	L. Tang.	L. Sin.	d.	,	Prop. Pts.			
					67°							

	23°											
,	L. Sin.	d.	L. Tang.	c. d.	L. Cotg.	L. Cos.	d.		Prop. Pts.			
0	9.59 188	30	9.62 785	35	0.37 215	9.96 403	6	60				
I 2	9.59 218 9.59 247	29	9.62 820 9.62 855	35	0.37 180	9.96 397 9.96 <b>392</b>	5	59 58				
3	9.59 277	30 30	9.62 890	35 36	0.37 110	9.96 387	5 6	57	.1 3.6 3.5			
4	9.59 307	29	9.62 926	35	0.37 074	9.96 381	5	56	.2 7 2 7.0			
5 6	9.59 336 9.59 366	30	9.62 961 9.62 996	35	0.37 039 0.37 <b>0</b> 04	9.96 376 9.96 370	6	55 54	.3 10.8 10.5 .4 14.4 14.0			
7 8	9.59 396	30 29	9.63 031	35 35	0.36 969	9.96 365	5	53	.5 18.0 17.5			
9	9 · 59 42 <u>5</u> 9 · 59 455	30	9.63 066 9.63 101	35	o.36 934 o.36 899	9.96 360 9.96 354	6	52 51	6 21.6 21.0			
10	9.59 484	29	9.63 135	34	0.36 865	9.96 349	5	50	.7 25.2 24.5 .8 28.8 28.0			
11	9.59 514	30 29	9.63 170	35 35	0.36 830	9.96 343	6 5	49 48	9 32.4 31.5			
12 13	9·59 543 9·59 573	30	9.63 205	35	0.36 795 0.36 760	9.96 338 9.96 333	. 5	48 47				
14	9.59 602	29 30	9.63 275	35 35	0.36 725	9.96 327	6 5	46	34			
15 16	9.59 632	29	9.63 310	35	0.36 690	9.96 322	6	45	.1 3.4 .2 6.8 V			
17	9.59 661 9.59 690	29	9.63 343 9.63 379	34	0.36 655 0.36 621	9.96 316	5	44	.3 10.2			
18	9.59 720	30 29	9.63 414	35 35	0.36 586	9.96 305	6 5	42	.4 13.6			
19 <b>20</b>	9.59 749	29	9.63 449	35	0.36 551	9.96 300	6	41	.5 17.0 .6 20.4			
2U 2I	9.59 778 9.59 808	30	9.63 484 9.63 519	35	0.36 516 0.36 481	9.96 <b>294</b> 9.96 289	5	40	.7 23.8			
22	9.59 837	29 29	9.63 553 9.63 588	34 35	0.36 447	9.96 284	5	39 38	.8 27.2 .9 30.6			
23 24	9.59 866 9.59 895	29	9.63 588 9.63 623	35	0.36 412	9.96 278 9.96 273	5	37 36	.91 30.0			
25	9.59 924	29	9.63 657	34	0.36 343	9.96 267	6	35	l i			
26	9 59 954	30 29	9.63 692	35 34	0.36 308	9.96 262	5	34	30 29 .1 3.0 2.9			
27 28	9.59 983 9.60 012	29	9.63 <b>726</b> 9.63 <b>7</b> 61	35	0.36 274	9.96256	5	33	.I 3.0 2.9 .2 6.0 5.8 .3 9.0 8.7			
29	9.60 041	29	9.63 796	35	0.36 204	9.96 245	6	32 31				
80	9.60 070	29 29	9.63 830	34 35	0.36 170	9.96 240	5 6	80	.4 12.0 11.6 .5 15.0 14.5			
31 32	9.60 099 9.60 128	29	9.63 865 9.63 899	34	0.36 135	9.96 234 9.96 229	5	29 28	.6 18.0 17.4			
33	9.60 157	29	9.63 934	35	0.36 066	9.96 223	6	27	.7 21.0 20.3 .8 24.0 23.2			
34	9.60 186	29 29	9.63 968	34 35	0.36 032	9.96 218	5 6	26	.9 27.0 26.1			
35 36	9.60 21 <del>3</del> 9.60 244	29	9.64 003 9.64 037	34	0.35 997 0.35 963	9.96 212 9.96 207	5	25 24				
37 38	9.60 273	29 29	9.64 072	35	0.35 928	9.96 201	6	23	1 28			
38 39	9.60 302 9.60 331	29	9.64 106 9.64 140	34 34	o.35 894 o.35 860	9.96 196	5 6	22 21	.1 2.8			
40	9.60 359	28	9.64 175	35	0.35 825	9.96 190	5	20	.2 5.6 .3 8.4			
41	9.60 388	29 29	9.64 209	34	0.35 791	9.96 179	6	19	.4 11.2			
42 43	9.60 417 9.60 446	29	9.64 243	34 35	0.35 757	9.96 174 9.96 168	5	18	.5 14.0			
43	9.60 474	28	9.64 312	34	0.35 722 0.35 688	9.96 162	6	17 16	.6 16.8 .7 19.6			
45 46	9.60 503	29 29	9.64 346	34 35	0.35 654	9.96 157	5 6	15	.8 22.4			
40	9.60 532 9.60 561	29	9.64 381 9.64 41 <del>5</del>	34	0.35 619	9.96 151 9.96 146	5	14	.9 25.2			
47 48	9.60 589	28	9 64 449	34	0.35 551	9.96 140	6	13 12				
49	9.60618	29 28	9.64 483	34 34	0.35 517	9.96 135	5 6	11	6   5			
50 51	9.60 646 9.60 675	29	9.64 517	35	0.35 483 0.35 448	9.96 129 9.96 123	6	10 9	.1 0.6 0.5 .2 1.2 1.0			
52	9.60 704	28	9.04.586	34	0.35 414	9.96 118	5	8				
53 54	9.60 732 9.60 76.	20	9.64 620 9.64 654	34 34	0.35 380	9.96 112	6 5	7	.4 2.4 2.0			
55	9.60 789	28	9.64 688	34	0.35 346	9.96 107	6		.5 3.0 2.5 .6 3.6 3.0			
56	9.60 818	29 28	9.64 722	34	0.35 278	9.96 095	6	5 4 3 2	1 .7   A.2   3.5			
57	9.60 846 9.60 873	29	9.64.756	34 34	0.35 244 0.35 210	9.96 090 9.96 084	5 6	3	.8 4.8 4.0 .9 5.4 4.5			
55 56 57 58 59 <b>60</b>	9.60 903	28 28	9.64 790 9.64 824	34	0.35 176	9.96 079	5	1	1.51 7.71 7.3			
60	9.60 931	20	9.64 858	34	0.35 142	9.96 073	6	0				
	L. Cos.	d.	L. Coty.	c. d.	L. Tang.	L. Sin.	d.	7	Prop. Pts.			
!					66°							

	24°											
,	L. Sin.	d.	L. Tang.	c. d.	L. Cotg.	L. Cos.	d.		Prop. Pts.			
0	9.60 931	29	9.64 858	34	0.35 142	9.96 073	6	60	***************************************			
I 2	9.60 960 9.60 988	28	9.64 892 9.64 926	34	0.35 108	9.96 067 9.96 062	5	59 58				
3	9.61 016	28 29	9.64 960	34 34	0.35 040	9.96 056	6	57 56	34 33 .1 3.4 3.3			
4	9.61 045	28	9.64 994	34	0.35 006	9.96 050	5	56	6.8 6.6			
5	9.61 101	28	9.65 028 9.65 062	34	0.34 972 0.34 938	9.96 04 <b>3</b> 9.96 039	6	55 54	.3 IO.2 9.9 .4 I3.6 I3.2			
7	9.61 129	28 29	9.65 096	34 34	0.34 004	9.96 034	5	53	2   17 0   16 C			
9	9.61 158 9.61 186	28	9.65 130 9.65 164	34	0.34 870 0.34 836	9.96 028 9.96 022	6	52 51	.5 17.0 16.5 .6 20.4 19.8			
10	9.61 214	28 28	9.65 197	33	0.34 803	9.96 017	5	50	.7 23.8 23.1 .8 27.2 26.4			
11	9.61 242	28	9.65 231	34 34	0.34 769	9.96 011	6	49 48	.9 30.6 29.7			
12	9.61 270 9.61 298	28	9.65 265 9.65 299	34	0.34 735 0.34 701	9.96 005 9.96 000	5	48 47				
14	9.61 326	28 28	9.65 333	34 33	0.34 667	9.95 994	6	46	29			
15 16	9.61 354 9.61 382	28	9.65 366	34	0.34 634	9.95 988	6	45	.I 2.9 2 5.8			
	9.61 411	29	9.65 400 9.65 434	34	0.34 600	9.95 982 9.95 977	5	44 43	3 8.7			
17 18	9.61 438	27 28	9.65 467	33	0.34 533	9.95 971	6	42 42	.4 11.6			
19 <b>20</b>	9.61 466	28	9.65 501	34 34	0.34 499	9.95 965	5	41	.5 14.5 .6 17.4			
2U 2I	9.61 494 9.61 522	28	9.65 53 <del>\$</del> 9.65 568	33	0.34 465 0.34 432	9.95 960 9.95 954	6	40	.7 20.3			
22	9.61 550	28 28	9.65 602	34 34	0.34 398	9.95 948	6	39 38	.8 23.2 .9 26.1			
23 24	9.61 578 9.61 606	28	9.65 636 9.65 669	33	0.34 364 0.34 331	9.95 942 9.95 937	5	37 36	.91 -0.1			
	9.61 634	28	9.65 703	34	0.34 297	9.95 931	6	35				
25 26	9.61 662	28 27	9.65 736	33 34	0.34 264	9.95 925	6	34	.1 2.8			
27 28	9.61 689 9.61 717	28	9.65 770 9.65 803	33	0.34 230 0.34 197	9.95 920	5	33	.2 5.6			
29	9.61 743	28 28	9.65 837	34	0.34 163	9.95 914 9.95 908	6	32 31	.3 8.4 .4 II.2			
80	9.61 773	27	9.65 870	33 34	0.34 130	9.95 902	5 -	80				
3I 32	9.61 800 9.61 828	28	9.65 904 9.65 937	33	0.34 096	9.95 897 9.95 891	6	29 28	.6 16.8			
33	9.61 856	28 27	9.65 971	34	0.34 029	9.95 885	6 6	27	.7 19.6 .8 22.4			
34	9.61 883	28	9.66 004	33 34	0.33 996	9.95 879	6	26	.9 25.2			
35 36	9.61 911 9.61 939	28	9.66 038 9.66 071	33	0.33 962 0.33 929	9.95 873 9.95 868	5	25 24				
37 38	9.61 966	27 28	9.66 104	33	0.33 896	9.95 862	6	23	27			
38 39	9.61 994 9.62 021	27	9.66 138 9.66 171	34 33	0.33 862 0.33 829	9.95 856 9.95 850	6	22 21	.1 2.7			
40	9.62 049	28	9.66 204	33	0.33 796	9.95 844	6	20	.2 5.4 .3 8.1			
41	9.62 076	27 28	9.66 238	34 33	0.33 762	9.95 839	5 6	19 18	.3 8.1 .4 10.8			
42 43	9.62 104 9.62 131	27	9.66 271 9.66 304	33	0.33 729 0.33 696	9.95 833 9.95 827	6		.5 13.5 .6 16.2			
44	9.62 159	28 27	9.66 337	33	0.33 663	9.95 821	6	17 16	.6 16.2 .7 18.9			
45 46	9.62 186	27	9.66 371	34 33	0.33 629	9.95 815	6 5	15	.8 21.6			
40 47	9.62 214 9.62 241	27	9.66 404 9.66 437	33	0.33 596 0.33 563	9.95 810 9.95 804	6	14 13	.9 24.3			
47 48	9.62 268	27 28	9.66 470	33	0.33 530	9.95 798	6	12				
<u>49</u> <b>50</b>	9.62 296	27	9.66 503	33 34	0.33 497	9.95 792	6	11	6 5			
	9.62 350	27	9.66 537 9.66 570	33	0.33 463 0.33 430	9.95 786 9.95 780	6	10	.1 0.6 0.5 .2 1.2 1.0			
51 52	9.62 377	27 28	9.66 603	33 33	0.33 397	9.95 775	5	8	.3 1.8 1.5			
53 54	9.62 40 <del>3</del> 9.62 432	27	9.66 636 9.66 669	33	0.33 364 0.33 331	9.95 769 9.95 763	6	7 6	.4 2.4 2.0			
	9.62 459	27	9.66 702	33	0.33 298	9.95 757	6		.4 2.4 2.0 .5 3.0 2.5 .6 3.6 3.0			
55 56 57 58 59	9 62 486	27 27	9.66 735 9.66 768	33 33	0.33 265	9.95 751	6 6	5 4 3 2	1 .7   4.2   3.5			
57   58	9.62 513 9.62 541	28	9.66 801	33	0.33 232 0.33 199	9 · 95 745 9 · 95 739	6	3	.8 4.8 4.6 .9 5.4 4.5			
59	9.62 568	27 27	9.66 834	33	0.33 166	9.95 733	6	1	7, 3, 1, 4,3			
60	9.6 2593		9.66 867	33	0.33 133	9.95 728	5	0				
	L. Cos.	d.	L. Cotg.	c. d.	L. Tang.	L. Sin.	d.	,	Prop. Pts.			
					65°							

	25°											
,	L. Sin.	d.	L. Tang.	c. d.	L. Cotg.	L. Cos.	d.		Prop. Pts.			
0	9.62 593	27	9.66 867	33	0.33 133	9.95 728	6	60				
I 2	9.62 622 9.62 649	27	9.66 900 9.66 933	33	0.33 100	9.95 722 9.95 716	6	59 58				
3	9.62 676	27 27	9.66 966	33 33	0.33 034	9.95 710	6	57	.1 3.3 3.2			
4	9.62 703	27	9.66 999	33	0.33 001	9.95 704	6	56	.1 3.3 3.2 .2 6.6 6.4			
5 6	9.62 730 9.62 757	27	9.67 032 9.67 063	33	0.32 968 0.32 935	9 95 698 9 95 692	6	55	.3 9.9 9.6			
7 8	9.62 784	27 27	9.67 098	33	0.32 902	9.95 686	6	54 53	.4 13.2 12.8 .5 16.5 16.0			
	9.62 811 9.62 838	27	9.67 131	33 32	0.32 869	9.95 680	6	52	.6 19.8 19.2			
9 10	9.62 863	27	9.67 163	33	0.32 837	9.95 668	6	51 50	.7 23.1 22.4 .8 26.4 25.6			
11	9.62 892	27 ·	9.67 229	33	0.32 771	9.95 663	5		.9 29.7 28.8			
12	9.62 918	27	9.67 262	33 33	0.32 738	9.95 657	6	49 48				
13 14	9.62 945 9.62 972	27	9.67 29 <del>5</del> 9.67 327	32	0.32 705	9.95 651 9.95 643	6	47 46	1 27			
15	9.62 999	27	9.67 360	33	0.32 640	9.95 639	6	45	.1 2.7			
16	9.63 026	27 26	9.67 393	33 33	0.32 607	9.95 633	6	44	.2 5.4 3 8.1			
17 18	9.63 052 9.63 079	27	9.67 426 9.67 458	32	0.32 574 0.32 542	9.95 627 9.95 621	6	43 42	3 8.1 .4 10.8			
19	9.63 106	27 27	9.67 491	33	0.32 509	9.95 615	6	41	.5 13.5			
20	9.63 133	26	9.67 524	33 32	0.32 476	9.95 609	6	40				
2I 22	9.63 159 9.63 186	27	9.67 556 9.67 589	33	0.32 444	9.95 603 9. <b>95 5</b> 97	6	39 38	.8 21.6			
23	9.63 213	27 26	9.67 622	33	0.32 378	9 95 591	6 6	37	.9 24.3			
24	9.63 239	27	9.67 654	32 33	0.32 346	9.95 585	6	36				
25 26	9.63 266 9.63 292	26	9.67 687 9.67 719	32	0.32 313	9·95 579 9·95 573	6	35	26			
27 28	9.63 319	27 26	9.67 752	33	0.32 248	9.95 567	6	34	.1 2.6 .2 5.2			
	9 63 345	27	9.67 785	33 32	0.32 215	9.95 56 <u>1</u>	6	32	.3 7.8			
29 80	9.63 372 9.63 398	26	9.67.817	33	0.32 183	9 95 555	6	31 <b>80</b>	.4 10.4			
31	9.63 423	27	9.67 882	32	0.32 118	9 95 549 9 95 543	6	29	.5 13.0 .6 15.6			
32	9.63 451	26 27	9.67915	33 32	0.32 085	9.95 537	6	28	.7 18.2			
33 34	9.63 478 9.63 504	26	9.67 947 9.67 980	33	0.32 053	9.95 53 <u>1</u> 9.95 52 <u>5</u>	6	27 26				
	9.63 531	27	9.68 012	32	0.31 988	9.95 519	6	25	.9  23.4			
35 36	9.63 557	26 26	9.68 044	32 33	0.31 956	9.95 513	6	24				
37 38	9.63 583	27	9.68 077 9.68 109	32	0.31 923	9.95 507 9.95 500	7	23 22	7			
39 1	9.63 636	26 26	9.68 142	33	0.31 858	9 95 494	6	21	.I 0.7 .2 I.4			
40	9.63 662	27	9.68 174	32 32	0.31 826	9.95 488	6	20	.3 2.1			
41 42	9.63 689 9.63 715	26	9.68 206 9.68 239	33	0.31 794	9 95 482 9 95 476	6	19 18	.4 2.8 .5 3.5			
43	9.63 741	26 26	9.68 271	32 32	0.31 729	9.95 470	6	17	.6 4.2			
44	9.63 767	27	9 68 303	33	0.31 697	9.95 464	6	16	7 4.9			
45 46	9 63 794 9 63 820	26	9.68 336 9.68 368	32	0.31 664 0.31 632	9.95 458 9.95 452	6	15 14	.8 5.6 .9 6.3			
47 48	9.63 846	26 26	9.68 400	32	0.31 600	9.95 446	6	13	, ,			
48 49	9.63 872	26	9.68 432 9.68 46 <del>5</del>	33	0.31 568	9.95 440	6	12 11	1646			
50	9.63 898	26	9.68 497	32	0.31 535	9.95 434	7	10	.1 0.6 0.5			
51	9 63 950	26 26	9.68 529	32	0.31 471	9.95 421	6.	9	.2 1.2 t.0			
52 52	9.63 976 9.64 002	26	9.68 561	32	0.31 439	9.95 415	6	8 7 6	.3 1.8 1.5 .4 2.4 2.0			
53 54	9.64 028	26	9.68 593 9.68 626	33	0.31 407	9.95 409 9.95 403	6	6	.4 2.4 2.0 .5 3.0 2.5			
	9.64 054	26 26	9.68 658	32	0.31 342	9.95 397	6		.6  3.6  3.0			
56	9.64.080	26	9.68 690 9.68 722	32	0.31 310	9.95 391	7	5 4 3 2	.7 4.2 3.5 .8 4.8 4.0			
55 56 57 58 59	9.64 106 9.64 132	26	9.68 754	32	0.31 2/6	9.95 384 9.95 378	6		.9 5.4 4.5			
59	9.64 158	26 26	9.68 786	32 32	0.31 214	9.95 372	6	1				
60	9.64 184		9.68 818		0.31 182	9.95 366		0				
	L. Cos.	d.	L. Cotg.	c. d.	L. Tang.	L. Sin.	d.	, ,	Prop. Pts.			
					64°							

	26°										
,	L. Sin.	d.	L. Tang.	c. d.	L. Cotg.	L. Cos.	d.		Prop. Pts.		
0	9.64 184	26	9.68 818	32	0.31 182	9.95 366	6	60	<u> </u>		
I 2	9.64 210 9.64 236	26	9.68 850 9.68 882	32	0.31 1 <u>5</u> 0 0.31 118	9.95 360	6	59 58			
3	9.64 262	26 26	9.68 914	32	0.31 086	9.95 354 9.95 348	6	50 57	32 31		
4	9.64 288	25	9.68 946	32 32	0.31 054	9.95 341	7	56	.I 3.2 3.I .2 6.4 6.2		
5	9.64 313	26	9.68 978	32	0.31 022	9.95 335	6	55	.3 9.6 9.3		
	9.64 339 9.64 365	26	9.69 010	32	0.30 990	9.95 329 9.95 323	6	54	.4 12.8 12 4		
8	9.64 391	26 26	9.69 074	32 32	0.30 926	9.95 317	6	53 52	.5 16.0 15 5 .6 19.2 18.6		
9	9.64 417	25	9.69 106	32	0.30 894	9.95 310	7 6	51	.7 22.4 21.7		
10	9.64 442 9.64 468	26	9.69 138 9.69 170	32	0.30 862	9.95 304	6	50			
12	9.64 494	26	9.69 202	32	0.30 830	9.95 298 9.95 292	6	49 48	.9   28.8   27.9		
13	9.64 519	25 26	9.69 234	32 32	0.30 766	9.95 286	6	47			
14	9.64 545	26	9.69 266	32	0.30 734	9 95 279	7	46	.1 2.6		
15 16	9.64 571 9.64 596	25	9.69 298 9.69 329	31	0.30 702	9.95 273 9.95 267	6	45	.1 2.6 .2 5.2		
17	9.64 622	26 25	9.69 361	32	0.30 639	9.95 261	6	44 43	.3 7.8		
18	9.64 647	25 26	9 69 393	32 32	0.30 607	9.95 254	7	42	.4 10.4		
19 26	9.64.673	25	9.69 425	32	0.30 575	9 95 248	6	41	.5 13.0 .6 15.6		
20 21	9.64 698 9.64 724	26	9.69 457 9.69 488	31	0.30 543	9.95 242	6	40	.7 18.2 .8 20.8		
22	9.64 749	25 26	9.69 520	32	0.30 480	9.95 236 9.95 229	7	39 38			
23	9.64 773	25	9.69 552	32	0.30 448	9.95 223	6	27	.9 23.4		
24	9.64 800	26	9.69 584	31	0.30 416	9.95 217	6	36			
25 26	9.64 826 9.64 851	25	9.69 615 9.69 647	32	0.30 385	9.95 211	7	35	25		
	9.64 877	26	9.69.679	32	0.30 353	9.95 204 9.95 198	6	34 33	.1 2.5		
27 28	9.64 902	25 25	9.69 710	31 32	0.30 290	9.95 192	6	32	.2 5.0		
29	9 64 927	26	9 69 742	32	0.30 258	9 95 185	7	31	.3 7.5 .4 10.0		
<b>30</b> 31	9.64 953 9.64 978	25	9.69 774 9.69 805	31	0.30 226	9.95 179	6	80	.5 12.5		
32	9.65 003	25	9.69 827	32	0.30 195	9.95 173 9.95 167	6	29 28	.6 15.0		
33	9.65 029	26 25	9.69.868	31	0.30 132	9.95 160	7 6	27	.7 17.5 .8 20.0		
34	9.65 054	25	9.69 900	32	0.30 100	9.95 154	6	26	.9 22.5		
35 36	9.65 079 9.65 104	25	9.69 932	31	0.30 068	9.95 148	7	25			
37	9.65 130	26	9.69 995	32	0.30 037	9.95 141 9.95 13 <b>5</b>	6	24 23			
37 38	9.65 153	25 25	9.70 026	31 32	0.29 974	9.95 129	6	22	.I 2.4		
39	9.65 180	25	9.70 058	31	0.29 942	9.95 122	7 6	21	.I 2.4 .2 4.8		
40 41	9.65 205 9.65 230	25	9.70 089 9.70 121	32	0.29 911	9.95 116	6	20	.3 7.2		
42	9.65 255	25	9.70 152	31	0.29 848	9.95 110 9.95 103	7	19	.4 9.6 .5 12.0		
43	9.65 281	26 25	9.70 184	32 31	0.29 816	9.95 097	6	17	.5 12.0 .6 14.4		
44	9.65 306	25	9.70 215	32	0.29 783	9.95 090	7	16	.7 16.8		
45 46	9.65 331 9.65 356	25	9.70 247 9.70 278	31	0.29 753	9.95 084	6	15			
47 48	9.65 381	25	9.70 309	31	0.29 722	9.95 078 9.95 071	7	14 13	.9 21.6		
48	9.65 406	25 25	9.70 341	32 31	0.29 659	9.95 o6 <b>₹</b>	6	12			
49 <b>50</b>	9.65 431	25	9.70 372	32	0.29 628	9.95 059	6 7	11	7 6		
51	9.65 456 9.65 481	25	9.70 404 9.70 435	31	0.29 596	9.95 052	6	10	.1 0.7 0.6		
52	9.65 506	25	9.70 466	31	0.29 565	9.95 046 9.95 039	7	9 8	.2 I.4 I.2 .3 2.1 I.8		
52 53 54	9.65 531	25 25	9.70 498	32	0.29 502	9.95 033	6	7	.4 2.8 2.4		
54	9.65 556	24	9.70 529	31	0.29 471	9.95 027	7		.5 3.5 3.0		
55 56	9.65 605	25	9.70 560 9.70 592	32	0.29 440	9.95 020	6	5 4	.5 3.5 3.0 .6 4.2 3.6 .7 4.9 4.2 .8 5.6 4.8		
57 58	9.65 630	25	9.76 623	31	0.29 408	9.95 014 9.95 007	7	4	.7 4.9 4.2 .8 5.6 4.8 .9 6.3 5.4		
58	9.65 655	25 25	9.70 654	31	0.29 346	9.95 ∞1	6 6	3 2	.9 6.3 5.4		
<u>59</u> <b>60</b>	9.65 680	25	9.70 685	32	0.29 315	9 94 995	7	1			
<u> </u>	9.65 70\$		9.70 717	_	0.29 283	9.94 988		0			
اـــــــــــــــــــــــــــــــــــــ	L. Cos.	d.	L. Cotg.	c. d.		L. Sin.	d.	,	Prop. Pts.		
					63°						

	2 <b>7</b> °											
	L. Sin.	d.	L. Tang.	c. d.		L. Cos.	d.	1	Prop. Pts.			
0	9.65 703	24	9.70 717	31	0 29 283	9.94 988	6	60				
I 2	9.65 729 9.65 754	25	9.70 748 9.70 779	31	0.29 252 0.29 221	9.94.982	7	59 58	4 4 1			
3		25	9.70 810	3E	0.29 190	9.94 969	6	57	32 3E 3E 3.1			
4	9.65 779 9.65 804	25 24	9.70 841	31 32	0.29 159	9 94 962	7	57 56	.2 6.4 6.2			
5	9.65 828	25	9.70 873	31	0.29 127	9.94 956	7	55	.3 9.6 9.3			
7	9 65 853 9 65 878	25	9.70 904 9.70 935	3 <b>E</b>	0.29 096	9 94 949 9 94 94 <b>3</b>	6	54 53	.4 12.8 12.4 .5 16.0 15.5			
7 8	9 65 902	24 25	9.70 966	31 31	0.29 034	9.94 936	7	52	.6 19.2 18.6			
9	9.65 927	25	9.70 997	31	0.29 003	9.94 930	7	51	.7 22.4 21.7			
10	9.6 <b>5</b> 952 9.65 976	24	9.71 028	31	0.28 972 0.28 941	9.94.923	6	50	.8 25.6 24.8 .9 28.8 27.9			
12	9.66 001	25	9.71 090	31	0.28910	9.94 911	6	49 48	.91 20.01 27.9			
13	9.66 025	24 25	9.71 121	31 32	0.28 879	9.94 904	7	47	1.00			
14	9.66 050	25	9 71 153	31	0.28 847	9.94 898	7	46	.1 3.0			
15 16	9.66 075 9.66 099	24	9.71 184	3x	0.28 785	9.94.891 9.94.885	6	45 44	.1 3.0 .2 6.0			
17	9.66 124	25	9.71 246	31	0.28 754	9.94878	7	43	3 90			
	9.66 148	24 25	9.71 277	31 31	0.28 723	9 94 871	7	42	.4 I2.0 .5 I5.0			
19 <b>20</b>	9.66 173 9.66 197	24	9.71 308	31	0.28 661	9 94 86 <del>3</del> 9 94 85 <b>8</b>	7	41 40	.6 18.o			
21	9.66 221	24	9.71 339 9.71 370	31	0.28 630	9.94.852	6		.7 21.0 .8 24.0			
22	9.66 246	25 24	9.71 401	3E 30	0.28 599	9.94 845	7	39 38	.8 24.0 .9 27.0			
23	9.66 270 9.66 293	25	9.71 431	31	0.28 569	9.94.839	7	37 36	.9 (2).0			
24	9.66 319	24	9.71 462	31	0.28 507	9.94.832	6					
25 26	9 66 343	24	9.71 524	31	0.28 476	9.94 819	7	35 34	25 24			
27 28	9.66 368	25 24	9.71 555 9 71 586	3E	0.28443	9 94 813	6	33	.I 2.5 2.4 .2 5.0 4.8			
28	9.66 392 9.66 416	24	9 71 586	31	0.28 414	9.94.806 9.94.799	7	32 31	3 7.5 7.2			
30	9.66 441	25 .	9 71 617	3€	0.28 352	9 94 793	6	30	.4 10.0 9.6 .5 12.5 12.0			
31	9.66 463	24	9 71 679	31	0.28 321	9.94 786	7 6	29	.5 12.5 12.0 .6 15.0 14.4			
32	9.66 489	24	9 71 709	30	0.28 291	9.94 780	7	28	.7 17.5 16.8			
33	9.66 513 9.66 537	24	9 71 740 9 71 771	31	0.28 260	9 94 773 9 94 767	6	27 26				
	9.66 562	25	9.71 802	31	0.28 198	9.94 760	7	25	.9 22.5 21.6			
35 36	9.66 586	24 24	9.71 833	30	0.28 167	9 94 753	7	24				
37 38	9.66 610	24	9 71 863	31	0.28 137	9.94.747	7	23 22	23			
39	9.66 658	24	9.71 925	31	0.28 075	9.94 734	6	21	.I 2.3 .2 4.6			
40	9.66 682	24	9.71 955	30	0.28 045	9.94 727	7	20	.3 6.9			
41	9.66 706	24 25	9 71 986	31	0.28 014	9.94 720	6	19	.4 9.2			
42 43	9.66 731	24	9.72 017	31	0 27 983	9.94 714	7	18	.5 11.5 .6 13.8			
44	9.66 779	24	9.72 078	30	0.27 922	9.94 700	7	16				
45 46	9.66 803	24	9.72 109	31	0 27 891	9.94 694	6	15	.7 16.1 .8 18.4.			
46	9.66 827	24	9.72 140	39	0.27 860	9.94 687	7	14	.9 20.7			
47 48	9.66 851	24	9.72 170 9.72 201	31	0.27 799	9.94 674	6	13				
49	9.66 899	24	9 72 231	- 3ª	0.27 769	9.94 667	7	11	17 6			
50	9.66 922	24	9.72 262	32	0.27 738	9.94 660	6	10	.1 0.7 0.6			
51	9.66 946	24	9.72 293	30	0.27 707	9.94.654	7	8	.2 I.4 I.2 .3 2.1 I.8			
52 53	9.66 994	24	9.72 323 9.72 354	32	0.27 646	9.94.640	7	7	.4 2.8 2.4			
54	9.67 018	24	9.72 384	30 - 31	0.27 616	9.94 634	6	7 6				
55	9.67 042	24	9.72 413	30	0.27 585	9.94 627	7	5 4 3 2	.5 3.5 3.0 .6 4,2 3.6 .7 4,9 4.2 .8 5,6 4.8			
55 56 57 58 59	9.67 066	24	9 72 445	31	0.27 555	9 94 620	6	4 2	.7 4.9 4.2 .8 5,6 4.8 .9 6.3 5.4			
58	9.67 113	23	9 72 506	30	0.27 494	9.94 607	7		.9 6.3 5.4			
59	9.67 137	24	9.72 537	- 30	0.27 463	9.94 600	7	I				
60	9.67 161	.	9.72 567	-	0.27 433	9.94 593		0				
1	L. Cos.	d.	L. Cotg.	c. d	L. Tang.	L. Sin.	d.	,	Prop. Pts.			
					$62^{\circ}$							

. 28°										
,	L. Sin.	d.	L. Tang.	c. d.	L. Cotg.	L. Cos.	d.		Prop. Pts.	
0	9.67 161	24	9.72 567 9.72 598	33	0.27 433	9.94 593	6	60		
i 2	9.67 185 9.67 208	93	9.72 598	30	0.27 402 0.27 372	9.94 587 9.94 580	7	59 58	1 1	
3	9.67 232	24	9.72 659	32	0.27 341	9.94 573	7	57 I	.1 3.1 3.0	
4	9.67 256	24 24	9.72 689	30 31	0.27 311	9.94 567	7	56	.1 3.1 3.0 .2 6.2 6.0	
ş	9.67 280	83	9.72 720	300	0.27 280	9.94 560	7	55	.3 9.3 9.0	
	9.67 303	24	9.72 750 9.72 780	30	0.27 230 0.27 220	9.94 553 9.94 546	7	54 53	.4 12.4 12.0 .5 15.5 15.0	
8	9.67 350	93 94	9.72 811	31	0.27 189	9.94 540	6	52	.5 15.5 15.0 .6 18.6 18.0	
9	9.67 374	24	9.72 841	30 31	0.27 159	9.94 533	7 7	51	.7 21.7 21.0	
10	9.67 398 9.67 421	23	9.72 872	30	0.27 128	9.94 526	7	50	.8 24.8 24.0 .9 27.9 27.0	
12	9.67 445	24	9.72 902 9.72 932	30	0.27 068	9.94 519 9.94 513	6	49 48	.91 27.91 27.0	
13	9.67 468	23 24	9.72 963	31	0.27 037	9.94 506	7 7	47		
14	9.67 492	23	9.72 993	30	0.27 007	9.94 499	7	46	.1 2.9	
15 16	9.67 515	24	9.73 023	31	0.26 977 0.26 946	9.94 492	7	45	.2 5.8 .3 8.7	
17	9.67 56z	23	9 73 054 9 73 084	30	0.26 916	9.94 485 9.94 479	6	44 43		
18	9.67 586	24	9.73 114	30	0.26 886	9.94 472	7	42	.4 11.6	
19	9.67 609	24	9.73 144	30	0.26 856	9.94 465	7 7	41	.5 14.5 .6 17.4	
20	9.67 633	23	9.73 175	30	0.26 825	9.94 458	7	40		
2I 22	9.67 656 9.67 680	24	9.73 205 9.73 235	30	0.26 795 0.26 765	9.94 451	6	39 38	.7 20.3 .8 23.2	
23	9.67 703	23	9.73 265	30	0.26 735	9.94 438	7	27	.9 26.1	
24	9.67 726	23 24	9.73 295	30	0.26 705	9.94 431	7	36		
25	9.67 730	23	9.73 326	30	0.26 674	9.94 424	7	35	1 24 1 23	
26 27	9.67 773	23	9.73 356 9.73 386	30	0.26 644	9.94 417	7	34	.I 2.4 2.3	
27 28	9.67 796 9.67 820	24	9.73 416	30	0.26 584	9.94 410 9.94 404	6	33 32	.2 4.8 4.6	
29	9.67 843	23 23	9.73 446	30	0.26 554	9.94 397	7	31	.3 7.2 6.9 .4 9.6 9.2	
80	9.67 866	24	9.73 476	31	0.26 524	9.94 390	7	80	.5 12.0 11.5	
31 32	9.67 890 9.67 913	23	9.73 507	30	0.26 493	9.94 383	7	29 28	.6  14.4  13.8	
33	9.67 936	23	9·73 537 9·73 567	30	0.26 433	9.94 376 9.94 369	7	27	.7 16.8 16.1 .8 19.2 18.4	
34	9.67 959	23 23	9.73 597	30	0.26 403	9.94 362	7 7	26	.9 21.6 20.	
35 36	9.67 982	24	9.73 627	30	0.26 373	9.94 355	6	25		
30	9.68 006 9.68 029	23	9.73 657 9.73 687	30	0.26 343	9.94 349	7	24		
37 38	9.68 052	23	9.73 717	30	0.26 283	9.94 342 9.94 335	7	23 22	.I 2.2	
39	9.68 075	23	9.73 747	30	0.26 253	9.94 328	7	21		
40	9.68 098	23	9.73 777	30	0.26 223	9.94 321	7	20	.3 6.6	
41 42	9.68 121 9.68 144	23	9.73 807 9.73 837	30	0.26 193	9.94 314	1 7	18	.4 8.8	
43	9.68 167	23	9.73 867	30	0.26 133	9.94 307 9.94 300	7	17	.5 11.0 .6 13.2	
44	9.68 190	23	9.73 897	30	0.26 103	9.94 293	7	16	.7 15.4 .8 17.6	
45	9.68 213	24	9.73 927	30	0.26 073	9.94 286	7	15		
46	9.68 237 9.68 260	23	9.73 957	30	0.26 043	9.94 279	6	14	.9  19.8	
47 48	9.68 283	23	9.73 987 9.74 017	30	0.25 983	9.94 273	7	13		
49	9.68 305	22	9.74 047	30	0.25 953	9.94 259	7	11	1716	
50	9.68 328	23	9.74 077	30	0.25 923	9.94 252	7	10	.1 0.7 0.	
51 52	9.68 351 9.68 374	23	9.74 107	30	0.25 893	9.94 245	7	8	.2 1.4 1. .3 2.1 1.	
53	9.68 307	23	9 74 137 9 74 166	29	0.25 834	9.94 238 9.94 231	7	8 7	1 1 2 8 2.	
_54_	9.68 420	23	9.74 196		0.25 804	9.94 224	7	6	1 . 4 2 . 4 3.	
55	9.68 443	23	9.74 226	1 -	0.25 774	9.94 217	7	5	.6 4.2 3. .7 4.9 4.	
57	9.68 466 9.68 489	23	9.74 256 9.74 286	1	0.25 744	9.94 210	7 7	5 4 3 2	.7 4.9 4. .8 5.6 4.	
58	9.68 512	23	9.74 316	30	0.25 684	9.94 203 9.94 196	7	1 3	.8 5.6 4. .9 6.3 5.	
52 53 54 55 56 57 58 59	9.68 534	22	9.74 345	29 - 30	0.25 655	9.94 189	7	1	1	
UU	9.68 557		9.74 375	30	0.25 625	9.94 182	7	0		
	L. Cos.	d.	1	1 -	L. Tang.	L. Sin.			Prop. Pts.	

	29°											
,	L. Sin.	d.	L. Tang.	c. d.	L. Cotg.	L. Cos.	d.		Prop. Pts.			
0	9.68 557	23	9 74 375	30	0.25 625	9.94 182	7	60				
I 2	9.68 580 9.68 603	123	9.74.405	30	0.25 595	9.94 175 9.94 168	7	59 58				
3	9.68 625	22 23	9 · 74 435 9 · 74 465	30 29	0.25 535	9.94 161	7	57	.I 3.0			
4	9.68 648	23	9.74 494	30	0.25 506	9.94 154	7	57 56	.1 3.0 .2 6.0			
5	9.68 671 9.68 694	23	9 · 74 524 9 · 74 554	30	0.25 476	9.94 I47 9.94 I40	7	55 54	.3 9.0			
7	9.68 716	22	9.74 583	30	0.25 417	9.94 133	7	53	.4 12.0 .5 15.0			
9	9.68 739 9.68 762	23	9.74 613 9.74 643	30	0.25 387	9.94 126	7	52	.6 18.0			
10	9.68 784	22	9.74 673	30	0.25 327	9.94 119	7	50	.7 21.0 .8 24.0			
11	9.68 807	23 22	9.74 702	30 30	0.25 298	9.94 103	7	49	.9 27.0			
I2 I3	9.68 829 9.68 852	23	9.74 732 9.74 762	30	0.25 268	9.94.098	7 8	48				
14	9.68 875	23 22	9.74 791	29	0.25 209	9.94 090 9.94 083	7	47 46	199			
15	9.68 897	23	9.74 821	30	0.25 179	9.94 076	7	45	.1 2.9			
16	9.68 920 9.68 942	22	9.74 851 9.74 880	30 29	0.25 149	9.94 069	7	44	.2 5.8 .3 8.7			
17 18	9.68 963	23	9.74 910	30	0.25 120	9.94 062 9.94 055	7	43 42	.4 11.6			
19	9.68 987	23	9.74 939	29 30	0.25 061	9.94 048	7	41	.5 14.5			
20	9.69 010	22	9.74 969	29	0.25 031	9.94 041	7	40	.6 17.4 .7 20.3			
2I 22	9.69 032 9.69 053	23	9.74 998 9.75 028	30	0.25 002	9.94 034 9.94 027	7	39 38	.8 23.2			
23	9.69 077	22	9.75 058	30 29	0.24 942	9.94 020	7	37 36	.9  26.1			
24	9.69 100	22	9.75 087	30	0.24 913	9.94 012	7					
25 26	9.69 122 9.69 144	22	9.75 117	29	0.24 883	9.94 005	7	35 34	23			
27	9.69 107	23 22	9.75 176	30 29	0.24 824	9.93 991	7. 7	33	.I 2.3 .2 4.6			
28 29	9.69 189 9.69 212	23	9.75 205 9.75 235	30	0.24 795	9.93 984 9.93 977	7	32 31	.3 6.9			
80	9.69 234	22	9.75 264	29	0.24 736	9.93.970	7	30	.4 9.2			
31	9.69 256	22	9.75 294	30 30	0.24 706	9.93 963	7	29	.5 11.5 .6 13.8			
32 33	9.69 279 9.69 301	22	9.75 323 9.75 353	30	0.24 677	9.93 955 9.93 948	7	28 27	.7 16.1			
33	9.69 323	22 22	9.75 382	29	0.24 618	9.93 941	7	26	.8 18.4 .9 20.7			
35	9.69 345	23	9.75 411	29 30	0.24 589	9.93 934	7	25	.,,,			
36	9.69 368 9.69 390	22	9.75 441 9.75 470	29	0.24 559	9.93 927	7	24	. 1			
37 38	9.69412	22	9 75 500	30	0.24 500	9.93 920 9.93 912	8	23 22	.1 2.2			
39	9.69 434	22	9.75 529	29	0.24 471	9.93 905	7	21				
40 41	9.69 456 9.69 479	23	9.75 558 9.75 588	30	0.24 442 0.24 412	9.93 898 9.93 891	7	20	.2 4.4			
42	9.69 501	22	9.75 617	29	0.24 383	9.93 884	7	19 18	.4 8.8 .5 II.0			
43	9.69 523	22	9.75 647	30 29	0.24 353	9.93 876	8	17	.6 13.2			
44 45	9.69 545	22	9.75 676	29	0.24 324	9.93 869	7	16	.7 15.4 .8 17.6			
46	9.69 589	22 22	9.75 733	30	0.24 265	9.93 853	7	15	.9 19.8			
47 48	9.69 611	22	9.75 764	29 29	0.24 236	9.93 847	8	13				
49	9.69 633	22	9.75 793 9.75 822	29	0.24 207	9.93 840 9.93 833	7	12 11	8 7			
50	9.69 677	22	0.75 852	.30	0.24 148	9.93 826	7	10	.1 0.8 0.7			
51	9.69 699	22	9.75 881	29 29	0.24 119	9.93 819	7 8	8	.2 1.6 1.4			
52 53	9.69 721 9.69 743	22	9.75 910 9.75 939	29	0.24 090 0.24 061	9.93 811 9.93 804	7	8	.3 2.4 2.1 .4 3.2 2.8			
54	9.69 765	22	9.75 969	30	0.24 031	9.93 797	7 8	7	1 5 40 25			
55 56	9.69 787	22	9.75 998	29 29	0.24 002	9.93 789	7	5	.6 4.8 4.2 .7 5.6 4.9 .8 6.4 5.6			
57	9.69 809 9.69 831	22	9.76 027 9.76 056	29	0.23 973	9.93 782	7	5 4 3 2	.7 5.6 4.9 .8 6.4 5.6 .9 7.2 6.3			
57 58	9.69 853	22	9.76 086	30	0.23 914	9.93 775 9.93 768	7		.9  7.2  6.3			
59 <b>60</b>	9.69 875	22	9.76 113	29 29	0.23 885	9.93 760	7		Į.			
<u> </u>						9.93 753		<u> </u>	Duon Die			
	L. Cos.	d.	L. Cotg.	c. d.		L. Sin.	d.		Prop. Pts.			
					60°							

	30°											
1	L. Sin.	d.	L. Tang.	c. d.	L. Cotg.	L. Cos.	d.		Prop. Pts.			
0	9.69 897	22	9.76 144	99	0.23 856	9 93 753	7	60	7			
I 2	9.69 919 9.69 941	22	9.76 173 9.76 202	99	0.23 827	9 93 746   9 93 738	8	59 58	\ m : m			
3	9 69 963	22 21	9.76 231	39 30	0 23 769	9 93 731	7	57 56	.I 3.0 2.9			
4	9.69 984	22	9.76 261	29	0 23 739	9 93 724	7		.2 6.0 5.8			
5	9.70 028	22	9.76 319	29	0.23 681	9 93 717	8	55 54	.3 9.0 8.7 .4 12.0 11.6			
7	9.70 030	22	9.76 348	29 29	0 23 652	9.93 702	7	53	.5 15.0 14.5			
9	9.70 072 9.70 093	21	9.76 377 9.76 406	29	0 23 623	9.93 69 <del>5</del> 9.93 687	8	52 51	.6 18.0 17.4 .7 21.0 20.3			
10	9.70 115	99 92	9.76 435	29	0.23 565	9.93 680	7	50	.7 21.0 20.3 .8 24.0 23.2			
11	9.70 137	22	9.76 464	29 29	0.23 536	9.93 673	7	49	.9 27.0 26.1			
12 13	9.70 159 9.70 180	21	9.76 493 9.76 522	29	0.23 507 0.23 478	9 93 665 9.93 658	7	48 47				
14	9.70 202	22	9.76 551	29 29	0.23 449	9 93 650	8 7	46	28			
15 16	9.70 224	31	9.76 580 9.76 609	29	0.23 420	9.93 643	7	45	.1 2.8 .2 5.6			
17	9.70 245 9.70 267	22	9.76 639	30	0.23 391	9 93 636 9 93 628	8	44 43	.3 8.4			
18	9.70 288	21 22	9.76 668	29 29	0.23 332	9.93 621	7	42	.4 II.2 .5 I4.0			
19 20	9.70 310	22	9.76 697	28	0 23 303	9.93 614	8	41	8.61 6.			
21	9.70 332 9.70 353	21	9.76 725 9.76 754	29	0.23 275   0.23 246	9.93 599	7		.7 19.6 .8 22.4			
22	9.70 375	22 21	9.76 783	29 29	0.23 217	9.93 591	8	39 38	.8 22.4 .9 25.2			
23 24	9.70 396 9.70 418	32	9.76 812 9.76 841	29	0.23 188 0.23 159	9 93 584 9 93 577	7	37 36	,,,			
25	9.70 439	21	9.76 870	29	0.23 130	9 93 569	8	35	1 22			
26	9.70 461	21	9.76 899	29 29	0.23 101	9.93 562	7	34	.I 2.2			
27 28	9.70 482 9 70 504	22	9.76 928 9.76 957	29	0.23 072	9 · 93 554 9 · 93 547	7	33 32	.2 4.4			
29	9.70 525	31	<b>9</b> . 76 986	29	0.23 014	9.93 539	8	31	.3 6.6 .4 8.8			
80	9.70 547	21	9.77 015	29	0.22 985	9.93 532	7	30	.5 11.0			
31 32	9.70 568 9.70 590	22	9.77 044 9.77 073	29	0.22 956	9.93 525 9.93 517	8	29 28	.6 13.2 .7 15.4			
33	9.70 611	21 22	9.77 101	28	0.22 899	9.93 510	7	27	.8 17.6			
34	9.70 633	21	9.77 130	29	0.22 870	9.93 502	7	26	.9  19.8			
35 36	9.70 675	21	9.77 159 9.77 188	29	0.22 812	9.93.495	8	25 24				
37 38	9.70 697	21	9.77 217	29	0.22 783	9.93 480	7	23	21			
30	9.70 718 9.70 739	21	9.77 246 9.77 274	28	0.22 754	9.93 472 9.93 465	7	22 21	.1 2.1			
40	9.70 761	22 21	9.77 303	29	0.22 697	9 93 457	8	20	.2 4.2 .3 6.3			
41	9.70 782 9.70 803	21	9.77 332	29	0.22 668	9.93 450	8	19 18	.4 8.4			
42 43	9.70 824	21	9.77 361 9.77 390	29	0.22 639	9.93 442	7	17	.5 10.5 .6 12.6			
44	9.70 846	22 21	9.77 418	28	0.22 582	9.93 427	8 7	16	.7 14.7			
45 46	9.70 867 9.70 888	2,1	9.77 447	29	0.22 553	9.93 420	8	15 14	.8 16.8 .9 18.9			
47	9.70 909	21 22	9.77 476 9.77 503	29	0.22 524	9 93 412	7	13	.91 .0.9			
47 48	9.70 931	21	9.77 533	28	0.22 467	9 93 397	8 7	12				
<u>49</u> 50	9.70 952	21	9.77 502 9.77 591	29	0.22 438	9.93 390	á	10	1 0.8 0.7			
	9.70 994	21	9.77 619	28	0.22 381	9 93 375	7		.2 1.6 1.4			
52	9.71 015	21 21	9.77 648	29	0.22 352	9 93 367	8 7	8	.3 2.4 2.1 .4 3.2 2.8			
53	9.71 036 9.71 058	22	9.77 677 9.77 706	29	0.22 323	9.93 360	8	7 6	.5 4.0 3.5			
55	9.71 079	21	9.77 734	28	0.22 266	9.93 344	8	5 4	1.0 4.8 4.2			
56	9.71 100 9.71 121	21	9.77 763 9.77 791	29	0.22 237	9 93 337	8	4	.7 5.6 4.9 .8 6.4 5.6 .9 7.2 6.3			
38	9.71 142	21	9.77 820	29	0.22 180	9.93 329 9.93 322	7	3 2	.9 7.2 6.3			
51 52 53 54 55 56 57 58 59	9.71 163	21	9.77 849	29	0.22 151	9.93 314	8 7	I	1			
60	9.71 184		9.77 877		0.22 123	9 93 307		0				
-	L. Cos.	d.	L. Cotg.	c. d.		L. Sin.	d.	<u> </u>	Prop. Pts.			
					59°							

	31°											
,	L. Sin.	d.		c. d.	L. Cotg.	L. Cos.	d.		Prop. Pts.			
0	9.71 184	21	9.77 877	29	0.22 123	9.93 307	8	60				
1 2	9.71 205 9.71 226	21	9.77 906 9.77 935	29	0.22 004	9.93 299 9.93 291	8	59 58				
3	9.71 247	21 21	9.77 963	28 29	0.22 037	9.93 284	7	57	.I 2.9			
4	9.71 268	31	9.77 992	28	0.22 008	9.93 276	7	56	.2 5.8			
5	9.71 289 9.71 310	21	9.78 049	29	0.21 980	9.93 269 9.93 <b>261</b>	8	55 54	.3 8.7 .4 11.6			
7 8	9.71 331	21 21	9.78 077	28 29	0.21 923	9.93 253	8	53				
8	9.71 352 9.71 373	21	9.78 106 9.78 13 <del>5</del>	29	0.21 864	9.93 <b>246</b> 9.93 <b>238</b>	8	52	.6 17.4			
10	9.71 393	30	9.78 163	28	0.21 837	9.93 230	8	51 50	.7 20.3 .8 23.2			
11	9.71.414	2I	9.78 192	29 28	0.21 808	9.93 223	7 8		.9 26.1			
I2 I3	9.71 435 9.71 456	21	9.78 220 9.78 249	29	0.21 780	9.93 215	8	49 48				
14	9.71 477	21	9.78 277	28	0.21 751	9.93 207 9.93 200	7	47 46	1 28			
15	9.71 498	2I 2I	9.78 306	29 28	0.21 694	9.93 192	8	45	.1 2.8			
16	9.71 519	20	9.78 334 9.78 363	29	0.21 666	9.93 184	7	44	.2 5.6 .3 8.4			
17 18	9.71 539 9.71 560	21	9.783 <b>9</b> 1	28	0.21 609	9.93 177 9.93 169	8	43 42	.4 11.2			
19	9.71 581	21 21	9.78 419	28 29	0.21 581	9.93 161	8	41	.5 14.0 .6 16.8			
20 21	9.71 602 9.71 622	20	9.78 448 9.78 476	28	0.21 552	9.93 154	8	40	.7 19.6			
22	9.71 643	21	9.78 503	29	0.21 524 0.21 495	9.93 146 9.93 138	8	39 38	.7 19.6 .8 22.4			
23	9.71 664	21	9.78 533	28 29	0.21 467	9.93 131	7 8	37	.9  25.2			
24	9.71 685	20	9.78 562	28	0.21 438	9.93 123	8.	36				
26	9.71 726	21	9.78 618	28	0.21 382	9.93 115 9.93 108	7	35 34	21			
27 28	9.71 747	30	9.78 647	29 28	0.21 353	9.93 100	8	33	.I 2.I .2 4.2			
20	9.71 767 9.71 788	21	9.78 675 9.78 704	29	0.21 325	9.93 092 9.93 084	8	32 31	.3 6.3			
80	9.71 809	21	9.78 732	28	0.21 268	9.93 077	7	30	.4 8.4			
31	9.71 829	20 21	9.78760	28 29	0.21 240	9.93 069	8	20	.5 10.5 .6 12.6			
32 33	9.71 850 9.71 870	20	9.78 789 9.73 817	28	0.21 211	9.93 061	8	28 27	.7 14.7 .8 16.8			
34	9.71 891	21	9.78 845	28	0.21 155	9.93 046	7 8	26	.9 18.9			
35	9.71 911	21	9.78 874	29	0.21 126	9.93 038	8	25				
36 37	9.71 932 9.71 952	20	9.78 902 9.78 930	28	0.21 098	9.93 030	8	24 23				
37 38	9.71 973	2I 2I	9 78 959	29 28	0.21 041	9.93 014	8	22	.I 2.0			
39	9.71 994	20	9.78 987	28	0.21 013	9.93 007	8	21	.2 4.0			
40 41	9.72 014 9.72 034	20	9.79 OI 5 9.79 O43	28	0.20 985	9.92 999 9.92 <b>9</b> 91	8	20 19	.3 6.0 .4 8.0			
42	9.72 055	21	9.79 072	29	0.20 928	9.92 983	8	18				
43	9.72 075	20 21	9.79 100	28 28	0.20 900	9.92 976	7 8	17	.6 12.0			
44	9.72 096	20	9.79 128	28	0.20.8/2	9.92 968	8	16	.7 14.0 .8 16.0			
45 46	9.72 137	2I 20	9.79 185	29	0.20 815	9.92 952	8	14	.9 18.0			
47 48	9.72 157	20	9.79 213	28 28	0.20 787	9.92 944	8 8	13				
49	9.72 177 9.72 198	21	9.79 <b>241</b> 9.79 <b>269</b>	28	0.20 759 0.20 731	9.92 936 9.92 929	7	12 11	1817			
50	9.72 218	20	9.79 297	28	0.20 703	9.92 921	8	10	.1 0.8 0.7			
51	9.72 238	20 21	9.79 326	29 28	0.20 674	9.92 913	8 8	9	2 1.6 1.4			
52 53	9.72 259	20	9.79 354 9.79 382	28	0.20 646	9.92 905 9.92 897	8	8	.3 2.4 2.1 .4 3.2 2.8			
54	9.72 299	20 21	9.79 410	28 28	0.20 590	9.92 889	8	7 6	ا دا مَاء دا			
55 56	9.72 320	90	9.79 438	28	0.20 562	9.92 881	7	5	.6 4.8 4.2 .7 5.6 4.9 .8 6.4 5.6			
57	9.72 340 9.72 360	20	9.79 466 9.79 493	29	0.20 534	9 92 874 9 92 866	8	4	.7 5.6 4.9 .8 6.4 5.6 .9 7.2 6.3			
57 58 59	9.72 381	21	9.79 523	28 28	0.20 477	9.92 858	8	3 2	.9 7.2 6.3			
<u>59</u>	9.72 401	20	9.79 551	28 28	0.20 449	9.92 850	8	1				
	9.72 421 T. Con	<del></del>	9·79 579		0.20 421	9.92 842	<u> </u>	_0				
<u> </u>	L. Cos.	d.	L. Cotg.	ic. (L.	L. Tang.	L. Sin.	d.	′	Prop. Pts.			
H					58°							

	32°											
,	L. Sin.	d.	L. Tang.	c. d.	L. Cotg.	L. Cos.	d.		Prop. Pts.			
0	9.72 421	90	9.79 579	28	0.20 421	9.92 842	8	60	/			
1 2	9.72 441 9.72 461	20	9.79 607 9.79 635	28	0.20 393 0.20 365	9.92 834 9.92 826	8	59 58	٧.			
3	9.72 482	21 20	9.79 663	28 28	0.20 337	9.92 818	8	57	.I 2.9 2.8			
4	9.72 502	20	9.79 691	-e	0.20 309	9.92 810	7	57 56	.2 5.8 5.6 .3 8.7 8.4			
5	9.72 522 9.72 542	20	9.79 719 9.79 747	28	0.20 281 0.20 253	9.92 803 9.92 795	8	55				
	9.72 562	20 20	9.79 776	29	0.20 224	9.92 787	8	54 53	.4 11.6 11.2 .5 14.5 14.0			
7 8	9.72 582	20	9.79 776 9.79 804	28 28	0.20 196	9.92 779	8	52	.6 17.4 16.8			
9 10	9.72 602	20	9.79 832 9.79 860	28	0.20 168	9.92 771	8	51	.7 20.3 19.6			
11	9.72 643	21	9.79 888	28	0.20 140	9.92 763 9.92 755	8	50 40	.8 23.2 22.4 .9 26.1 25.2			
12	9.72 663	20 20	9.79 916	28 28	0.20 084	9.92 747	8	49 48	19, 200, 250			
13	9.72 683 9.72 703	20	9.79 944	28	0.20 056	9.92 739	8	47	1 27			
14	9.72 723	20	9.79 972	28	0.20 000	9.92 731	8	46	.1 2.7 .			
15 16	9.72 743	20	9.80 028	28 28	0.19 972	9.92 723 9.92 715	8	45 44	.2 5.4			
17 18	9.72 763	20	9.80 056	28	0.19 944	9.92 707	8	43				
10	9.72 783 9.72 803	20	9.80 084 9.80 112	28	o. 19 916 o. 19 888	9.92 699 9.92 691	8	42 41				
20	9.72 823	20	9.80 140	28	0.19 860	9.92 683	8	40	.6 16.2			
21	9.72 843	20	9.80 168	28 27	0.19 832	9.92 675	8		.7 18.9 .8 21.6			
22	9.72 863 ·9.72 883	20	9.80 195 9.80 223	28	0.19 <b>803</b> 0.19 777	9.92 667	8	39 38	.9 24.3			
23 24	9.72 902	19	9.80 251	28	0.19 749	9.92 659 9.92 651	8	37 36				
25	9.72 922	20	9.80 279	28 28	0.19 721	9.92 643	8	35	1 21 20			
26	9.72 942	20	9.80 307	28	0.19 693	9.92 635	8	34	.1 2.1 2.0			
27 28	9. <b>72 962</b> 9.72 982	20	9.80 335 9.80 363	28	0.19 66 <del>3</del> 0.19 637	9.92 627 9.92 619	8	.33 32	.2 4.2 4.0			
29	9.73 002	20	9.80 391	28 28	0.19 609	9.92 611	8	31	.3 6.3 6.0 .4 8.4 8.0			
80	9.73 022	19	9.80 419	28	0.19 581	9.92 603	8	80	.5 10.5 10.0			
31 32	9.73 041 9.73 061	20	9.80 447 9.80 474	27	0.19 553 0.19 526	9.92 59 <del>5</del> 9.92 587	8	29 28				
33	9.73 081	90 90	9.80 502	28	0.19 498	9.92 579	8	27	.7 14.7 14.0 .8 16.8 16.0			
34	9.73 101	30	9.80 530	28 28	0.19470	9.92 571	8	26	.9 18.9 18.0			
35 36	9.73 121 9.73 140	19	9.80 558 9.80 586	28	0.19442	9.92 563	8	25				
37	9.73 160	20	9.80 614	28	0.19 414 0.19 386	9 92 55 <b>3</b> 9 92 <b>5</b> 46	9	24 23				
37 38	9.73 180	20	9.80 642	28 27	0.19 358	9.92 538	8	22	.I I.9 0.9			
39 <b>40</b>	9.73 200	19	9.80 669	28	0.19 331	9.92 530	8	21	.2 3.8 1.8			
41	9.73 239	20	9.80 697 9.80 725	28	O. 19 303 O. 19 275	9.92 522 9.92 514	8	20 19	.3 5.7 2.7 .4 7.6 3.6			
42	9.73 259	20 19	9.80 753	28 28	0.19 247	9.92 506	8	18	5 9.5 4.5			
43 44	9.73 278 9.73 298	20	9.80 781	27	0. I9 2I9 0. I9 192	9.92 498	8	17 16	6 11.4 5.4			
	9.73 318	30	9.80 836	28	0.19 164	9.92 490	8	15	.7 13.3 6.3 .8 15.2 7.2			
45 46	9.73 337	19 20	9.80 864	28 28	0.19 136	9.92 473	9	14	.8 15.2 7.2 .9 17.1 8.1			
47 48	9·73 357 9·73 377	20	9.80 892 9.80 919	27	0.19 108	9.92 465	8	13				
49	9 73 396	19	9.80 947	98	0.19 053	9.92 457 9.92 449	8	12 11	1817			
50	9.73 416	20 19	9.80 975	28 28	0.19 025	9.92 441	8	10	.1 0.8 0.7			
51 52	9.73 435	20	9.81 003	27	0.18 997	9.92 433 9.92 425	8	9 8	.2 1.6 1.4			
53	9 · 73 455 9 · 73 474	19	9.81 o30 9.81 o58	28	0. 18 970 0. 18 942 j	9.92 425 9.92 416	9	7	.3 2.4 2.1 .4 3.2 2.8			
53 54	9.73 494	20 19	9.81 086	28 27	0.18 914	9.92 408	8	7 6	.5 4.0 3.5			
55 56 57 <b>58</b> 59	9.73 513	20	9.81 113	2/ 28	0.18 887	9.92 400	8	5	6 4.8 4.2			
57	9 73 533 9 73 552	19	9.81 141 9.81 169	28	0.18 859 0.18 831	9.92 392 9.92 384	8	4	.7 5.6 4.9 .8 6.4 5.6 .9 7.2 6.3			
58	9.73 572	20 29	9.81 196	27 28	0.18 804	9.92 376	8	3 2	.9 7.2 6.3			
60	9 73 591	20	9.81 224	26 28	0.18 776	9.92 367	9	1	Ī			
<u> </u>	9 73 611	-7			0.18 748	9.92 359		0				
<b>I</b>	L. Cos.	d.	L. Cotg.	c. d.	L. Tang.	L. Sin.	d.	,	Prop. Pts.			
٦١					57°			_				

	33°											
•	L. Sin.	d.	L. Tang.	c. d.	L. Cotg.	L. Cos.	d.		Prop. Pts.			
0	9.73 611	19	9.81 252	27	0.18 748 0.18 721	9.92 359	8	60				
I 2	9.73 630 9.73 6 <b>3</b> 0	20	9.81 279 9.81 307	28 28	0.18 693	9 92 351 9 92 343	8	59 58	28   27			
3	9.73 669	20	9.81 335	27	0.18 665	9 92 335	9	57	.1 2.8 2.7			
4	9.73 689	19	9.81 362 9.81 390	28	0.18638	9.92 320	8	56	.2 5.6 5.4			
5	9.73 727	19 20	9.81 418	96 27	0.18 582	9.92 310	8	55 54	.3 8.4 8.1 .4 11.2 10.8			
7 8	9.73 747	19	9.81 445	28	0.18 555 0.18 527	9.92 302	9	53	.5 14.0 13.5			
9	9.73 766 9.73 785	19 20	9.81 473 9.81 500	27 28	0.13 527	9.92 293 9.92 285	8	52 51				
10	9.73 803	10	9.81 528	28 28	0.18 472	9.92 277	8	50	.8 22.4 21.6			
II I2	9.73 824 9.73 843	19	9 81 556 9 81 583	27	O. 18 444 O. 18 417	9.92 269 9.92 260	9	49 48	.9 25.2 24.3			
13	9.73 863	19	9.81 611	28	0.18 389	9.92 252	8 .	47				
14	9.73 882	19	9.81 638	27 26	0.18 362	9.92 244	9	46	.1 2.0			
15	9.73 901 9.73 921	20	9.81 666 9.81 693	27	0.18 334 0.18 307	9.92 235	8	45	.1 2.0 .2 4.0			
17	9.73 940	19	9.81 721	26	0.18 279	9.92 219	8	44 43	.3 6.0			
	9.73 959	19	9.81 748	27 28	0.18 252	9.92 211	9	42	.4 8.0 .5 10.0			
19 <b>20</b>	9.73 978 9.73 997	19	9 81 776	27	0.18 224	9 92 202	8	41 40	.6 12.0			
21	9.74 017	20 E9	9.81831	28 27	0.18 169	9.92 186	8	39 38	.7 14.0 .8 16.0			
22 23	9.74 030 9.74 055	19	9 81 858 9 81 886	26	0.18 142 0.18 114	9.92 177	8	38	.9 18.0			
24	9.74 074	19	9.81 913	27 26	0.18 087	9.92 161	8	37 36				
25 26	9.74 093	19	9.81 941	27	0.18 059	9.92 152	9	35	19			
26 27	9.74 II3 9.74 I32	19	9.81 968	28	0.18 032 0.18 004	9.92 144 9.92 136	8	34 33	.1 -1.9			
28	9.74 151	19	9.82 023	27 28	0.17 977	9.92 127	9	32	.2 3.8 .3 5.7			
29	9.74 170	19	9.82 051	27	0.17 949	9.92 119	8	31	.4 7.6			
<b>80</b> 31	9.74 189 9.74 208	19	9.82 078 9.82 to6	28	0.17 922	9.92 111	9	80 29	.5 9.5 .6 11.4			
32	9.74 227	19	9.82 133	27 28	0.17867	9.92 094	8 8	28	.7 13.3 .8 15.2			
33 34	9.74 246 9.74 265	19	9.82 161 9.82 188	27	0.17839	9.92 086	9	27 26				
	9.74 284	19	9.82 215	27	0.17 785	9.92 069	8	25	.9  17.1			
35 36	9.74 303	19	9.82 243	28	0.17 757	9.92 060	8	24				
37 38	9.74 322 9.74 341	19	9.82 270 9.82 298	28	0.17 730	9.92 052 9.92 044	8	23	.1 1.8·			
39	9.74 360	19	9.82 325	27 27	0.17673	9.92 035	8	21	.I 1.8 2 3.6			
40	9.74 379	19	9.82 352 9.82 380	28	0.17 648	9.92 027	9	20	-3 5.4			
41 42	9.74 398 9.74 417	19	9.82 407	27	0.17 620	9.92 018	8	19	.4 7.2 .5 9.0			
43	9.74 436	19	9.82 435	28	0.17 565	9.92 002	8	17	.6 10.8			
44	9·74 455 9·74 474	19	9.82 462	27 .	0.17 538	9.91 993	8	16	.7 12.6 .8 14.4			
45 46	9 74 493	19	9.82 517	28	0.17483	9.91 976	9	14	.9 16.2			
47 48	9.74 512	19	9.82 544 9.82 571	27	0.17 456	9.91 968	9	13	<b>1</b>			
49	9.74 531 9.74 549	18	9.82 599	28	0.17 401	9.91 951	8	11	1918			
50	9.74 568	19	9.82 626	27	0.17 374	9.91 942	9	10	.1 0.9 0.8			
51 52	9.74 587 9.74 606	19	9.82 653 9.82 681	28	0.17 347	9.91 934 9.91 925	9	9 8	.2 I.8 I.6 .3 2.7 2.4			
53 54	9.74 625	19	9.82 708	27	0.17 292	9.91 917	8	7 6	4 3.6 3.2			
54	9.74 644	18	9 82 735	27	0.17 265	9.91 908	8		.5 4.5 4.0 .6 5.4 4.8			
55 56 57 58 59 <b>60</b>	9.74 662 9.74 681	19	9.82 762 9.82 790	28	0.17 238	9.91 900 9.91 891	9	5 4 3 2	3 2.7 2.4 3.6 3.2 5 4.5 4.0 6 5.4 4.8 7 6.3 5.6 8 7.2 6.4			
57	9.74 700	19	9.82 817	27 27	0.17 183	9.91 883	8	3	.8 7.2 6.4 .9 8.1 7.2			
58	9.74 719 9.74 737	18	9.82 844 9.82 871	27	0.17 156	9.91 874 9.91 866	8	2 1	.91 5.41 7.2			
60	9.74 756	19	9.82 899	28	0.17 101	9.91 857	9	0				
	L. Cos.	d.	L. Cotg.	c. d.	L. Tang.		d.	一	Prop. Pts.			
					56°							
<b>I</b> '												

					34°				
,	L. Sin.	d.		c. d.	L. Cotg.	L. Cos.	d.		Prop. Pts.
0	9.74 756	19	9.82 899	27	0.17 101	9.91 857	8	60	
I 2	9·74 775 9·74 794	19	9.82 926 9.82 953	27	0.17 074	9.91 849	9	59 58	
3	9.74 812	18	9.82 980	27 28	0.17 020	9.91 832	8 9	57 56	.1 2.8 2.7
4	9.74 831 9.74 850	19	9.83 035	27	0.16 992 0.16 965	9.91 823	8	56	.2 5.6 5.4
5	9.74 868	18	9.83 062	27	0.16 938	9.91 806	9	55 54	.3 8.4 8.1 .4 11.2 10.8
7 8	9.74 887	19	9.83 089	27 28	0.16 911	9.91 798	8	53	.5 14.0 13.5
9	9.74 906 9.74 924	x8	9.83 117 9.83 144	27	0. 16 883 0. 16 856	9.91 789 9.91 781	8	52 51	.6 16.8 16.2 .7 19.6 18.9
10	9 74 943	19 18	9.83 171	27	0.16 829	9.91 772	9	50	.7 19.6 18.9 .8 22.4 21.6
11	9.74 961 9.74 980	19	9.83 198	27 27	0.16 802	9.91 763	9	49 48	.9 25.2 24.3
12 13	9.74 999	19	9.83 225 9.83 252	27	0.16 775 0.16 748	9.91 75 <del>5</del> 9.91 746	9	47	
14	9 75 017	18	9.83 280	28 27	0.16 720	9.91 738	8 9	46	36
15 16	9.75 036	18	9.83 307 9.83 334	27	0.16 693 0.16 666	9.91 729	9	45	.1 2.6 .2 5.2
17	9.75 054 9.75 073	19 18	9.83 361	27	0.16 639	9.91 720 9.91 712	8	44	.3 7.8
18	9.75 091	10	9.83 388	27 27	0.16612	9.91 703	<b>9</b> 8	42	.4 10.4 .5 13.0
19 <b>20</b>	9.75 110	18	9.83 415	27	o. 16 585 o. 16 558	9.91 695	9	41	.6 15.6
21	9.75 147	19 18	9.83 470	28	0.16 530	9.91 686 9.91 677	9		.7 18.2 .8 20.8
22	9.75 165	19	9.83 497	27 23	0.16 503	9.91 669	8	39 38	.9 23.4
23 24	9.75 184 9.75 202	18	9. <b>8</b> 3 524 9.83 551	27	0.16 476 0 16 449	9.91 660 9.91 651	9	37 36	٠, ٠,
25	9.75 221	19 18	9.83 578	27 27	0.16 422	9.91 643	8	35	1 29
26	9.75 239 9.75 258	19	9.83 605 9.83 632	27	0.16.395	9.91 634	9	34	1 1.0
27 28	9.75 276	18	9.83 659	27	0.16368 0.16341	9.91 625 9.91 617	8	33 32	.2 3.8
29	9.75 294	18	9.83 686	27 27	0.16 314	9.91 608	9	31	.3 5.7 .4 7.6
80 31	9.75 313 9.75 331	<b>18</b>	9.83 713	27	0 16 287	9.91 599	8	80	.5 9.5
32	9.75 330	29 28	9.83 740 9.83 768	28	0.16 260 0.16 232	9.91 591 9.91 582	9	29 28	.6 11.4 .7 13.3
33	9.75 368	18	9.83 795	27 27	0.16 205	9.91 573	9	27	.8 15.2
34 35	9.75 386	19	9.83 822	27	0.16 178	9.91 565	9	26 25	.9  17.1
36	9 75 423	18 18	9 83 876	27	0.16 124	9.91 556 9 91 547	9	24	
37 38	9.75 441 9.75 459	18	9.83 903	27 27	0.16 097	9.91 538	8	23	) 28
39	9.75 478	19 18	9.83 930 9.83 957	27	0.16 070 0.16 043	9.91 530 9.91 521	9	22 21	.1 1.8
40	9.75 496	18	9.83 984	27	0.16 016	9.91 512	9	20	.2 3.6 .3 5.4
41 42	9.75 514 9.75 533	39	9.84 011 9.84 038	27 27	0.15 989	9.91 504	8	19 18	.4 7.2
43	9 75 551	18 18	9.84 063	27	O. 15 962 O. 15 935	9.91 495 9.91 486	9	37	.5 9.0 .6 10.8
44	9.75 569	18	9.84 092	27 27	0.15 908	9.91 477	8	16	.7 12.6
45 46	9.75 587 9.75 605	18	9.84 119 9.84 146	27	0.15 881 0.15 854	9.91 469 9.91 460	9	15 14	.8 14.4 .9 16.2
47 48	9 75 624	19 18	9.84 173	27	0.15 827	9.91 451	9	13	.,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,
48 49	9.75 642 9.75 660	18	9.84 200 9.84 227	27 27	0.15 800	9.91 442	9	12	
50	9.75 678	18	9.84 254	27	0.15 773 0.15 746	9.91 433	8	10	.1 0.9 0.8
51	9.75 696	18 18	9.84 280	26 27	0.15 720	9.91 416	9	اما	.2 1.8 1.6
52 53	9.75 714 9.75 733	19	9.84 307 9.84 334	27	0.15 693 0.15 666	9.91 407 9.91 398	9	8 7 6	.3 2.7 2.4 .4 3.6 3.2
54	9.75 751	18 18	9.84 361	27	0.15 639	9.91 398	9		5 4.5 4.0
55	9.75 769 9.75 787	<b>38</b>	9.84 388	27 27	0.15 612	9.91 381	8	5	1.61 s.al a 8
57	9 75 805	18	9.84 415 9.84 442	27	0.15 585	9.91 372 9.91 363	9	4 3 2	.7 6.3 5.6 .8 7.2 6.4
55 56 57 58 59	9 75 823	18 18	9.84 469	27 27	0.15 531	9.91 354	9		9 8.1 7.2
60	9.75 841	18	9.84 496	.27	0.15 504	9.91 345	9	1	
	L. Cos.	₫.			0.15 477	9.91 336		9	
	UIN.		L. Cotg.	C. 4.		L. Sin.	d.	,	Prop. Pts.
					55°				

					350				
	L. Sin.	d.	L. Tang.	c.d.	L. Cotg.	L. Cos.	d. ·		Prop. Pts.
O	9.75 859 9.75 877	18	9.84 523 9.84 550	27	0.15 477	9.91 336	8	60	, , , , , ,
I 2	9.75 895	18 18	9.84 576	26	0.15 450 0.15 424	9.91 328 9.91 319	9	59 58	1 27 1 26
3	9.75 913	18	9.84 603	27	0.15 397	9.91 310	9	57 56	.1 2.7 2.6
4	9 · 75 931 9 · 75 949	18	9.84 630 9.84 657	27	0.15 370	9.91 301	9	56	2 54 5.2
5 6	9.75 967	18	9.84 684	27 27	0.15 316	9.91 292	9	55 54	.3 8.1 7.8 .4 10.8 10.4
7 8	9.75 985 9.76 ∞3	18	9.84 711 9.84 738	27	0.15 289	9.91 274	9 8	53	5 13.5 13.0
9	9.76 021	18 18	9.84 764	26	0.15 262	9.91 266 9.91 257	9	52 51	.6 16.2 15.6 .7 18.9 18.2
10	9.76 039	18	9.84 791	27	0.15 209	9.91 248	9	50	.8 21.6 20.8
11 12	9.76 057 9.76 075	18	9.84 818 9.84 84 <del>5</del>	27	0.15 182	9.91 239	9	49 48	.9 24.3 23.4
13	9.76 093	18 18	9.84 872	27	0.15 128	9.91 230 9.91 221	9	47	
14	9.76 111	18	9.84 899	27 26	0.15 101	9.91 212	9	46	.1 1.8
15 16	9.76 129 9.76 146	17	9.84 925 9.84 952	27	0.15 075	9.91 203 9.91 194	9	45	.1 1.8
17 18	9.76 164	18 18	9.84 979	27 27	0.15 021	9.91 185	9	44 43	.3 5 4
18 19	9.76 182 9.76 200	18	9.85 006 9.85 033	27	0.14 994 0.14 967	9.91 176	9	42	.4 7.2 .5 9.0
20	9.76 218	18	9.85 059	26	0.14 941	9.91 167	9	41 40	.6 10.8
21	9.76 236	18	9.85 086	27	0.14 914	9.91 149	9	39 38	.7 12.6 .8 14.4
22 23	9.76 253 9.76 271	18	9.85 113	27	0.14 887	9.91 141 9.91 132	9	38	.9 16 2
24	9.76 289	18	9.85 166	26 27	0.14 834	9 91 123	9	37 36	
25	9.76 307	17	9.85 193	27	0.14 807	9.91 114	9	35	1 17
26 27	9.76 324 9.76 342	18	9.85 220 9.85 247	27	0.14 780	9.91 10 <del>5</del> 9 91 096	9	34 33	.1 1.7
27 28	9.76 360	18 18	9.85 273	26 27	0.14 727	9.91 087	9	3 <b>2</b>	.2 3.4 .3 5.1
29	9.76 378	17	9 85 300	27	0.14 700	9.91 078	9	31	.4 6.8
<b>80</b> 31	9.76 395 9.76 413	18	9.85 327 9.85 354	27	0.14 673	9.91 069 9.91 060	9	80	.5 8.5
32	9.76 431	18	9.85 380	26 27	0.14 620	9.91 051	9	29 28	.6 10.2 .7 11.9
33 34	9.76 448 9.76 466	18	9.85 407 9.85 434	27	0.14 593	9.91 042 9.91 033	9	27 26	.8 13 6
	9.76 484	18	9 85 460	26	0.14 540	9.91 023	10	25	.9 15.3
35 36	9.76 50i	17	9.85.487	27	0.14 513	9.91 014	9	24	٠
37 38	9.76 519 9.76 537	18	9.85 514 9.85 540	26	0.14 486	9.91 005 9.90 996	.9 9	.23 .22	10.
39	9.76 554	17	9 85 567	27	0.14 433	9.90 987	9	21	.I I.O .2 2.0
40	9.76 572	18	9 85 594	27 26	0.14 406	9.90 978	9	20	.3 30
4 <sup>1</sup> 4 <sup>2</sup>	9.76 590 9.76 607	17	9 85 620	27	0.14 380	9.90 969 9.90 960	9	19 18	.4  4.0
43	9.76 625	18	9.85 674	27 26	0.14 326	9.90 951	9	17	.5 5 0 .6 6 0
44	9.76 642	18	9 85 700	27	0.14 300	9.90 942	9	16	.7 7.0 .8 8.0
45 46	9.76 677	17	9.85 727 9.85 754	27	0.14 273	9.90 933 9.90 924	9	15 14	.0 0.0
47 48	9 76 693	18	9.85 780	26	0.14 220	9.90 915	9	13	
40 49	9.76 712 9.76 730	18	9.85 807 9.85 834	27	0.14 193	9.90 906 9.90 896	io	12 11	1918
50	9.76 747	17	9.85 860	26	0.14 140	9.90 887	9	10	.1 0.9 0.8
51	9 76 763	18 17	9.85 887	27 26	0.14 113	9.90 878	9	9	.2 1.8 1.6
52 53	9.76 782 9.76 800	18	9.85 913 9.85 940	27	0.14 087	9.90 869 9.90 860	9	7	.3 2.7 2.4 .4 3.6 3.2
54	9.76 817	17	9.85 967	27 26	0.14 033	9.90851	9	7 6	.4 3.6 3.2 .5 4.5 4.0 .6 5.4 4.8 .7 6.3 5.6 .8 7.2 6.4
55	9.76 835 9.76 852	17	9.85 993 9.86 020	27	0.14.007	9.90 842	9	5	.5 4.5 4.0 .6 5.4 4.8 .7 6.3 5.6 .8 7.2 6.4
57	9.76 870	18	9.86 046	26	0.13 980 0.13 954	9.90 832 9.90 823	9	4 3 2	.8 7.2 6.4 .9 8.1 7.2
58	9.76 887	17	9 86 073	27 27	0.13 927	9.90 814	9		9 8.1 7.2
55 56 <b>57</b> <b>58</b> 59	9 76 904	18	9.86 100	26	0.13 900	9.90 803	9.	0	
	L. Cos.	d.		0.4	L. Tang.			_	Duon Die
	II. CUN.	u.	n. Corg.	ic. u.		L. Sin.	d.	,	Prop. Pts.
<u>L</u>			<u></u>		<b>54°</b>				

					···	36°				
I	•	L. Sin.	d.	L. Tang.	c. d.	L. Cotg.	L. Cos.	d.		Prop. Pts.
1	0	9.76 922 9.76 939	17	9.86 126 9.86 153	27	0.13 874	9.90 796 9.90 787	,	60	
ı	2	9.76 957	18	9.86 179	26 27	0.13821	9.90 777 9.90 768	10	59 58	27   26
I	3	9.76 974 9.76 991	17	9.86 200 9.86 232	26	0.13 794 0.13 768	9.90 768	9	57 56	1 2.7 26
I	4	9.77 009	18	9.86 259	27	0.13 741	9.90 759	9	55	.2 5.4 5.2 .3 8.1 7.8
I	5	9.77 026	17	9.86 285	26 27	0.13 715	9.90 741	9	54	.4 10 8 10.4
ı	8	9.77 043 9.77 061	18	9.86 312 9.86 338	26	0.13688	9.90 731 9.90 722	9	53 52	.5 13 5 13 0 .6 16.2 15 6
ı	9	9.77 078	17	9.86 365	27 27	0.13 635	9.90 713	9	51	.7 18.9 18.2
ı	10	9.77 095 9.77 112	17	9.86 392 9.86 418	26	0.13 608 0.13 582	9 90 704 9.90 694	10	50	.8 21.6 20 8 .9 24.3 23.4
l	12	9.77 130	18	9.86 443	≎7. 26	0.13 555	9 90 685	9	49 48	31 131 3 1
١	13 14	9.77 147 9.77 164	17	9.86 471 9.86 498	27	O. 13 529 O. 13 502	9.90 676 9.90 667	9	47 46	Į Ią
l	15 16	9.77 181	17	9.86 524	26 27	0.13 476	9.90 657	10	45	81 1.
I		9.77 199 9.77 216	17	9.86 551 9.86 577	26	0.13 449 0.13 423	9.90 648 9.90 639	9	44 43	.2 3.6 .3 5.4
۱	18	9.77 233	17	9.86 603	26 27	0.13 397	9.90 630	9	42	.4 7.2
ı	19 <b>20</b>	9.77 250	18	9.86 630	20	0.13 370	9.90 620	9	41 40	8.01 6.
ı	21	9.77 283	17	9.86 683	27 26	0.13 317	9.90 602	9	39 38	.7 12.6 .8 14.4
ı	22 23	9.77 302 9.77 319	17	9.86 709 9.86 736	27	0.13 291 0.13 264	9.90 592 9.90 583	10 9	38 37	.9 16.2
ı	24	9.77 336	17	9.86 762	26 27	0.13 238	9.90 574	9	36	
ı	25 26	9·77 353 9·77 370	17	9.86 789 9.86 815	26	0.13 211	9.90 56 <del>3</del> 9.90 555	9	35	1 27
ł	27 28	9.77 387	17	9.86 842	27 26	0.13 158	9.90 546	9	34 33	.I I.7 .2 3.4
ı	28 29	9.77 405 9.77 422	17	9.86 868 9.86 894	26	0.13 132	9.90 537 9.90 527	9 10	32 31	.3 5.1
ı	80	9.77 439	17	9.86 921	27 26	0.13 079	9.90 518	9	30	
ı	31	9 . 77 456 9 . 77 473	17	9.86 947 9.86 974	27	0.13 053 0.13 026	9.90 509	9	29 28	,6 10.2
I	32 33	9.77.490	17	9.87 000	26	0.13 000	9.90 499 9.90 490	9	27	.7 11.9 .8 13.6
ı	34	9.77 507	17	9.87 027	27 26	0.12 973	9.90 480	9	26	.9 15.3
I	35 36	9.77 524 9.77 541	17	9.87 <b>053</b> 9.87 <b>07</b> 9	26	0.12 947 0.12 921	9.90 471	9	25 24	
I	37 38	9.77 558	17	9.87 106 9.87 132	27 26	0.12 894 0.12 868	9.90 452	10	23	16
ı	39	9·77 575 9·77 592	17 17	9.87 158	26	0.12 842	9.90 443 9.90 434	. 9	22 21	.I I.6 .2 3.2
ı	40	9.77 609	17	9.87 183	27 26	0.12 815	9.90 424	10	20	.3 4.8
ı	4I 42	9.77 626 9.77 643	17	9.87 211 9.87 238	27	0.12 789	9.90 415	9 10	19 18	.4 . 6.4
ı	43	9.77 660	17	9.87 264	3Q	0.12 736	9.90 396	9	17	.6 9.6
ı	44	9.77 677	17	9.87 290	27	0.12 710	9.90 386	9	16	.7 11.2 .8 12.8
I	45 46	9.77 711	17	9.87 343	26 26	0.12 657	9.90 368	9 10	14	9 14.4
ı	47 48	9.77 728 9.77 744	16	9.87 369 9.87 396	27	0.12 631	9.90 358 9.90 349	9	13 12	
ı	49	9.77 761	17	9.87 422	26 26	0.12 578	9.90 339	9	11	10 9
	50 51	9.77 778 9.77 795	17	9.87 448 9.87 475	27	O. 12 552 O. 12 525	9.90 330 9.90 320	10	10	.I I.O O.9
ı	52	9.77 795 9.77 812	17	9.87 501	26 26	0.12 499	9.90 311	9	8 7 6	.3 3.0 2.7 .4 4.0 3.6
	53 54	9.77 829 9.77 846	17	9.87 527 9.87 554	27	0. <b>I2 473</b> 0. <b>I2 44</b> 6	9.90 301 9.90 292	9	6	.4 4.0 3.6 .5 5.0 4.5 .6 6.0 5.4
	55	9.77 862	16	9.87 580	26 26	0.12 420	9.90 282	10		
I	50 57	9.77 879 9.77 896	17	9.87 606 9.87 633	27	0.12 394 0.12 367	9.90 273 9.90 263	9 10	5 4 3 2	.7 7.0 6.3 .8 8.0 7.2
۱	58	9.77 913	17	9.87 659	26 26	0.12 341	9.90 254	9 10		.9  9.0  8.1
ı	55 56 57 58 59 <b>60</b>	9.77 930 9.77 946	16	9.87 685	26·	0.12 315 0.12 289	9.90 244	9		
		L. Cos.	d.	L. Cotg.	c. d.		L. Sin.	d.	<del>,</del>	Prop. Pts.
						53°			<u> </u>	- Alope Atas
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					37°					
,	L. Sin.	d.	L. Tang.	c. d.	L. Cotg.	L. Cos.	d.		Pr	op. Pts.
0	9.77 946	17	9.87 711	27	O. I2 289	9.90 235	10	60		
1 2	9.77 963 9.77 980	17	9.87 738 9.87 764	26	0.12 262 0.12 236	9.90 225 9.90 216	9	59 58		
3	9.77 997 9.78 013	17	9.87 790	26 27	0.12 210	9.90 206	9	57		1 2.7
4		17	9.87817	26	0.12 183	9.90 197	10	56		2 5.4
5	9.78 030 9.78 047	17	9.87 843 9.87 869	26	0.12 157 0.12 131	9.90 187 9.90 178	9	55 54		
7 8	9.78 063	16 17	9.87895	26 27	0.12 103	9.90 168	10	53		
	9.78 080 9.78 097	27	9.87 922	26	0.12 078 0.12 052	9.90 159	10	52		6 16.2
9 10	9.78 113	16	9.87 974	26	0.12 032	9.90 149 9.90 139	10	51 50	:	7 18.9 8 21.6
11	9.78 130	17 17	9.88 000	26 27	0.12 000	9.90 130	9	40		9 24.3
12	9.78 147 9.78 163	16	9.88 027 9.88 053	26	0.11 973 0.11 947	9.90 I20 9.90 III	9	48		
13 14	9.78 180	17	9.88 079	26	0.11 921	9.90 101	10	47 46		26
15	9.78 197	17 16	9.88 105	26 26	0.11 893	9.90 091	9	45		1 2.6
16	9.78 213 9.78 230	17	9.88 131 9.88 158	27	0.11 869 0.11 842	9.90 082 9.90 072	.10	44		2 5.2 3 7.8
17 18	9.78 246	16	9.88 184	26	0.11 816	9.90 063	9	43 42		4 10.4
19	9.78 263	37	9.88 210	26 26	0.11 790	9.90 053	10	41	•	5 13.0 6 15.6
20	9.78 280 9.78 296	16	9.88 236 9.88 262	26	0.11 764 0.11 738	9.90 043	9	40	:	7 18.2
2I 22	9.78 313	17	0.88 280	27	0.11 711	9 90 034 9 90 024	10	39 38		
23	9.78 329	16	9.88 313	26 26	0.11 685	9.90 014	10 9	37		9 23.4
24	9.78 346	16	9.88 341	26	0.11 659	9.90 005 9.89 995	10	36		
25 26	9.78 379	17	9.88 393	26	0.11 607	9.89 985	10	35 34		17
27 28	9.78 395	16	9.88 420	27 26	0.11 580	9.89 976	9	33		I I.7 2 3.4
28	9.78 412 9.78 428	16	9.88 446 9.88 472	26	0.11 554 0.11 528	9.89 966 9.89 956	10	32 31		3 5.I 4 6.8
80	9.78 443	17	9.88 498	26	0.11 502	9.89 947	9	80		
31	9.78 461	16	9.88 524	26 26	0.11 476	9.89 937	10	29	:	6 10.2
32 33	9.78 478 9.78 494	16	9.88 550 9.88 577	27	0.11 450 0.11 423	9.89 927 9.89 918	9	28 27		7 11.9 8 13.6
34	9.78 510	16 17	9.88 603	26 26	0.11 397	9.89 908	10	26		9 15.3
35 36	9.78 527	16	9.88 629	26	0.11 371	9.89 898	10	25		)
30	9.78 543 9.78 560	17	9.88 655 9.88 681	26	0.11 345 0.11 319	9.89 888 9.89 879	.9	24 23		
37 38	9.78 576	16 16	9.88 707	26 26	0.11 293	9.89869	10	22		I I.6
39	9.78 592	17	9.88 733	26	0.11 267	9.89 859	10	21		2 3.2
40 41	9.78 609 9.78 625	16	9.88 759 9.88 786	27	0.11 241 0.11 214	9.89 <u>8</u> 49 9.89840	9	20		3 4.8 4 6.4
42	9.78 642	17 16	9.88 812	26 26	0.11 188	9.89830	10	18		
43	9.78 658 9.78 674	16	9.88 838 9.88 864	26	0.11 162	9.89 820 9.89 810	10	17 16		5 8.0 6 9.6
44	9.78 691	17	9.88 890	26	0.11 130	9.89 801	9	15	:	7 11.2 8 12.8
45 46	9.78 707	16 16	9.88 916	26 26	0.11 084	9.89 791	10 10	13		9 14.4
47 48	9.78 723 9.78 739	16	9.88 942 9.88 968	26	0.11 058	9.89 781 9.89 771	10	13		
49	9.78 739 9.78 756	17	9.88 994	26	0.11 006	9.89 771 9.89 761	10	12 11	1	10   9
50	9.78 772	16 16	9.89 020	26	0.10 980	9.89 752	9	10	.1	1.0 0.9
51	9.78 788 9.78 803	17	9.89 046	26 27	0.10 954 0.10 927	9.89 742	10	8	.2	
52 53	9.78 821	16	9.89 073	26	0.10 927	9.89 732 9.89 722	10	8 7	·3	3.0 2.7 4.0 3.6
53 54	9.78 837	16 16	9.89 123	26 26	0.10875	9.89 712	10	7 6	. 5 . 6	5.0 4.5 6.0 5.4
55 56	9.78 853 9.78 869	16	9.89 ISI 9.89 I77	26	0.10 849 0.10 823	9.89 702	9	5	.0	5.0 4.5 6.0 5.4 7.0 6.3 8.0 7.2 9.0 8.1
57	9.78 886	17	9.89 203	26	0.10 823	9.89 693 9.89 683	10	5 4 3 2	.8	7.0 6.3 8.0 7.2
57 58 59	9.78 902	16 16	9.89 229	26 26	0.10 771	9.89 673	10		.91	9.0 8.1
59 <b>60</b>	9.78 918	16	9.89 255 9.89 281	26	0.10 745	9.89 663	10	0		
<u> </u>	9.78 934 T. Com	<del></del>			0.10719	9.89 653	<u> </u>	<b></b> -		
لنـــا	L. Cos.	d.	L. Cotg.	ic. d.		L. Sin.	đ.	/	Pr	op. Pts.
l					52°					

					38°				
•	L. Sin.	d.	L. Tang.	c. d.	L. Cotg.	L. Cos.	d.		Prop. Pts.
0	9.78 934	16	9.89 281	26	0.10 719	9.89 653	10	60	
I 2	9.78 950 9.78 967	17	9.89 307 9.89 333	26	0.10693 0.10667	9.89 643 9.89 633	10	59 58	1 06 1 00
3	9.78 983	16 16	9.89 359	96 96	0.10 641	9.89 624	10	57	.I 2.6 2.5
4	9.78 999	16	9.89 385	26	0.10613	9.89 614	10	56	.2 5.2 5.0
5	9.79 013 9.79 031	16	9.89 437	26	o. 10 589 o. 10 563	9.89 604 9.89 594	10	55 54	.3 7.8 7.5 .4 10.4 10.0
7 8	9.79 047	36 16	9.89 463	só só	0.10 537	9.89 584	10	53	
9	9.79 003	16	9 89 489 9 89 515	<b>2</b> 6	0.10 511	9.89 574 9.89 564	10	52 51	.5   13.0   12.5   .6   15.6   15.0   .7   18.2   17.5
10	9.79 095	16 16	9.89 541	só só	0.10 459	9.89 554	10	50	.7 18.2 17.5 .8 20.8 20.0
11	9.79 111	17	9.89 567	<b>s</b> 6	0.10 433	9.89 544	10	49	.9 23.4 22.5
12 13	9.79 128 9.79 144	16	9.89 593	<b>s</b> 6	0.10 407 0.10 381	9.89 534 9.89 524	10	48 47	
14	9.79 160	16 16	9.89 645	26 26	0.10 353	9.89 514	10	46	17
15 16	9.79 176	16	9.89 671	æ6	0.10 329	9.89 504	9	45	.I I.7 .2 3.4
	9.79 192 9.79 208	16	9.89 723	<b>26</b>	0.10 303 0.10 277	9.89 495	10	44 43	.3 5.I .4 6.8
17	9.79 224	16 16	9.89 749	26 26	0.10 251	9.89 475	10	42	
19 <b>20</b>	9.79 240	16	9.89 775	26	0.10 225	9.89 465	10	41	.6 10.2
2U 2I	9.79 256 9.79 272	16	9.89 827	26	0.10 199 0.10 173	9.89 45 <u>5</u> 9.89 44 <u>5</u>	10	40 30	.7 11.9 .8 13.6
22	9.79 288	16 16	9.89853	26 26	0.10 147	9.89 435	10	39 38	.9 15.3
23 24	9.79 304 9.79 319	15	9.89879 9.89903	26	0.10 121	9.89 42 <b>5</b> 9.89 415	10	37 36	3,1-3.5
	9.79 335	16	9.89 931	26	0.10 069	9.89 405	10	35	1 16   15
25 26	9.79 351	16 16	9.89 957	26 26	0.10 043	9.89 395	10	34	.1 1.6 1.5
27 28	9.79 367 9.79 383	16	9.89 983 9.90 009	26	0.10017	9.89 38 <del>5</del> 9.89 375	10	33 32	2 3.2 3.0
29	9.79 399	16 16	9.90 035	26 26	0.09 965	9.89 364	11	31	.3 4.8 4.5 .4 6.4 6.0
80	9.79 415	16	9.90 061	25	0.09 939	9.89 354	10	80	.5 8.0 7.5
31 32	9.79 431 9.79 447	16	9.90 086	26	0.09 914	9.89 344 9.89 334	10	29 28	.6 9.6 9.0 .7 11.2 10.5
33	9.79 463	16 15	9.90 138	26 26	0.09 862	9.89 324	10	27	.7 11.2 10.5 .8 12.8 12.0
34	9.79 478	16	9.90 164	26	0.09 836	9.89 314	10	26	.9 14.4 13.5
35 36	9.79 494 9.79 510	16	9.90 190 9.90 216	- 26	0.09 810	9.89 304 9.89 294	10	25 24	
37 38	9.79 526	16 16	9.90 242	26 26	0.09 758	9.89 284	10	23	13
38	9.79 542 9.79 558	16	9.90 268 9.90 294	26	0.09 732	0.89 274 9.89 264	10	22 21	.1 1.1
40	9.79 573	15	9.90 320	26	0.09 680	9.89 254	10	20	.2 2.2 .3 3.3
41	9.79 589	16 16	9.90 346	26 25	0.09 654	9.89 244	10	19	.4 4.4
42 43	9.79 605 9.79 621	16	9.90 371 9. <b>9</b> 0 397	26	0.09 629	9.89 233 9.89 223	10	18 17	.5 5.5 .6 6.6
44	9.79 636	15 16	9.90 423	26 26	0.09 577	9.89 213	10	16	
45	9.79 652	16	9.90 449	26	0.09 551	9.89 203	10	15	.7 7.7 .8 8.8 .9 9.9
46 47	9.79668 9.79684	16	9.90 475 9.90 501	26	0.09 525	9.89 193 9.89 183	10	14 13	יפיע ופי
47 48	9.79 699	15 16	9.90 527	26 26	0.09 473	9.89 173	10	12	
49 <b>50</b>	9.79 715	16	9.90 553	25	0.09 447	9.89 162	10	10	.I I.O 0.9
51	9.79 731 9.79 746	15	9.90 578 9.90 604	26	0.09 422 0.09 396	9.89 <b>152</b> 9.89 <b>142</b>	10	٥	.2 2.0 1.8
52	9.79 702	16 16	9.90 630	26 26	0.09 370	9.89 132	10	<u> </u>	.3 3.0 2.7
53 54	9.79 778 9.79 793	15	9.90 656 9.90 682	26	0.09 344	9.89 122 9.89 112	10	8 7 6	.3 3.0 2.7 .4 4.0 3.6 .5 5.0 4.5 .6 6.0 5.4
55	9.79 809	16	9.90 708	26	0.09 292	9.89 101	11		3 3.0 2.7 4 4.0 3.6 5 5.0 4.5 6 6.0 5.4 7.0 6 3 8 8.0 7.2 9 9.0 8.1
56	9.79 825	16 15	9.90 734	26 25	0.09 266	9.89091	10	5 4 3 2	.7 7.0 6 3 .8 8.0 7.2
58	9.79 840 9.79 856	16	9.90 759 9.90 785	26	0.09 241	9.89081 9.89071	10	3	.9 9.0 8.1
55 56 57 58 59 <b>60</b>	9.79 872	16 15	118 00.61	26 26	0.09 189	9.89 060	11	1	
60	9.79 887		9.90 837		0.09 163	9.89 050		9	
	L. Cos.	d.	L. Cotg.	e. d.		L. Sin.	d.	,	Prop. Pts.
					51°	,			ţ

					39°				
,	L. Sin.	d.	L. Tang.	c. d.		L. Cos.	d.		Prop. Pts.
0	9.79 887	16	9.90 837 9.90 863	26	0.09 163	9.89 050 9.89 040	10	60	
I 2	9.79 903 9.79 918	15	9.90 889	26	0.09 137	9.89 030	10	59 58	1 26
3	9 79 934	16	9.90 914	25 26	0.09 086	9.89 020	10	57	.1 2.6
4	9.79 950	15	9.90 940	26	0.09 034	9.89 009	10	56	.2 5.2
5	9.79 981	16 15	9.90 992	26 26	0.09 008	9.88 989	10	55 54	.3 7.8 .4 10.4
7 8	9.79 996 9.80 012	16	9.91 018 9.91 043	25	0.08 982	9.88 978 9.88 968	10	53 52	.5 13.0
9	9.80 027	15 16	9.91 069	26 26	0.08 931	9.88 958	10	51	.6 15.6 .7 18.2
10	9.80 043	15	9.91 095	26	0.08 903	9.88 948	11	50	.8 20.8
II I2	9.80 058 9.80 074	16	9.91 121 9.91 147	26	o.o8 879 o.o8 853	9.88 937 9.88 927	10	49 48	.9  23.4
13	9.80 oS9	15	9.91 172	25 26	0.08 828	9.88 917	10	47	
14	9.80 103	25	9.91 198	26	0.08 802	9.88 906 9.88 896	10	46	.I 2.5
15 16	9.80 120	16	9.91 224 9.91 250	26	0.08 750	9.88 886	10	45 44	.2 5.0
17 18	9.80 151	15 15	9.91 276	26 25	0.08 724	9.88 875	11	43	.3 7.5 .4 10.0
18	9.80 166 9.80 182	16	9.91 301 9.91 327	26	0.08 699	9.88 865 9.88 855	10	42 41	.4 10.0 .5 12.5 .6 15.0
20	9.80 197	15 16	9.91 353	26 26	0.08 647	9 88 844	11	40	.6  15.0
21	9.80 213 9.80 228	15	9.91 379	25	0.08 621	9 88 834 9 88 824	10	39 38	.7 17.5 .8 20.0
22 23	9.80 244	16	9.91 404 9.91 430	26	0.08 570	9.88 813	11	30 37	.9 22.5
24	9.80 259	15 15	9.91 456	26 ·	0.08 544	9.88 803	10	37 36	
25 26	9.80 274	26	9.91 482 9.91 507	25	0.08 518	9.88 793 9.88 782	71	35	z6
27 28	9.80 305	15 15	9.91 533	26 26	0.08467	9.88 772	10	34 33	.1 I.6 2 3.2
28 29	9.80 320 9.80 336	16	9.91 55 <u>9</u> 9.91 58 <u>5</u>	26	0.08 441	9.88 761 9.88 751	10	32	.3 4.8
80	9.80 351	15	9.91 610	25	0.08 390	9.88 741	10	$\frac{31}{80}$	4 6.4
31	9 80 366	15	9 91 636	26 26	0.08364	9.88 730	11	29	.5 8.0 6 9.6
32 33	9.80 382 9.80 397	15	9.91 662	26	0.08 338	9.88 720 9.88 709	11	28 27	.7 11.2
34	9.80 412	15 16	9.91 713	25 26	0.08 287	9.88 699	10	26	8 12.8 .9 14.4
35 36	9.80 428 9.80 443	15	9.91 73 <u>9</u> 9.91 765	26	0.08 261	9.88 688 9.88 678	10	25	,, , , ,
37	9.80 443	15	9 91 791	26	0.08 209	9.88 668	10	24 23	25
37. 38	9.80 473	15 16	9.91 816	25 26	0.08 184	9.88 657	10	22	.1 1.5
39 40	9.80 489	15	9.91 842 9.91 868	26	0.08 158	9.88 647	11	$\frac{21}{20}$	2 3.0
41	9 80 519	15 15	9.91 893	25 26	0.08 107	9.88 626	10	19	3 4·5 4 6.0
42	9.80 534 9.80 550	16	9.91 91 <u>9</u> 9.91 945	26	0.08 081	9.88 615 9.88 605	11	18	.5 7.5
43 44	9.80 563	15	9.91 971	26	0.08 029	9.88 594	11	17 16	.6 9.0 7 10.5
45 46	9.80 580	15	9.91 996	25 26	0.08 004	9.88 584	10	15	.8 12.0
81 A7 I	9.80 595 9.80 610	15	9.92 022	26	0.07 978	9.88 573 9.88 563	10	14	.9  13.5
48	9 80 625	15 16	9 92 073	25 26	0.07 927	9.88 552	11	12	i
49 <b>50</b>	9.80.641	15	9.92 099	26	0.07 901	9.88 542 9.88 531	11	11	.I I.I I.O
51	9.80 671	15	9.92 12 <del>5</del> 9.92 150	25	0.07 875	9.88 521	10	10	.2 2.2 2.0
52	9.80 686	15 15	9.92 176	26 26	0.07 824	9.88 510	11	8	.3 3.3 3.0
53 54	9.80 701 9.80 716	15	9.92 202 9.92 227	25	0.07 798	9.88 499 9.88 489	10	7 6	.3 3.3 3.0 .4 4.4 4.0 .5 5.5 5.0 .6 6.6 6.0
	9.80 731	15	9.92 253	26 26	0.07 747	9.88 478	11		.5 5.5 5.0 .6 6.6 6.0
56	9.80 746 9.80 762	15	9.92 279 9.92 304	20 25	0.07 721 0.07 696	9.88 468 9.88 457	10	5 4 3 2	7 7.7 7.0 .8 8.8 8.0
55 56 57 58 59	9.80 777	15	9.92 330	26	0.07 670	9.88 447	10		.9 9.9 9.0
59 <b>60</b>	9.80 792	15 15	9.92 356	26 25	0.07 644	9.88 436	11	· I	
00	9.80807	<del></del> -	9.92 381		0.07 619	9.88 425		0	
	L. Cos.	d.	L. Cotg.	c. a.	L. Tang.	L. Sin.	d.	. /	Prop. Pts.
l					50°				

	40°											
7	L. Sin.	d.		c. d.	L. Cotg.	L. Cos.	d.		Prop. Pts.			
0	9.80 807	15	9.92 381	<b>s</b> 6	0.07 619	9.88 425	10	60				
1 2	9.80 822 9.80 837	15	9.92 407	<b>96</b>	0.07 593	9.88 41 <del>5</del> 9.88 404	11	59 58				
3	9.80 852	15	9.92 433 9.92 458	25 26	0.07 542	9 .88 394	10	57	.1 2.6			
4	9.80 867	15	9.92 484	26	0.07 516	9.88 383	11	57 56	.2 5.2			
ş	9.80 882 9.80 897	15	9.92 510 9.92 535	25	0.07 490	9.88 372 9.88 362	10	55 54	.3 7.8			
7 8	9.80 912	15 15	9.92 561	s6 s6	0.07 439	9.88 351	11	53	.4 10.4 .5 13.0			
	9.80 927 9.80 942	15	9.92 587	25	0.07 413 0.07 388	9.88 340 9.88 330	10	52	.6 15.6			
9 10	9.80 957	15	9.92 612	26	0.07 362	9.88 319	11	51 50	.7 18.2 .8 20.8			
11	9.80 972	15	9.92 663	25 26	0.07 337	0.88 308	11		.9 23.4			
12	9.80 987 9.81 002	15	9.92 689	26	0.07 311	9.88 298 9.88 287	11	49 48				
13 14	9.81 017	15	9.92 740	25	0.07 260	9.88 276	11	47 46	95			
15 16	9.81 032	15	9.92 766	số số	0.07 234	9.88 266	10	45	.I 2.5			
16	9.81 047 9.81 061	14	9.92 792 9.92 817	25	0.07 208	9.88 253 9.88 244	11	44	.2 5.0 .3 7.5			
17 18	9.81 076	15	0.02 843	26	0.07 183 0.07 157	9.88 234	10	43 42	.4 10.0			
19	9.81 091	15	9.92 868	25 26	0.07 132	9.88 223	11	41	.5 12.5 .6 15.0			
20	9.81 106 9.81 121	25	9.92 894	<b>s</b> 6	0.07 106	9.88 212 9.88 201	11	40	.7 17.5			
22	9.81 136	15	9. <b>92 920</b> 9.92 945	25	0.07053	9.88 191	10	39 38				
23	9.81 151	15 15	9.92 971	96 25	0.07 029	9.88 180	11	37 36	.9 22.5			
24	9.81 166	14	9.02 996	26	0.07 004	9.88 169	21	36				
25 26	9.81 195	15	9.93 022 9.93 048	<b>26</b>	0.06 952	9.88 148	10	35 34	15			
27 28	9.81 210	15 15	9.93 073	25 26	0 06 927	9.88 137	11	33	.I I.5 .2 3.0			
28 29	9.81 22 <del>5</del> 9.81 240	15	9.93 099 9.93 124	25	0.06901	9.88 126 9.88 115	11	32 31	-3 4-5			
80	9.81 254	14	9.93 150	26	0.06 850	9.88 105	10	80	.4 6.0 .5 7.5			
31	9.81 269	15	9.93 175	25 26	0.06825	9.88 094	11	29 28	.6 9.0			
32 33	9.81 284 9.81 299	15	9.93 201 9.93 227	26	0.06 799	9.88 083 9.88 072	71	28 27	.7 10.5 .8 12.0			
34	9.81 314	15	9.93 252	25 26	0.06 748	9.88 061	11	<b>2</b> 6	.9 13.5			
35 36	9.81 328	15	9.93 278	25	0.06 722	9.88 051	11	25	31 00			
30	9.81 343 9.81 358	15	9.93 303 9.93 329	26	0.06 697	9.88 040 9.88 029	, II	24 23				
37 38	9.81 372	14	9 93 354	25 26	0.06 646	9.88 018	11	22	.1 1.4			
39	9.81 387	15	9.93 380	26	0.06 620	9.88 007	11	21	.2 2.8			
40 41	9.81 402 9.81 417	15	9.93 406 9.93 431	25	0.06 594	9.87 996 9.87 985	11	20	.3 4.2 .4 5.6			
42	9.81 431	14 15	9.93 457	26	0.06 543	9.87 975	10	18	.4 5.6 .5 7.0			
43	9.81 446 9.81 461	15	9.93 482	25 26	0.06 518	9.87 964 9.87 953	11	17 16	.5 7.0 .6 8.4 .7 9.8			
44 45	9.81 475	14	9.93 508	25	0.06 467	9.87 942	11	15	.7 9.8 .8 11.2			
46	9.81 490	15	9.93 559 9.93 584	26	0.06 441	9.87 931	11	14	.9 12.6			
47 48	9.81 50 <del>5</del> 9.81 519	14		25 26	0.06 416	9.87 920 9.87 909	11	13	l			
49	9.81 534	15	9.93 610 9.93 636	26	0.06 390 0.06 364	9.87 898	11	12 11	111   10			
50	9.81 549	15	9.93 661	25	0.06 330	9.87 887	11	10	.1 1.1 1.0			
51 52	9.81 563 9.81 578	15	9.93 687	26 25	0.06 313	9.87877 9.87866	10	9	.2 2.2 2.0			
53	9.81 592.	14	9.93 712 9.93 738	26	0.06 262	9.87.855	II	8 7 6	.3 3.3 3.0 .4 4.4 4.0			
53 54	9.81 607	15	9.93 763	25 26	0.06 237	9.87 844	11		3 3.3 3.0 4 4.4 4.0 5 5.5 5.0 .6 6.6 6.0 .7 7.7 7.0 .8 8.8 8.0			
55 56 57 58 59	9.81 622 9.81 636	14	9.93 789 9.93 814	25	0.06 211	9.87 833	11	5 4	7 7.7 7.0			
57	9.81 651	15	9.93 840	26	0.06 160	9.87 822 9.87 811	11	3	.8 8.8 8.0			
58	9.81 665 9.81 680	14	9.93 865	25 26	0.06 135	9.87800	11	3 2	.9  9.9  9.0			
<u>60</u>	9.81 694	14	9.93 891 9.93 916	25	0.06 109	9.87 789 9.87 778	11					
	L. Cos.	d.	L. Cotg.	c. d.		L. Sin.	d.	<del>,</del>	Prop. Pts.			
					49°							

					41°					
,	L. Sin.	d.	L. Tang.	c. d.	L. Cotg.	L. Cos.	d.		Prop	o. Pts.
0	9.81 694	15	9.93 916	26	0.06 084	9.87 778	32	60		
1 2	9.81 709 9.81 723	14	9.93 942 9.93 967	25	o.o6 o58 o.o6 o33	9.87 767 9.87 756	11	59 58	Ι.	
3	9.81 738	15 14	9.93 993	26 25	0.06 007	9.87 745	II II	57	т.	<b>25</b> 2.6
4	9.81 752	15	9.94 018	26	0.05 982	9.87 734	11	56	.1	5.2
5	9.81 767 9.81 781	14	9.94 044 9.94 069	25	0.05 956	9.87 723 9.87 712	11	55	.3	7.8
7 8	9.81 796	15 14	9.94 095	26 25	0.05 905	9.87 701	II	54 53	.4	10.4 13.0
	9.81 810 9.81 823	15	9.94 120	26	0.05 880	9.87 690	11	52	.5	15.6
9 10	9.81 839	14	9.94 146	25	0.05 854	9.87 679	11	51 50	.7 .8	18.2 20.8
11	9.81 854	15	9.94.197	26 25	0.05 803	9.87 657	II II		9.	23.4
12	9.81 868	14	9.94 222	26	0.05 778	9.87 646	11	49 48		•
13 14	9.81 882 9.81 897	15	9.94 <b>24</b> 8 9.94 <b>273</b>	25	0.05 752 0.05 727	9.87 63 <del>3</del> 9.87 624	11	47 46	1 1	25
	9.81 911	14 15	9.94 299	26	0.05 701	9.87 613	11	45	1.	2.5
15 16	9.81 926	14	9.94 324	25 26	0.05 676	9.87601	12	44	.2	5.0
17 18	9.81 940 9.81 95 <del>5</del>	15	9.94 350 9.94 375	25	0.05 650	9.87 590 9.87 579	11	43 42	·3	7.5 10. <b>0</b>
19	9.81 969	14	9.94 401	26 25	0.05 599	9.87 568	II II	41	.6	12.5
20	9.81 983	15	9.94 426	26	0.05 574	9.87 557	11	40	.0	15.0 17.5
2I 22	9.81 998 9.82 012	.14	9.94 452 9.94 477	25	0.05 548	9.87 546 9.87 535	11	39 38	.7 .8	20.0
23	9.82 026	14	9.94 503	26 25	0.05 497	9.87 524	II	37	.91	22.5
24	9.82 041	14	9.94 528	26	0.05 472	9.87 513	12	_36		
25 26	9.82 053 9.82 069	14	9·94 554 9·94 579	25	0.05 446	9.87 501 9.87 490	11	35	1	15
27 28	9.82 084	15 14	9.94 604	25 26	0.05 396	9.87 479	11	34 33	.2	1.5
	9.82 098	14	9.94 630	25	0.05 370	9.87 468	11	32	.3	3.0 4.5
29 80	9.82 112	14	9.94 655	26	0.05 345	9.87 457 9.87 446	II	31 <b>80</b>	.4	6.0
31	9.82 141	15	9.94 706	25	0.05 294	9.87 434	12	29	.5 .6	7·5 9·0
32	9.82 153	14	9.94 732	26 25	0.05 268	9.87 423	II	28	.7 .8	10.5
33 34	9.82 169 9.82 184	15	9·94 757 9·94 783	26	0.05 243	9.87 412 9.87 401	11	27 26	.8	12.0 13.5
35	9.82 198	14	9.94 808	25	0.05 192	9.87 390	II	25	.91	43.3
II 36 I	9.82 212	14	9.94 834	26 25	0.05 166	9.87 378	12	24		
37 38	9.82 226	14	9.94 859 9.94 884	25	0.05 141	9.87 367 9.87 356	11	23	_	14
39	9.82 255	15 14	9.94 910	26 25	0.05 090	9.87 345	11	21	. I . 2	1.4 2.8
40	9.82 269	14	9.94 935	25 26	0.05 065	9 87 334	12	20	.3	4.2
4I 42	9.82 283 9.82 297	14	9.94.961 9.94.986	25	0.05 039 0.05 014	9.87 322 9.87 311	11	19 18	.4	5.6
43	9.82 311	14 15	9.95 012	26 25	0.04 988	9.87 300	11	17	.5 .6	7.0 8.4
44	9.82 326	15	9.95 037	25 25	0.04 963	9.87 288	11	16	.7 .8	9.8
45 46	9.82 340 9.82 354	14	9.95 062 9.95 088	26	0.04 938	9.87 277 9.87 266	11	15 14	.8 .9	11.2 12.6
47 48	9.82 368	14	9.95 113	25 26	0.04 887	9.87 253	11	13	'	·
	9.82 382 9.82 396	14	9.95 139	25	0.04 861	9.87 243	11	12		<b>.</b>
<u>49</u> <b>50</b>	9.82 410	34	9.95 164	26	0.04 836	9.87 232 9.87 221	**	10	.1 1	2 11
51	9.82 424	14	9.95 215	25	0.04 785	9.87 209	II			.1
52	9.82 439	15 14	9.95 240	25 26	0.04 760	9.87 198	11	8	.3i 3	.6 3.3
53 54	9.82 453 9.82 467	14	9.95 266 9.95 291	25	0.04 734 0.04 709	9.87 187 9.87 175	12	7	.4 4 .5 6 .6 7	.8 4.4 .0 5.5
	9.82 481	14	9.95 317	26	0.04 683	9.87 164	11	- 5	.6  7	.2 6.6
55 56 57 58 59	9.82 495	14 14	9.95 342	25 26	0.04 658	9.87 153	12	4	.7 8 .8 9	.4 7.7 .6 8.8
38	9.82 509 9.82 523	14	9.95 368 9.95 393	25	0.04 632 0.04 607	9.87 141 9.87 130	11	3 2	.9 10	.8 9.9
59	9.82 537	14 14	9.95 418	25 26	0.04 582	9.87 119	17 12	1		
60	9.82 551		9.95 444		0.04 556	9.87 107		9		
	L. Cos.	d.	L. Cotg.	c. d.	L. Tang.	L. Sin.	d.	,	Prop	. Pts.
					48°					

			<del></del>		<b>42°</b>				
7.	L. Sin.	d.	L. Tang.	c. d.	L. Cotg.	L. Cos.	d.		Prop. Pts.
0	9.82 551	14	9.95 444	25	0.04 556	9.87 107	11	60	
I 2	9.82 565 9.82 579	14	9.95 469 9.95 493	26	0.04 531 0.04 505	9.87 096 9.87 08 <del>5</del>	11	59 58	1 26
3	9 82 593	14	9.95 520	25 25	0.04 480	9.87 073	11	57	.1 2.6
4	9.82 607 9.82 621	14	9.95 545 9.95 571	26	0.04 455	9.87 062	12	56	.2 5.2
5	9.82 635	14 14	9.95 596	25 26	0.04 404	9.87 039	11	55 54	.3 7.8 .4 10.4
7 8	9.82 649 9.82 663	14	9.95 622 9.95 647	25	0.04 378 0.04 353	9.87 028 9.87 016	12	53	.5 13.0
9	9.82 677	14 14	9.95 672	25 26	0.04 328	9.87 003	11	52 51	.6 15.6 .7 18.2 .8 20.8
10	9.82 691 9.82 703	24	9.95 698	25	0.04 302	9.86 993 9.86 982	11	50	.8 20.8 .9 23.4
II I2	9.82 719	14	9.95 723 9.95 748	25 26	0.04 277 0.04 252	9.86 970	12 11	49 48	.91 23.4
13	9.82 733	14 14	9.95 774	25	0.04.226	9.86 959	12	47	1 25
14	9.82 747 9.82 761	24	9.95 799	26	0.04 201	9.86 947	11	46 45	.1 2.5
15 16	9.82 77 <del>5</del> 9.82 788	14	9.95 850	25 25	0.04 150	9.86 924	12	44	.2 5.0
17 18	9.82 788	14	9.95 875 9.95 901	26	0.04.125	9.86 913 9.86 902	11	43 42	.3 7.5 .4 10.0
19	9.82 816	24 24	9 95 926	25 26	0.04 074	9.86 890	12	41	.5 12.5
20	9.82 830 9.82 844	14	9.95 952	25	0.04.048	9 86 879 9 86 867	12	40	.6 15.0 .7 17.5 .8 20.0
2I 22	0.82 858	14	9.95 977 9.96 002	25	0.04.023	9.86 855	12	39 38	
23	9.82 872 9.82 885	14	9.96 028 9.96 053	25	0.03 972	9.86 844 9.86 832	11	37	.9 22.5
24 25	9.82 899	14	9.96 078	25	0.03 947	9.86 821	11	36 35	
26	9.82 913	14 14	9.96 104	26 25	0.03 896	9.86 809	12	34	.1 1.4
27 28	9.82 927 9.82 941	14	9.96 129 9.96 155	26	0.03 871	9.86.798 9.86.786	12	33 32	.2 2.8
29	9.82 955	14 13	9.96 180	25 25	0 03 820	9.86 775	11	31	.3 4.2 .4 5.6
30	9.82 968	14	9.96 205	26	0.03 795	9.86 763 9.86 752	11	80	.5 7.0 .6 8.4
31 32	9.82982 9.82996	14	9.96 231 9.96 256	25	0.03 769	9.86 740	12	29 28	.6 8.4 .7 9.8
33	9.83 010	14	9.96 281	25 26	0.03 719	9.86 728 9.86 717	11	27 26	.8 11.2
34	9.83 023	24	9.96 307	25	0.03 668	9.86 705	12	25	.9   12.6
35 36	9.83 051	14 14	9.96 357	25 26	0.03 643	9.86 694	11	24	
37 38	9.83 005	13	9.96 383 9.96 408	25	0.03 617	9.86 682 9.86 670	12	23 22	13
39	9.83 092	14	9.96 433	25 26	0.03 567	9.86 659	11	21	.1 1.3 .2 2.6
40	9.83 106	14	9.96 459	25	0.03 541	9.86 647 9.86 635	12	20	.3 3.9
4I 42	9.83 120 9.83 133	13	9.96 484 9.96 510	26	0.03 516	9 86 624	11	19 18	.4 5.2 .5 6.5
43	9 83 147	14 14	9 96 535	25 25	0.03 465	9.86 612 9.86 600	12	17 16	.5 6.5 .6 7.8
44	9.83 161	13	9.96 560	26	0.03 440	9.86 589	212	15	.7 9.1 .8 10.4
45 46	9.83 188	34 14	9.96611	25 25	0.03 389	9.86 577	12	14	.9 11.7
47 48	9.83 202 9.83 215	13	9 96 636 9 96 662	26	0.03 364	9.86 565 9.86 554	11	13 12	
49	9.83 229	14	9.96 687	25 25	0.03 313	9.86 542	12	11	129   12
50 51	9.83 242 9.83 256	14	9.96 712	26	0.03 288	9.86 530 9.86.518	12	10	.I I.2 I.I .2 2.4 2.2
52	9.83 270 9.83 283	14	9.96 738 9.96 763	25	0.03 237	9.86 507	11	8	3 3.6 3.3
52 53 54	9.83 283	13	9.96 788 9.96 814	25 26	0.03 212	9 86 495 9 86 483	12	7 6	.3 3.6 3.3 .4 4.8 4.4 .5 6.0 5.5
55	9.83 297	13	9.96 839	25	0.03 186	9.86 472	**		3 3.6 3.3 4.8 4.4 5 6.0 5.5 6 7.2 6.6 7.2 6.6 7.2 8.4 7.8 9.6 8.8 9.6 8.9
55 56 57 58 59	9 83 324 9 83 338	14 14	9.96 864	25 26	0.03 136	9.86 460	12	5 4 3 2	.6 7.2 6.6 .7 8.4 7.7 .8 9.6 8.8
57 58	9.83 338 9.83 351	13	9.96 890 9.96 91 <del>5</del>	25	0.03 110	9.86 448 9.86 436	12	3 2	.9 10.8 9.9
59	9.83 365	14	9.96 940	25 26	0.03 060	9 86 425	11	1	
60	9.83 378		9.96 966		0.03 034	9.86 413		0	
	L. Cos.	d.	L. Cotg.	c. d.	L. Tang.	L. Sin.	d.	'	Prop. Pts.
					47°				

					43°				
,	L. Sin.	đ.	L. Tang.	c. d.	L. Cotg.	L. Cos.	d.		Prop. Pts.
0	9 83 378	14	9.96 966	25	0.03 034	9.86 413	12	60	
[ 2	9.83 392 9.83 405	13	9.96991 9.97016	25	0.03 009	9.86 401 9.86 389	12	59 58	
3	9.83 419	13	9.97 042	26 25	0.02 958	9.86 377	12	57	.1 2.6
4	9.83432	14	9.97 067	25	0.02 933	9.86 366	12	56	.2 5.2
5	9.83 446 9.83 459	13	9.97.092 9.97.118	26	0.02 908	9.86 354 9.86 342	12	55	.3 7.8
7 8	9.83 473	14	9.97 143	25	0.02 857	9.86 330	12	54 53	.4 10.4 .5 13.0
	9.83 486	13	9 97 168	25 25	0.02 832	9.86 318	12	52	.6 15.6
9 10	9.83 <del>5</del> ∞	13	9.97 193	26	0.02 807	9.86 306	11	51	.7 18.2
11	9.83 513 9.83 527	14	9.97 219 9.97 244	25	0.02 756	9.86 29 <b>5</b> 9.86 283	12	<b>50</b> 49	.8 20.8 .9 23.4
12	9.83 540	E3	9.97 269	25 26	0.02 731	9.86 271	12	48	1713.4
13 14	9.83 554 .9.83 567	13	9.97 295	25	0.02 705	9.86 259 9.86 247	12	47	1 25
15	9.83.581	14	9.97 345	25	0.02 655	9.86 235	12	46	.1 2.5
16	9.83 594	13	9.97 371	26 25	0.02 629	9.86 223	12	45 44	.2 5.0
17 18	9.83 608	E3	9.97 396	25	0.02 604	9.86 211	12	43	.3 7.5 .4 10.0
10	9.83 621 9.83 634	13	9.97 421 9.97 447	26	0.02 579	9. <b>86 200</b> 9.86 188	12	42 41	
20	9.83 648	14	9.97 472	25	0.02 528	9.86 176	12	40	.5 I2.5 .6 I5.0
21	9.83 661	13	9 97 497	25 26	0.02 503	9.86 164	12	30	.7 17.5 .8 20.0
22 23	9.83 674 9.83 688	14	9.97 523 9.97 548	25	0.02 477	9.86 152 9.86 140	12	38	.9 22.5
24	9.83 701	13	9 97 573	25	0.02 427	9.86 128	12	37 36	
25 26	9.83 715	14	9.97 598	25 26	0.02 402	9.86 116	12	35	1 24
	9.83 728 9.83 74E	13	9.97 624	25	0.02 376	9.86 104	12	34	.1 1.4
27 28	9.83 755	14	9.97 649 9.97 674	25	0.02 351	9.86 o92 9.86 o80	12	33 32	.2 2.8
29	9:83 768	13	9.97 700	26 25	0.02 300	9.86 o68	12	31	.3 4.2 .4 5.6
80	9.83 781	14	9.97 725	25	0.02 275	9.86 056	12	30	.5 7.0 .6 8.4
31 32	9.83 79 <b>3</b> 9.83 808	13	9.97 750 9.97 776	26	0.02 250	9.86 044 9.86 032	12	29 28	.5 7.0 .6 8.4 .7 9.8
33	9.83 821	13	9.97 801	25 25	0.02 199	9.86 020	12	27	.7 9.8 .8 11.2
34	9.83 834	14	9.97 826	25	0.02 174	9.86 008	12	26	.9 12.6
35 36	9.83 848 9.83 861	13	9.97 851 9.97 877	26	0.02 149	9.85 996 9.85 984	12	25	
37	9.83874	E3	9.97 902	25	0.02 098	9.85 972	12	24 23	1 r3
37 38	9.83887	13	9.97 927	25 26	0.02 073	9.85 960	12	22	
<u>39</u> <b>40</b>	9.83 901 9.83 914	13	9.97 953	25	0.02 047	9.85 948	12	21	.1 I.3 .2 2.6
41	9.83 927	13	9.97 978	25	0.02 022 0.01 997	9.85 936 9.85 924	I2	<b>20</b>	.3 3.9 .4 5.2
42	9.83 940	13 14	9.98 029	26 25	0.01 971	9.85 912	12	18	.5 6.5 .6 7.8
43 44	9.83 954 9.83 967	13	9.98054	25	0.01 946	9.85 900 9.85 888	12	17 16	.6 7.8
	9.83 980	13	9.98 104	25	0.01 896	9.85 876	12	15	.7 9.1 .8 10.4
45 46	9.83 993	13	9.98 130	26 25	0.01 870	9.85 864	12	14	.9 11.7
47 48	9.84 006	14	9.98 155	25 25	0.01 845	9.85 851 9.85 839	13	13 12	
49	9.84 033	13	9.98 206	26	0.01 794	9.85 827	12	11	1 x2   xx
50	9.84 046	13	9.98 231	25	0.01 769	9.85 815	12	10	.I I.2 I.I
51	9.84 059	13	9.98 256	25 25	0.01 744	9.85 803	12	9	.2 2.4 2.2
52 53	9.84 0/2	13	9.98 307	26	0.01 719	9.85 791 9.85 779	. 12	8	.3 3.6 3.3 .4 4.8 4.4 .5 6.0 5.5
54	9.84 098	13 14	9.98 332	25 25	0.01 668	9.85 760	13	7	.5 6.0 5.5
55	9.84 112	13	9.98 357	26	0.01 643	9.85 754	12	5	3 3.6 3.3 4 4.8 4.4 5 6.0 5.5 6 7.2 6.6 7 8.4 7.7 8 9.6 8.8
50	9.84 12 <del>5</del> 9.84 138	13	9.98 383 9.98 408	25	0.01 617 0.01 592	9.85 742 9.85 730	12	3	
55 56 57 58 59	9.84 151	13	9.98 433	25 05	0.01 567	9.85 718	12	2	.9 10.8 9.9
59	9.84 164	13	9.98 458	25 26	0.01 542	9.85 706	12	1	ĺ
60	9.84 177		9.98 484	_	0.01 516	9.85 693		0	
	L. Cos.	d.	L. Cotg.	c. d.	L. Tang.	L. Sin.	d.	,	Prop. Pts.
					46°				

					44°				
•	L. Sin.	d.	L. Tang.	c. d.	L. Cotg.	L. Cos.	d.		Prop. Pts.
U	9.84 177	13	9.98 484	25	0.01 516	9.85 693	12	60	
1 2	9.84 190	13	9.98 509 9.98 534	25	0.01491	9.85681	12	59 58	
3	9.84 216	13	9 98 560	26 25	0.01 440	9.85 657	12	57	.1 2.6
4	9.84 229	13	9.98 585	25	0.01 415	9.85 645	13	56	.2 5.2
<b>5</b>	9.84 242 9.84 255	13	9 98 610	25	0.01 390 0.01 365	9.85 632 9.85 620	12	55	.3 7.8
	9.84.269	14	9.98 661	26	0.01 339	9.85 608	12	54 53	.4 10.4 .5 13.0
3	9.84 282	13	9.98 686	25 25	0.01 314	9.85 596	12	52	.6 15.6
9	9.84 295	13	9.98 711	20	0.01 289	9.85 583	12	51	.7 18.2 .8 20.8
10	9.84308 9.84321	13	9.98 737 9.98 762	25	0.01 263 0.01 238	9.85 571 9.85 559	32	50	.8 20.8 .9 23.4
12	9.84 334	13	9.98 787	25 25	O.CI 213	9.85 547	13	49 48	-21-3-4
13	9.84.347	13	9.98812	26	0.01 188 0.01 102	9.85 534	12	47	t 25
15	9.84 360	23	9.98 838	25	0.01 137	9.85 522	12	46	.1 2.5
16	9.84 385	12	9.98 888	25	0.01 112	9.85 497	33.	45 44	.2 5.0
17	9.84 398	13 13	9.98913	25 26	0.01 087	9.85.485	12	43	·3 7·5
19	9.84 411 9.84 424	13	9.98 939 9.98 964	25	0.01 001	9.85 473 9.85 460	33	42 41	
20	9.84 437	23	9.98 989	25	0.01 011	9.85 448	32	40	.6 15.0
21	9.84 450	13 23	9.99013	25	0.00 985	9.85 436	33		.7 17.5 .8 20.0
22	9.84.463 9.84.476	13	9.99 040	25	0.00 960	9.85 423	32	39 38	.9 22.5
23 24	9.84 489	*3	9.99 065 9.99 090	25	0.00 935	9.85 399	12	37 36	
25	9.84 502	23	9 99 116	26	0.00 884	9.85 386	13	35	1 24
26	9.84 515	13 13	9.99 141	25 25	0.00 859	9.85 374	12 13.	34	.3 3.4
27 28	9.84.528 9.84.540	12	9.99 166 9.99 191	25	0.00 834	9.85 361 9.85 349	12	33	.2 2.8
29	9.84 553	23	9.99 217	26	0.00 783	9.85 337	12	32 31	.3 4.2 .4 5.6
80	9 84 566	23	9.99 242	25	0.00 758	9.85 324	33	80	.51 7.0
31	9.84 579	13 13	9.99 267	25 26	0.00 733	9.85 312	13	29 28	.6 8.4
32 33	9.84592 9.84605	13	9.99 293	25	0.09 707	9.85 299	12	27	.7 9.8 .8 11.2
34	9.84 618	13 12	9.99 343	25 25	0.00 657	9.85 274	13. 12	26	.9 12.6
35	9.84 630	33	9.99 368	26	0.00 632	9.85 262	12	25	
36 37	9.84 643 9.84 656	13	9.99 394 9.99 419	25	0.00 500 0.00 581	9.85 250 9.85 237	13	24 23	
38	9.84.669	13	9.99 444	25	0.00 556	9.85 223	13	22	.1 1.3
39	9.84.082	13	9.99 469	25. 26	0.00 531	9.85 212	13.	21	.1 1.3 .2 2.6
40	9.84.694 9.84.707	13	9.99 495	25	0.00 505	9.85.200	33	20 19	-3 3-9
41 42	9.84,720	13	9.99 520	25	0.00 455	9.85 175	12	18	.4 5.2 .5 6.5 .6 7.8
43	9.84 733	13	9.99 570	25 26	0.00 430	9 85 162	13.	17	.5 6.5 .6 7.8
44	9.84 745	13	9.99 596	25	0.00 404	9.85 150	13	16	.7 9.1 .8 10.4
45 46	9.84 758 9.84 771	13	9.99 621 9.99 646	25	0.00 379	9.85 137 9.85 125	12	15 14	.9 11.7
17	9.84 784	13 12	9.99 672	26	0.00 328	9.85 112	13	13	-
48	9.84.796	23	9.99 697	25 25	0.00 303	9.85 100	33	12	1 12
49 <b>50</b>	9.84 809	13	9.99 722 9.99 747	25	0.00 253	9.85 087	13	10	.1 1.2
51.	9.84 835	23	9.99 773	26	0.00 227	9.85 062	12	9	.2 2.4
52	9.84 847	13	9.99 798	25 25	0.00 202	9.85 049	13 12	8	3 3.6
53 54	9.84 860 9.84 873	13	9.99 823 9.99 848	25	0.00 177	9.85 037	13	76	.4 4.8
	9.84 885	12	9.99 874	26	0.00 126	9.85 012	13	5	.6 7.2
55 56	9 84 898	13	9.99 899	25	0.00 101	9.84 999	13	4	.7 8.4 .8 9.6
57 58	9.84 911 9.84 <b>92</b> 3	13	9.99 924	25 ·	0.00076	9.84.986	13	3 2	.9 10.8
59	9.84 923	13	9.99 94 <u>9</u> 9.99 975	26	0.00 051	9.84 961	23	1	
60	9.84 949	13	0.00 000	25	0.00.000	9.84 949	32	0	
	L. Cos.	d.	L. Cotg.	c. d.	L. Tang.	L. Sin.	d.	,	Prop. Pts.
					45°				
1					-A (7				

TABLE V.

NATURAL

SINES AND COSINES.

70											
	•	°	1		9	P°	3	3°	4		
·	N. sine	N. cos.	N. sine		N. sine	N. cos.	N. sine	N. cos.	N. sine	N. cos.	
0	.00000	1.00000	.01745	.99985	.03490	.99939	.05234	.99863	.06976	.99756	60
I	.00029	1.00000	.01774	.99984	.03519	.99938	.05263	99861	.07005	·99754	59 58
2	.00058	I.00000	.01803 .01832	.99984 .99983	.03548	.99937 .99936	.05292 .05321	.99860 .99858	.07034 .07063	.99752	58
3 4	.00116	1.00000	.01862	.99983	.03577 .03606	.99935	.05350	.99857	.07092	.99750 .99748	57 56
5	.00145	1.00000	.01891	99982	.03635	.99934	.05379	.99855	.07121	.99746	55
١ ا	.00175	1.00000	.01920	.99982	.03664	·99933	.05408	.99854	.07150	·99744	54
7 8	.00204	1.00000	.01949	99981	.03693	.99932	.05437	.99852	.07179	.99742	53
	.00233	1.00000	.01978 .02007	.99980 .99980	.03723	.99931	05466 .05495	.99851 .99849	.07208	.99740	52 51
9 10	.00202	1.00000	.02036	.99979	03752	.99930 . <b>99929</b>	.05524	.99847	.07237 .07266	.99738 .99736	50
11	.00320	.99999	.02065	99979	.03810	99927	.05553	.99846	.07295	.99734	40
12	.00349	.99999	.02094	.99978	.03839	.99926	05582	.99844	.07324	.99731	48
13	.00378	-99999	.02123	· <b>9</b> 9977	.03868	.99925	.05611	.99842	.07353	99729	47
14	.00407	-99999	.02152	·99977	.03897	.99924	.05640 .05669	.99841 .99839	.07382	99727	46
15 16	.00436	.99999 .99999	.02101	.99976 .99976	.03926 .03955	.99923 .99922	.05698	.99839 .99838	.07411 .07440	.99725 . <b>9</b> 9723	45 44
17	.00495	.99999	.02240	.99975	.03984	.99921	.05727	.99836	.07469	.99721	43
18	.00524	.99999	.02269	.99974	.04013	.99919	.05756	. <b>9</b> 9834	.07498	.99719	42
19	.00553	.99998	.02298	.99974	.04042	. <b>9</b> 9918	.05785	.99833	.07527	.99716	41
20	.00582	.99998	.02327	-99973	.04071	.99917	.05814	.99831	.07556	.99714	40
2I 22	.00611	.99998 .99998	.02356 .02385	.99972 .9 <b>997</b> 2	.04100	.99916 .9 <b>99</b> 15	.05844 • .05873	.99829 .99827	.07585 .99712 .07614 .99710		39 38
23	.00669	.99998	.02414	+99971	04199	.99913	105902	.99826	.07643 .99708		37
24	.00698	.99998	.02443	.99970	.04188	.99912	.05931	.99824	.07672	.99705	36
25	.00727	-99997	.02472	.99969	.04217	.99911	.05960	.99822	.07701	.99703	35
26	.00756	-99997	.02501	.99969	.04246	.99910	.05989	.99821	.07730	.99701	34
27 28	.00785	.99997 .99997	.02530 .02560	.99968 .99967	.04275	. <del>99909</del> .99907	.06018 .00047	.99819 .99817	.07759 .07788	.99699 .99696	33
29	.00844	.99996	.02589	.99966	.04333	.99907	06076		.07817	.99694	32 31
30	.00873	.99996	.02618	.99966	.04362	.99905	06105	.99813	.07846	.99692	30
31	00902	.99996	.02647	.99965	.04391	.99904	.06134	.99812	.07875	.99689	29
32	.00931	.99996	.02676	.99964	.04420		• <b>0</b> 6163	.99810	.07904	.99687	28
33	.00960	.99995	.02705	.99963	.04449	.99901	.06192		.07933	. <b>9</b> 9685	27
34 35	.00989	·99995	.02734 .02763	.99963 .99962	.04478 .04507	.99900 .9 <b>9</b> 898	.06221 .06250	.99806 .99804	.07962 .07991	.99683 .99680	26 25
36	.01047	.99995	.02792	.99961	.04536	.99897	.06279		.08020	.99678	24
	.01976	199994	.02821	.99960	.04565	.99896	.06308	.99801	.08049	99676	23
37 38	.01105	99994	.02850	-99959	.04594	.99894		· <b>997</b> 99	.08078	.99673	22
39	.01134	99994	.02879	.99959	.04623	· <b>99</b> 893	.06366	.99797	.08107	.99671	21
40 41	.01164 .01193	.99993 .99993	.02908 .02938	.99958 .99957	.04653 .04682	.99892 .99890	.06395 .06424	-99795   -99793	.08136 .08165	.99668	20 19
42	.01222	.99993	.02950	.99956	.04711	.99889	.06453	.99793	.08194	.99664	18
43	.01251	.99992	.02996	·99955	.04740	.99888	.06482	.99790	.08223	.99661	17
44	.01280	.99992	.03025	·99954	.04769	. <b>9</b> 9886	.06511	.99788	.08252	.99659	16
45	.01309	.99991	03054	.99953	.04798		.06540			.99657	15
46 47	.01338 .01367	.99991 .99991	.03083 .03112	.99952 .99952	.04827 .04856	.99883 .99882	.06569 .06598		.08310 .08339	.99654 .99652	14 13
48	.01396	.99990	.03141	.99951	.04885	.99881	.06627	.99780	.08368	.99649	12
49	.01425	.99990	.03170	.99950	.04914	.99879	.06656	.99778		.99647	11
50	01454	.99989	.03199	.99949	.04943	1 , , , ,	.06685	. <b>9</b> 9776			10
51 52	.01483	.99989	.03228	.99948		.99876	.06714	.99774		.99642	
52 53	.01513 .01542	.99989 .99988	.03257 .03286	·99947 ·99946	.05001 .05030		.06743 .06773	·99772 ·99770		.99639 .99637	, °
54	.01571	.99988	.03316	.99945	.05059		.06802	.99768	.08542	.99635	7
55	.01600	.99987	.03345			.99870	.06831	.99766	.08571	.99632	5
56	.01629	.99987	.03374	.99943	.05117	.99869	.06860	.99764	.08600	.99630	4
57 58	.01658	.99986			.05146						3
50	.01687 .01716	.99986 .99985	.03432 .03461		.05175 .05205						2
59 60	.01745	.99985	.03490								0
		N. sine							N. cos.		
<b> </b>		9°		8°		70		6°		,	<u> </u>
<u></u>		<i>U</i>	- 8	G		•	. 8	<u> </u>	85°		

Ī		5	٥	0	°	7	,0	8	°	9	°	
	,	N. sine	N. cos.	N. sine	N. cos.	N. sine	N. cos.	N. sine	N. cos.	N. sine	N. cos.	
	0	.08716			.99452	12187		.13917			.98769	60
1	I 2	.08745 .08774	.99617 .99614	.10482 .10511	·99449 ·99446		.99251 .99248	.13946 .13975	.99023		.98764 .98760	59 · 58
1	3	.08803	.99612	.10540	-99443	.12274	.99244	-14004		.15730	.98755	57
	4	.08831 .08860	.99609 .99607		.99440 .99437				.99011	.15758	.98751	56
	5	.08889	.99604		·99434		.9923 <b>7</b> .99233	.14061 .14090	.99006	.15787 .15816	.98746 .98741	55 54
	7 8	.08918	.99602	.10655	.99431	.12389	.99230	.14119	.98998	.15845	.98737	53
	8	.08947 .08976	. <b>9</b> 9599 . <b>995</b> 96	.10684 .10713	.99428 .99424	12418 12447	.99226	.14148 .14177	.98994 .98990	.15873	.98732 .98728	52
	10	.09005	·99594	.10742	99421	.12476		.14205			.98723	51 50
	11	.09034 .09063	.99591	.10771	.99418		.99215	.14234	.98982	.15959	.98718	40
ŀ	12	.09003	99588 99586	.10829	.99415	.12533	.99211	.14263 .14292	98978	.15988 .16017	.98714	48
	14	.09121	.99583	. 10858	.99409	.12591	.99204				.98704	47 46
	15 16	.09150	.99580		.99406			.14349	.98965	16074	.98700	45
	17	.09179 .09208	·99578 ·99575	.10916 .10945	.99402 .99399	.12649 .12678	.99197 .99193	.14378 .14407	.98961 .98957	.16103 .16132	.98695 .98690	44
	18	.09237	.99572	.10973	.99396		.99189	.14436	.98953	.16160	.98686	42
	19	.09266	.99570	11002	.99393	.12735	.99186	.14464	.98948	.16189	.98681	41
	20 21	.09295 .09324	99567	.11031	.99390 .99386	.12764 .12793	.99182 .99178	.14493 .14522	.98944 .98940		.98676 .98671	39
	22	.09353	.99562	.11089	.99383	12822	99175	.14551	.98936	.16275	98667	38
	23 24	.09382 .09411	.99559	.11118 .11147	.99380 .99377	.12851 .12880	.99171 .99167	.14580 .14608	.98931 .98927	.16304	.98662 .98657	37
ŀ	25	.09440	·99556 ·99553	.11176	·99374	.12908	.99163	.14637	.98923	.16333	.98652	36
	26	.09469	.99551	.11205	.99370		.99160	. 14666	.98919	.16390	.98648	34
	27 28	.09498	.99548		.99367				.98914		.98643	33
	29	.09527 .09556	·99545 ·99542	.11263 .11291	.99364 .99360		.99152 .99148	.14723 .14752	.98910 .98906		.98638 .98633	32 31
	30	.09585	.99540		-99357	.13053	.99144	.14781	.98902		.98629	30
ı	31	.09614	.99537	.11349	-99354	.13081	.99141	.14810	.98897	.16533	.98624	29
ı	32 33	.09642	·99534 ·99531	.11378 .11407	.99351 . <b>99</b> 347	.13110		.14838 .14867	.98893 .98889	.16562 .16591	.98619 .98614	28 27
	34	.09700	.99528	.11436	.99344	.13168	.99129	.14896	.98884	.16620	.98609	26
	35 36	.09729 .09758	.99526 .99523		.99341 .99337	.13197 .13226		.14925 .14954	.98880 .98876		.98604	25 .
ŀ	37-	.09787	.99520	.11494	·99334	.13254	.99118	.14982	-98871	.16706		23
	38	.09816		.11552	.99331	.13283	.99114	.15011	98867	.16734	.98590	22
	39	.09845 .09874	.99514		.99327	.13312				.16763	.98585	21
	40 41	.09903	.99 <b>511</b>	.11609 .11638	.99324 .99320	.13341 .13370	.99106 .99102	.150 <u>60</u> .150 <del>67</del>	.98854	.16820		20 19
	42	.09932	.99506	.11667	.99317	.13399	.99098	.15126	.98849	.16849	.98570	18
	43	.09961	.99503	.11696	.99314		.99094	.15155 .15184	.98845 .98841	.16878 .169 <b>0</b> 6	.98565	17
	44 45	.10019	.995∞ .99497		.99310		.99087	.15104	98836	. 16635	.98561 .98556	16 15
	46	.10048	·99494	.11783	.99303	.13514		.15241	.98832	16964	.98551	14
	47 48	.10077 .10106	.99491 .99488	.11812 .11840	.99300	.13543 .13572	.99079 .99075	.15270 .15299			.98546 .98541	13 12
ŀ	49	.10135	.99485	.11869	.99293	.13600	.99071	.15327	.98818		.98536	II
	50	.10164	.99482	.11898	.99290	. 13629	.99067	.15356	.98814	.17078	.98531	10
ı	51 52	.10192 .10221		.11927 .11956		.13658 .13687	.99063 .99059		.98809 .98805	.17107 .17136		
	53	.10250	·99473	.11985	.99279	.13716	.99055	.15442	.98800	.17164	.98516	8 7 6
1	54	.10279			.99276			.15471	.98796			
	55 56	.10308 .10337		.12043 .12071	.99272		.99047 .99043	.15500 .15529		.17222 .17250		5 4 3 2
	57 58	.10366	.99461	.12100	.99265	.13831	.99039	.15557	.98782	.17279	.98496	3
	58	.10395				.13860		.15586			.98491	2
	59 60	.10424 .10453	·99455 ·99452	.12158 .12187		.13889 .13 <b>9</b> 17		.15615 .15643				0
ŀ				N. cos.								<del>-</del>
ŀ			4°		3°		2°		1°		<b>0</b> °	i
١.								<u></u>	-		<u> </u>	<u></u>

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	N. sine	N. cos.	N. sine	N. cos.	N. sine	N. cos.	N. sine	N. cos.	N. sine	N. cos.	
0	17365	.98481	.19081	.98163	20791	.97815	.22495	.97437	.24192	.97030	60
ī	17393	.98476	.19109	.98157	.20820	.97809	.22523	.97430	.24220	.97023	
2	.17422	.98471	.19138	.98152	.20848	.97803	.22552	97424	.24249	.97015	59
	17451	.98466	.19167	.98146	.20877	97797	.22580	.97417	.24277	.97008	57
3	.17479	.98461	.19195	.98140	.20905	97791	.22608	.97411	.24305	.97001	57
4	17508	.98455	.19224	.98135	.20933	97784	.22637	.97404	.24333	.96994	55
5		.98450	.19252	.98129	20962	97778	.22665	.97398	.24362	.96987	
_	.17537			-	-				-	-	54
7 8	.17565	.98445	.19281	.98124	.20990	-97772	.22693	97391	.24390	.96980	53
	17594	.98440	.19309	.98118	.21019	.97766	.22722	-97384	.24418	.96973	52
9	.17623	.98435	.19338	.98112	.21047	.97760	.22750	-97378	.24446	.96966	51
10	.17651	.98430	.19366	.98107	.21076	97754	.22778	-97371	.24474	.96959	50
11	.17680	.98425	.19395	.98101	.21104	.97748	.22807	97305	-24503	.96952	49
12	.17708	.98420	.19423	.98096	.21132	.97742	.22835	.97358	.24531	.96945	48
13	-17737	.98414	19452	.98090	.21161	.97735	.22863	-97351	.24559	.96937	47
14	.17766	.98409	.19481	.98084	.21189	.97729	.22892	-97345	.24587	.96930	46
15	.17794	98404	19509	.98079	.21218	.97723	.22920	.97338	.24615	.96923	45
16	.17823	.98399	,19538	.98073	.21246	.97717	.22948	.97331	.24644	.96916	44
17	.17852	.98394	.19566	.98067	.21275	.97711	.22977	97325	.24672	.96909	43
18	.17880	.98389	-19595	,98061	.21303	.97705	.23005	.97318	.24700	.96902	42
19	.17909	.98383	.19623	.98056	.21331	.97698	.23033	.97311	,24728	.96894	41
20	.17937	.98378	.19652	.98050	.21360	.97692	.23062	.97304		.96887	40
21	.17966	.98373	.19680	.98044	.21388	.97686	.23090	.97298	.24756	.96880	
22	.17995	.98368	.19709	.98039	.21417	.97680	.23118	.97291	.24813	.96873	39
23	.18023	.98362	.19737	.98033	.21445	.97673	.23146	.97284	.24841	.96866	37
24	.18052	.98357	.19766	.98027	.21474	.97667	.23175	.97278	.24869	.96858	36
25	.18081	.98352	.19794	.98021	.21502	.97661	.23203	.97271	.24897	.96851	35
26	.18109	.98347	.19823	.98016	.21530	.97655	.23231	.97264	.24925	.96844	34
27	.18138	.98341	.19851	.98010	.21559	.97648	.23260	.97257	.24954	.96837	33
28	.18166	.98336	.19880	.98004	.21587	.97642		.97251	.24982	.96829	32
29	.18195	.98331	.19908	.97998	.21616	.97636	.23316	.97244	.25010	.96822	31
	.18224	.98325	.19937	.97992	21644	.97630	.23345	.97237	.25038	.96815	30
30	-				.21672	.97623	.23373		.25066	.96807	20
31	.18252	.98320	.19965	.97987	.21701	.97617	.23401	.97230	.25004	.96800	28
32	.18309	.98315	19994	.97981	.21729	97611		.97217	25122	.96793	27
33	.18338	,98310	20022	97975	.21758	.97604		.97210	.25151	.96786	26
34	.18367	-98304	.20051	.97969	.21786	.97598	.23486	.97203	.25179	.96778	25
35		.98299	.20079	97963	.21814	.97592	.23514	.97196	25207	.96771	24
36	.18395	.98294		97958	-				-		-
37 38	.18424	.98288	.20136	-97952	.21843	.97585	.23542	.97189	-25235	.95764	2
	.18452	.98283	.20165	.97946	.21871	97579		.97182	.25263	.96756	2
39	.18481	.98277	.20193	.97940	.21899	97573	.23599	.97176	.25291	.96749	21
40	.18509	.98272	-20222	-97934	.21928	.97566		.97169		.96742	20
41	.18538	.98267	.20250	.97928	-21956	.97560				.96734	2
42	.18567	.98261	.20279	.97922	21985	97553	.23684	-97155	.25376	.96727	13
43	.18595	.98256	.20307	.97916	-22013	.97547	.23712	.97148	.25404	.96719	I,
44	.18624	98250	.20336			97541				.95712	1
45	-18652	.98245	20364	.97905	.22070	-97534				.96705	L
46	18681	.98240	.20393	.97899							L
47	18710	.98234	.20421	.97893	.22126			.97120		.9.090	I
48	18738	.98229	.20450	.97887	.22155	97515		.97113	.25545	.96682	T
49	.18767	.98223	.20478	.97881	.22183	.97508	.23882			.96075	I
50	.18795	.98218		.97875	.22212	.97502	.23910	.97100	.25601		I
51	18824	.98212		.97869	.22240	.97496	.23938	.97093	.25629		1
52	.18852	.98207	.20563		.22268	.97489	.23966		.25657		
53	.18881	.98201	.20592	-97857	.22297	.97483			.25685		
54	.18910	.98196	.20620		.22325		.24023	.97072	.25713	-96638	
55	.18938	.98190	.20649	- 0		-97470	.24051		-	.96630	
55 56	.18967										
57	.18995		.20706	.97833				.97051			1
57 58	.19024									.96608	
50	.19052										
59	.19081									.96593	
	-	- 0				_			N. cos.		_
-		9°	-	8°	_	70	-	6°		5°	1

0 1 2 3 4 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25 26 27 28 29 30 31 32 33 34 35	N. sine  25882 25916 25938 25906 25994 26022 26050 26079 26107 26135 26103 26247 26275 26387 26387 26443 264471	96593 96578 96578 96576 96562 96555 96540 96592 96517 96509 96502 96479 96479 96471 96463	.27676 .27704 .27731 .27759 .27787 .27815 .27843 .27871 .27899	N. cos. .96126 .96118 .96110 .96102 .96086 .96078 .96070 .96062 .96054 .96046 .96054 .96037 .96037	N. sine  29237 29265 29293 29321 29348 29376 29400 29487 29487	N. cos, 95630, 95622, 95613, 95605, 95588, 95579, 95571, 95562	N. sine  30902 30929 30957 30985 31012 31040 31068	.95106 .95097 .95088 .95079 .95070 .95061 .95052	32557 32584 32612 32639 32667 32694 32722 32749	-94552 -94542 -94533 -94523 -94514	60 59 58 57 56 55 54
1 2 3 4 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25 26 27 28 29 30 31 32 33 34 35	25910 25938 25906 25909 26022 26059 26103 26103 26191 26247 26275 26303 26331 26359 26387 26415 26443	.96585 .96578 .96562 .96565 .96547 .96540 .96532 .96524 .96509 .96502 .96494 .96486 .96479 .96479 .96463	.27592 .27620 .27648 .27676 .27704 .27731' .27759 .27815 .27843 .27899 .27927 .27955	.96118 .96110 .96102 .96094 .96086 .96078 .96070 .96062 .96054 .96046	.29265 .29293 .29321 .29348 .29376 .29404 .29432 .29460 .29487	.95622 .95613 .95605 .95595 .95588 .95579 .95571	.30929 .30957 .30985 .31012 .31040 .31068	.95097 .95088 .95079 .95070 .95061 .95052	.32584 .32612 .32639 .32667 .32694 .32722 -32749	.94542 .94533 .94523 .94514 .94504 .94495	59 58 57 56 55 54
2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25 26 27 28 29 30 31 32 33 33 34 35 35 36 36 36 37 37 38 37 38 37 38 37 38 38 38 38 38 38 38 38 38 38 38 38 38	25938 25906 25994 26022 26050 26079 26135 26163 26191 26219 26247 26275 26331 26331 26339 26387 26345 26345	96578 96570 96562 96555 96547 96542 96532 96524 96570 96502 96494 96471 96463	27620 27648 27676 27704 27731 27759 27787 27815 27843 27871 27899 27927 27955	96110 96102 96094 96086 96078 96070 96062 96054 96046	.29293 .29321 .29348 .29376 .29404 .29432 .29460 .29487	.95613 .95605 .95596 .95588 .95579 .95571	.30957 .30985 .31012 .31040 .31068	95088 -95079 -95070 -95061 -95052	.32612 .32639 .32667 .32694 .32722 -32749	-94533 -94523 -94514 -94504 -94495	57 56 55 54
3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25 26 27 28 29 30 31 32 33 34 35 36 37 37 38 38 38 38 38 38 38 38 38 38 38 38 38	25966 25994 26022 26050 26107 26135 26163 26191 26247 26275 26303 26331 26359 26387 26445	.96570 .96562 .96555 .96547 .96540 .96532 .96524 .96517 .96509 .96494 .96470 .96471 .96463	.27648 .27676 .27704 .27731 .27759 .27787 .27815 .27843 .27871 .27899 .27927	.96102 .96094 .96086 .96078 .96070 .96062 .96054 .96046	.29321 .29348 .29376 .29404 .29432 .29460 .29487	.95605 .95596 .95588 .95579 .95571 .95562	.30985 .31012 .31040 .31068	-95079 -95070 -95061 -95052	-32639 -32667 -32694 -32722 -32749	·94523 ·94514 ·94504 ·94495	57 56 55 54
7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25 26 27 28 29 30 31 32 33 34 35	.25994 .26022 .26050 .26079 .26103 .26191 .262191 .26247 .26275 .26303 .26331 .26359 .26387 .26443	.96562 -96555 -96547 -96540 -96532 -96517 -96502 -96494 -96463 -96479 -96463	.27676 .27704 .27731 .27759 .27787 .27815 .27843 .27871 .27899 .27927	.96094 .96086 .96078 .96070 .96062 .96054 .96046	.29348 .29376 .29404 .29432 .29460 .29487	.95596 .95588 .95579 .95571 .95562	.31012 .31040 .31068	.95070 .95051 .95052	.32667 .32694 .32722 -32749	.94514 .94504 .94495	56 55 54
5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25 26 27 28 29 30 31 32 33 34 35 36 37 38 38 38 38 38 38 38 38 38 38	.26022 .26050 .26079 .26103 .26103 .26163 .26191 .26219 .26247 .26303 .26331 .26331 .26339 .26387 .263443	96547 96540 96532 96524 96517 96509 96502 96494 96486 96479 96463	.27704 .27731 .27759 .27787 .27815 .27843 .27871 .27899 .27927 .27955	.96078 .96070 .96062 .96054 .96046	.29404 .29432 .29460 .29487	.95588 .95579 .95571 .95562	.31068	.95051 .95052	-32694 -32722 -32749	·94504 ·94495	55 54
7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25 26 27 28 29 30 31 32 33 34 35	.26079 .26107 .26135 .26163 .26191 .26219 .26247 .26303 .26303 .26331 .26359 .26345 .26443	.96540 .96532 .96524 .96517 .96509 .96502 .96494 .96486 .96479 .96463	.27759 .27787 .27815 .27843 .27871 .27899 .27927 .27955	.96070 .96062 .96054 .96046	.29432 .29460 .29487	.95571 .95562	.31095	.95043	-32749	the same of the sa	
9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25 26 27 28 29 30 31 32 33 34 35	.26107 .26135 .26163 .26191 .26219 .26247 .26275 .26303 .26331 .26359 .26387 .26443	.96532 .96524 .96517 .96509 .96502 .96494 .96486 .96479 .96463	.27787 .27815 .27843 .27871 .27899 .27927	.96062 .96054 .96046 .96037	.29460	.95562				-94485	E 75 1
9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25 26 27 28 29 30 31 32 33 34 35	.26135 .26103 .26191 .26219 .26247 .26275 .26303 .26331 .26359 .26387 .26415 .26443	.96524 .96517 .96509 .96502 .96494 .96486 .96479 .96471	.27815 .27843 .27871 .27899 .27927 .27955	.96054 .96046 .96037	.29487		7311231				53
10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25 26 27 28 29 30 31 32 33 34 35	.26163 .26191 .26219 .26247 .26275 .26303 .26331 .26359 .26387	.96517 .96509 .96502 .96494 .96486 .96479 .96471	.27843 .27871 .27899 .27927 .27955	.96046			.31151	.95033	32777	·94476	52
11 12 13 14 15 16 17 18 19 20 21 22 23 24 25 26 27 28 29 30 31 32 33 34 35	.26219 .26247 .26275 .26303 .26331 .26359 .26387 .26415 .26443	.96509 .96502 .96494 .96486 .96479 .96471	.27871 .27899 .27927 .27955	.96037		·95554 ·95545	.31178	.95015	.32832	-94457	50
13 14 15 16 17 18 19 20 21 22 23 24 25 26 27 28 29 30 31 32 33 34 35	.26247 .26275 .26303 .26331 .26359 .26387 .26415 .26443	.96494 .96486 .96479 .96471 .96463	.27927	.900201	.29543	95530	.31206	.95006	32859	-94447	49
14 15 16 17 18 19 20 21 22 23 24 25 26 27 28 29 30 31 32 33 34 35	26275 26303 26331 26359 26387 26415 26443	.96486 .96479 .96471 .96463	.27955		.29571	.95528	.31233	94997	32887	-94438	48
15 16 17 18 19 20 21 22 23 24 25 26 27 28 29 30 31 32 33 34 35	26331 26331 26359 26387 26415 26443	.96479 .96471 .96463	.27955	.96021	.29599	.95519	.31261	.94988	-32914	-94428	47
16 17 18 19 20 21 22 23 24 25 26 27 28 29 30 31 32 33 34 35	26331 26359 26387 26415 26443	.96471 .96463	.27983	.96005	.29626	.95502	·31289 ·31316	·94979	.32942	.94418	46
17 18 19 20 21 22 23 24 25 26 27 28 29 30 31 32 33 34 35	26359 26387 26415 26443	.96463	28011	95997	.29682	95493	31344	.94961	.32969	.94409	45
20 21 22 23 24 25 26 27 28 29 30 31 32 33 34 35	26415		.28039	.95989	.29710	.95485	.31372	.94952	.33024	.94390	43
20 21 22 23 24 25 26 27 28 29 30 31 32 33 34 35	.26443	,96456	-28067	.95981	.29737	95476	-31399	94943	-33051	.94380	42
21 22 23 24 25 26 27 28 29 30 31 32 33 34 35		.96448	.28095	.95972	.29765	.95467	-31427	.94933	-33079	.94370	41
22 23 24 25 26 27 28 29 30 31 32 33 34 35		.96440	.28123	95964	.29793	95459	-31454	94924	.33106	.94361	40
23 24 25 26 27 28 29 30 31 32 33 34 35	26500	96433	.28150 .28178	95956	.29821	95450	31482	94915	-33134 -33161	.94351 .94342	39
25 26 27 28 29 30 31 32 33 34 35	.26528	.96417	.28206		.29876	95433	31537	94897	.33189	.94332	37
26 27 28 29 30 31 32 33 34 35	.26556	.96410	28234	.95931	.29904	95424	-31565	.94888	.33216	.94322	36
27 28 29 30 31 32 33 34 35	.26584	-96402	.28262	95923	.29932	.95415	-31593	.94878	-33244	-94313	35
28 29 30 31 32 33 34 35	26612	.96394	-28290	.95915	29960	.95407	.31620	.94869	-33271	.94303	34
30 31 32 33 34 35	.26668	96386	28318 28346	95907	29987	-95398 -95389	-31648	.94860	33298	.94293	33
30 31 32 33 34 35	.26696	.96379 .96371	.28374	.95898	.30015	95380	-31675 -31703	.94842	-33326 -333 <u>5</u> 3	.94284	32
31 32 33 34 35	.26724	.96363	28402	.95882	.30071	95372	.31730	.94832	-33381	.94264	30
32 33 34 35	.26752	.95355	28429	95874	-30098	-95363	-31758	.94823	-33408	94254	29
34 35	.26780	.96347	.28457	95865	-30126	95354	.31786	.94814	-33436		28
35	.26836	96340	.28485	95857	.30154	+95345	.31813	.94805	-33463		27
35	26864	.96332	.28513	95841	30209	·95337 ·95328	31841	94795	33490	94225	26
36	.26892	.96310	.28569	95832	.30237	.95319	.31896	-94777	-33545	.94206	24
-	-26920	.96308	.28597	.95824	.30265	-95310	-31923	-94768	-33573	.94196	23
37 38	26948	.96301	-28625	.95816		.95301	1000	.94758	.33600	.94186	22
39	.26976	.96293		95807	.30320	-95293	.31979	-94749	-33627	.94176	21
40	27004	.96285	.28680	95799	30348		32006	94740	·33655 ·33682	.94157	10
42	.27000	.96269		95782	-30403	.95266	:32061	94721	.33710	.94147	18
43	.27088	.96261	.28764	95774	-30431	-95257	-32089		33737	-94137	17
44	.27116	.96253	.28792	-95766	-30459	.95248	.32116	-94702	33764	.94127	16
45	.27144	96246		-95757	-30486		.32144	94603	33792	.94118	15
46	.27172	.96238		95749	30514		.32171	.94684		.94108	13
47	.27228	.96222	.28903	-95732	30570	-95213	.32227	.94665	33874	.94088	12
49	.27256	96214	-28931	95724	-30597	.95204	.32254	.94656	-33901	94078	11
50	27284	-96206	.28959	-95715	.30025	.95195	.32282	.94646	-33929	.94008	10
51	27312	.96198		-95707	.30653	.95186			-33956	.94058	2
52 53	27340		-29015 -29042		.30680	95177				.94049	8
54	27396				.30736		6 0				7 6
55	-27424	-	-			-	-	-		-	
50	.27452	.96158	-29126	.95664	.30791	95142	-32447	.94590	-34093		5 4 3 2
57 58	-27480				.30819	-95133	.32474				3
58	27508				-30846		32502				2 I
59		.96134					-32529 -32557				0
	.2750A		-						N. cos.		-
-	27564 N. cos.	100	7		-	the second	100 000	100000000000000000000000000000000000000		THE RESERVE	

	2	0°	2	1°	2	2°	9	3°	2	<b>4°</b>	1
,	N. sine	N. cos.	N. sine	N. cos.	N. sine	N. cos.	N. sine	N. cos.	N. sine	N. cos.	
0	.34202	,,,,	35837	.93358	.37461	.92718					
2	.34229 .34257	·93959 ·93949	.35864 .35891	.9334 <b>8</b> . <b>9</b> 333 <b>7</b>	.37488 .37515	.92707 .92697	.39100 .39127		.40700 .40727	7-313	59 58
3	.34284	· <b>9</b> 3939	35918	.93327	37542	92686	.39153	.92016	.40753	.91319	57
5	-34339	.93 <b>92</b> 9 .93919	·35945 ·35973	.9331 <b>6</b> .93306	·37595	.92664	.39180 .39207		.40780 .40806	.91307 .91295	56 55
5 6	.34366	.93909	.36000	.93295	.37622	.92653	·39234	.91982	40833	.91283	54
7 8	- <b>3439</b> 3 -34421	. <b>9</b> 3899 . <b>93889</b>	.36027 .36054	.93285 . <b>9</b> 3274	.37649 .37676	.92642 .92631	.39260 .39287		.40860 .40886	.91272 .91260	53 52
9	34448	. <b>93</b> 879	36081	.93264	.37703	92620	.39314	91948	.40913	.91248	51
10	·34475 ·34503	.93869 .93859	.36108 .36135	.93253 .93243	·37730 ·37757	.92609 .92598	.39341 .39367	.91936 .91925	.40939 .40966	.91236 .91224	50 49
12	.34530	.93849	.36162	.93232	37784	.92587	·39394	.91914	.40992	.91212	48
13 14	·34557 ·34584	.93839 .93829	.36190 .3621 <b>7</b>	.93222 . <b>9</b> 3211	.37811 .37838	.92576 . <b>9</b> 2565	.39421 .39448	.91902 .91891	.41019 .41 <b>045</b>		47 46
15	.34612	.93819	.36244	.93201	.37865	.92554	.39474	.91879	.41072	.91176	45
16 17	. <b>346</b> 39 . <b>34</b> 666	.93809 .93799	.36271 .36298	. <b>9</b> 3190 .93180	.37892 .37919	. <b>92</b> 543 .92532	.39501 .39528	.91868 .91856	.41098 .41125	.91164 .91152	44 43
17	.34694	.93789	36325	.93169	37946	.92521	·39555	.91845	.41151		42
19 20	.34721 .34748	·93779 ·93769	.36352 .36379	.93159 .93148	-37973 -37999	. <b>9</b> 2510 . <b>9249</b> 9	.39581	.91833 .91822	.41178 .41204	.91128 .91116	41 40
21	34775	· <b>937</b> 59	36406	93137	38026	.92488	39635	.91810		.91104	39 38
22 23	.34803 .34830	.93748 .93738	.36434 .36461	.93127 .93116	.38053 .38080	. <b>9247</b> 7 . <b>924</b> 66	.39661 .39688	.91799 .91787	.41257 .41284	.91092 .91080	38 37
24	.34857	.93728	36488	.93106	.38107	92455	.39715	91775	41310	.91068	36
25 26	.34884	.93718 .93708	.36515 .36542	.93095	.38134 .38161	.92444 .92432	·39741 ·39768	.91764 .91752	.41337		35
27	.34912 .34939	.93708 .93698	36569	.93084 . <b>9</b> 3074	38188	92432	·39795	.91741	.41363 .41390	.91044 .91032	34 33
28	.34966	.93688	.36596 .36623	.93063	.38215 .38241	.92410	.39822 .39848	91729 91718	.41416		32
29 30	·34993 ·35021	. <b>9367</b> 7 . <b>93</b> 667	.36650	.93052 . <b>930</b> 42	.38268	. <b>9239</b> 9 92388	.39875	.91706	.41443 .41469	.91008 .90996	30
31	.35048	.93657	36677	.93031	.38295	92377	.39902	.91694	.41496	.90984	29
32 33	.35075 .35102	.93647 .93637	.36704 .36731	.93020 .93010	.38322 .38349	. <b>92</b> 366 . <b>92</b> 355	.39928 .39955	.91683 .91671	.41522 .41549	.90972 .90960	28 27
34	.35130	93626	.36758	.92999	.38376	· <b>9</b> 2343	.39982	91660	-41575	.90948	26
35 36	.35157 .35184	. <b>936</b> 16 . <b>9360</b> 6	.36785 .36812	.92988 .92978	.38403 .38430	.92332 .92321	.40008 .40035	91648 91636	.41602 .41628	.90936 .90924	25 24
37 38	.35211	.93596	.36839	.92967	.38456	.92310	40062	.91625	.41655	.90911	23
38	.35239 .35266	.93585 .93575	.36867 .36894	.92956 . <b>92</b> 945	.38483 .38510	. <b>9229</b> 9 . <b>9228</b> 7	.40088 .40115	.91613 .91601	.41681 .41 <b>7</b> 07	.90899 .90887	22 21
40	35293	.93565	.36921	· <b>9</b> 2935	.38537	.92276	.40141	.91590	-41734	.90875	20
41 42	·35320 ·35347	·93555 ·93544	.36948 .36975	.92924 .92913	.38564 .38591	.92265 .92254	.40168 .40195	.91578 .91566	.41760 .41787	.90863 .90851	19 18
43	-35375	.93534	.37002	.92902	.38617	.92243	.40221	.91555	.41813	.90839	17
44 45	.35402 .35429	.93524 .93514	.37029 37056	.92892 .92881	.38644 .38671	. <b>922</b> 31	.40248 .40275	.91543 .91531	.41840 .41866	.90826 .90814	16 15
46	35456	.93503	.37083	.92870	.38698	. <b>922</b> 09	.40301	.91519	.41892	.90802	14
47 48	35484	·93493 ·93483	.37110	. <b>92859</b> .92 <b>84</b> 9	.38725 .38752	. <b>921</b> 98 . <b>921</b> 86	.40328 .40355	.91508 .91496		.90790 .90778	13 12
49	.35538	.93472	.37164	.92838	.38778	.92175	.40381	.91484	41972	.90766	11
50 51	.35565 .35592	.93462 .93452				.92164					10 9
52	.35619	.93441	.37245	.92805	.38859	.92141	.40461	.91449	.42051	.90729	8
53 54	.35647 .35674	.93431 .93420	.37272 .37299	. <b>927</b> 94 . <b>9278</b> 4		.92130					
55	.35701	.93410	.37326	92773	.38939	.92107	.40541	.91414	.42130	.90692	- 5
56	.35728 .35755	.93400		.92762	.38966 .38993					.90680	I 4 1
58	.35782	.93379	.37407	.92740	.39020	.92073	.40621	.91378	.42209	.90655	2
55 56 57 58 59 60	.35810 .35837	.93368 .93358	·37434 ·37461				.40647 .40674		.42235 .42262		
										N. sine	
		9°		8°		7°		<b>6°</b>	l	5°	

	2	5°	2	6°	2	7°	2	8°	2	9°	1
,	N. sine	N. cos.	N. sine	N. cos.	N. sine	N. cos.	N. sine	N. cos.	N. sine	N. cos.	
0	.42262		43837	.89879	45399	.89101	-46947	.88295	.48481	.87462	60
1	.42288	.90618	43863	.89867	45425	.89087	-46973		-48506	.87448	5
2	-42315	.90606	.43889	.89854	45451	.89074	-46999	.88267	.48532	87434	55
3	.42341	.90594	43916	.89841	-45477	.89061	47024	.88254	-48557	.87420	5
4	-42367		-43942	.89828	-45503		47050		-48583	87406	5
5	-42394				45529		-47076			.87391	5
5	.42420		-43994		45554		47101		.48634		5,
	-42446		-44020	-	.45580	-	-	-			-
78		2 2 10			.45606		-47127		.48659		53
	-42473		.44046	.89777			47153				5:
9	-42499		-44072	.89764	.45632		-47178	.00172	-48710	.87335	5
01	.42525		.44098		-45658	.88968	.47204		-48735	.87321	50
11	-42552		-44124		-45684		.47229		.48761	.87306	49
12	-42578	.90483	-44151	89726	45710		47255	88130	48786		48
13	.42604	.90470	-44177	.89713	-45736	.88928	47281	.88117	.48811	.87278	4
14	.42631	.90458	-44203	.89700	-45762	.88915	47306	.88103	.48837		46
15	-42657	.90446	-44229	.89687	-45787	.88902	47332		48862		45
16	-42683		-44255	.89674	45013	.88888	47358		48888	.87235	44
17	.42709		.44281	.89662	45839	.88875	47383	.88062	.48913	.87221	43
18	.42736			.89649	45865		47409	25.25	48938	.87207	
-	-	_		and the fact of		the second second second	-				42
19	.42762		-44333	.89636	.45891	00048	47434	.88034	48964	.87193	41
20	.42788		-44359	.89623	45917		47460	88020	.48989		40
21	.42815		-44385	.89610	-45942		47486	.88006	.49014		39
22	.42841	7 00.	-44411	.89597	.45968	.88808	47511	87993	.49040		38
23	.42867	.90346		.89584	·45994		-47537	.87979	.49065	.87136	37
24	.42894	.90334	-44464	.89571	.46020		-47562	.87965	.49090		37
25	.42920	.90321	-44490	.89558	-46046	.88768	-47588	.87951	.49116	.87107	35
26	.42946	3 3	-44516	.89545	46072	.88755	47614	.87937	.49141	.87093	34
	42972		-44542	.89532	.46097	.88741	.47639	.87923	.49166		
27 28	42999		.44568	.89519	.46123	.88728	.47665	87909	.49192		33
29	43025	.90271	-44594	.89506	.46149		.47690				32
	43051		.44594	.89493	.46175	.88701			49217	.87050	31
30	-	_	-				47716		49242	.87036	30
31	43077	.90246	.44646	.89480	.46201		47741	-87868	.49268	.87021	20
32	.43104		-44672	.89467	.46226		47767	87854	.49293	.87007	28
33	-43130		.44698	.89454	-46252		-47793	87840	.49318		27
34	-43156		-44724	.89441	.46278		47818	.87826	-49344	.86978	26
35	-43182		-44750	.89428	.46304		47844	.87812	.49369	.86964	25
36	-43209	.90183	-44776	.89415	.46330		-47869	.87798	-49394	.86949	24
	-43235	-	44802	.89402	46355		47895	87784	-49419		2
37 38	.43261	.90158	-44828	.89389	46381	.88593	47920		49445		22
39	-43287		-44854	.89376			47946	87756			21
40	43313		-44880	89363	46433			87742	49470	an esta	
	.43340				46458		47971	87743	49495		20
41			-44906			885333	-47997	.87729	49521	.86878	10
42	-43366	-	Secretary of the Control of the Cont	89337	46484		.48022		49546	_	15
43	-43392	.90095	-44958	-89324	.46510	.88526	-48048		49571	.86849	1
44	.43418		-44984		-46536		.48073	.87687	-49596		16
45	-43445		45010	.89298	46561		.48099		.49622	.86820	1
46	-43471	.90057	45036	.89285	.46587		.48124	.87659	-49647		12
47	-43497		-45062	.89272	.46613		48150		49672		13
47 48	43523		.45088	.89259	46639		.48175	.87631	49697		12
_	-43549			.89245	.46664		-	-	-		-
49			100			.88431	48201	87617	-49723		I
50	43575		-45140								10
51	43602			89219		80.417	48252	.87589		.86733	8
52	.43628								.49798 .49824	.86719	
53	.43654			89193		.88390	48303				1
54	.43680	-		and the second		.88377	48328	.87546	49849	.86690	(
55 56	.43706	.89943	.45269	.89167			48354	-87532	-49874	.86675	-
56	.43733		-45295			.88349	48379	.87518			4
57				.89140	.46870		48405	.87504	49924	A second second second	- 5
58	-43759 -43785	.89905		.89127	.46896			.87490	49950		100
50	43811	.89892			-46921		A8456	.87476	49930		1
57 58 59 60	43837		45373	.89101	.46947		48481	.87462			
77					-	N. sine	-		.50000		-
- 7	_	4°	-	3°			-	-		o°	,
	45	44-	45	45	- 6	20	6	10	G	454	

	3	0°	3	1°	3	2°	3	3°	3	4°	
,	N. sine	N. cos.	N. sine	N. cos.	N. sine	N. cos.	N. sine	N. cos.	N. sine	N. cos.	
0	.50000	.86603	-51504	.85717	52992	.84805	-54464	.83867	.55919	.82904	60
1	-50025	.86588	.51529		.53017	.84789	.54488	.83851	-55943	.82887	
2	+50050	.86573	-51554	.85687	-53041	.84774	-54513	.83835	-55968		59 58
3	.50076	.86559	.51579		.53066	.84759	-54537	.83819	55992		57
4	.50101	.86544	.51604		.53091	.84743	.54561		.56016		56
5	.50126	.86530	.51628	.85642	-53115	.84728	-54586	.83788	.56040		55
6	.50151	.86515	.51653	.85627	-53140	.84712	.54610	.83772	.56064		54
7 8	.50176	.86501	.51678	.85612	-53164	.84697	.54635	.83756	.56088	.82790	53
8	.50201	.86486	-51703	.85597	-53189	.84681	.54659	.83740	.56112	.82773	52
9	.50227	.86471	-51728	.85582	-53214	.84666	.54683	.83724	.56136	.82757	51
10	.50252	.86457	-51753	.85567	-53238	.84650	.54708	.83708	.56160		50
11	.50277	.86442	.51778	.85551	-53263	.84635	-54732	.83692	.56184	.82724	49
12	.50302	.86427	.51803	.85536	-53288	.84619	-54756	.83676	.56208	.82708	48
13	.50327	.86413	.51828	.85521	-53312	.84604	-54781	.83660	.56232	.82692	47
14	.50352	.86398	.51852	.85506	-53337	.84588	.54805	.83645	.56256	.82675	46
15	.50377	.86384	-51877	.85491	-53361	.84573	.54829	.83629	.56280		45
10	.50403	.86369		85476	-53386	84557	-54854	.83613	.56305	.82643	44
17	.50428	.86354	-51927	85461	-53411	84542	.54878	83597	.56329	.82626	43
_	50453	.86340	-51952	.85446	-53435	.84526	54902	.83581	-56353	.82610	42
19	-50478	.86325	-51977	.85431	.53460	.84511	-54927	.83565	.56377	.82593	41
20	.50503	86310	.52002	.85416	-53484	.84495 .84480	54951	.83549	.56401	.82577	40
21	-50553	.86295	.52026 .52051	85385	-53509	.84464	-54975	.83533 .83517	.56425	.82561	39 38
	-50578	.86266	.52076	85370	53534	.84448	-54999	.83501	.56449	.82544	
23	.50603	.86251	52101	85355	53558	.84433	-55024	.83485	.56473 .56497	.82528	37
	.50628	86237	.52126	.85340	.53607	.84417	-55072	.83469	.56521	.82495	
25 26	50654	86222	.52151	85325	.53632	.84402	-55097	.83453	.56545		35
	.50679	.86207	.52175	.85310	.53656	.84386	-55121	83437	.56569	.82478 .82462	34
27 28	.50704	.86192	.52200	.85294	.53681	.84370	-55145	83421	.56593	.82446	33
20	.50729	.86178	.52225	.85279	-53705	.84355	-55169	.83405	.56617	.82429	31
30	-50754	.86163	.52250		-53730	.84339	-55194	.83389	.56641	.82413	30
31	50779	.86148	.52275	.85249	-53754	.84324	-55218	.83373	.56665	.82396	29
32	.50804	.86133	.52299		-53779	.84308	.55242	.83356	.56689	.82380	28
33	.50829	.86119	-52324		-53804	.84292	.55266	.83340	.56713	.82363	27
34	.50854	.86104	.52349	.85203	-53828	.84277	.55291	.83324	.56736		26
35	.50879	.86089	-52374	.85188	-53853	.84261	-55315	.83308	.56760	.82330	25
36	.50904	86074	-52399	.85173	-53877	.84245	-55339	.83292	.56784	.82314	24
37	.50929	.86059	-52423	.85157	-53902	.84230	-55363	.83276	.56808	.82297	23
37 38	.50954	.86045	.52448		-53926	.84214	-55388	.83260	.56832	.82281	22
39	-50979	86030	52473	.85127	-53951	.84198	-55412	.83244	.56856		21
40	.51004	,86015	-52498	.85112	-53975	.84182	-55436	.83228	.56880		20
41	.51029	86000	.52522	.85096	54000	84167	.55460		.56904	.82231	19
42	.51054	.85985	-52547	.85081	-54024	.84151	-55484	.83195	.56928		18
43	-51079	.85970	.52572	85066	.54049	.84135	-55509	.83179	-56952	.82198	17
44	.51104	.85956		.85051	-54073	84120	-55533	.83163	.56976	.82181	16
45	.51129	85941	52621	85035	-54097	.84104	-55557	.83147	.57000		15
	-51154	85926	.52646 .52671	.85020	54122	.84072	.55581	.83131	-57024		14
47 48	.51179	.85911 .85896	.52696		-54146	.84057	.55605 .55630		-57047 -57071	.82132	13
_		-	-	.84974		.84041	-	.83082	_		_
49	.51229 .51254	.85881 .85866	-52720 -52745	.84959	-54195 -54220	0	.55654 .55678	.83066	-57095 -57119	.82098 .82082	11
50		.85851	52770	.84943	54244	0	.55702		57142	.82065	10000
51 52		.85836	.52794	.84928	.54269		.55726	.83034	.57167		9
53		.85821					.55750				7
54	-51354		.52844			n a	-55775	.83001	.57215		6
55	-51379	-	.52869	-	-	0 4	-55799	_	-57238	-	5
55 56		.85777	.52893			.83930	-55823			.81982	5
57	-51429	.85762	:52918		-54391		.55847	.82953		.81965	3
57 58	-51454	.85747	-52943	73 10 2		.83899	-55871		-57310		3 2
59		.85732	-52967	84820	+54440	.83883	.55895	.82920			-1
60	-51504		-52992		-54464	.83867	-55919	.82904		.81915	0
_	N. cos	N. sine	N. ros	N. sine	N. cos	N. sine	N. cos	N. sine	N. cor	N. sine	-
_	_			80		70	_	-		3.42	-
		9°	- 75	56.	- 5	7	- 5	6°	15	5°	

	3	5°	3	6°	3	7°	3	8°	3	9°	
,	N. sine	N. cos.	N. sine	N. cos.	N. sine	N. cos.	N. sine	N. cos.	N. sine	N. cos.	
0	-57358	.81915	.58779 .58802	.80902 .80885	60182	.79864	.61566	.78801	.62932	-77715	60
1	.57381	.81899	.58826	.80867	.60205	.79846	.61589	.78783 .78765	.62955	.77696	59 58
2	·57405 ·57429	.81865	.58849		.60251	.79811	.61635	.78747	.62977	.77678 .77660	57
3 4	-57453	.81848	.58873	.80833	.60274	-79793	.61658	.78729	.63022	.77641	56
5	.57477	.81832	.58896	.80816	.60298	.79776	.61681	.78711	.63045	.77623	55
5	-57501	.81815	.58920	.80799	.60321	-79758	.61704	.78694	.63068	.77605	54
7	-57524	.81798	.58943	.80782	.60344	.79741	.61726	.78676	.63090	.77586	53
7 8	.57548	.81782	.58967	.80765	.60367	-79723	.61749	.78658	.63113	.77568	52
9	-57572	.81765	.58990		.60390	.79706	.61772	.78640	.63135	.77550	51
10	-57596	.81748	.59014	.80730	.60414	.79688	.61795	.78622	.63158 .63180	-77531	50
11	-57619 -57643	.81731	.59037	.80696	.60460	.79653	.61841	.78586	.63203	77513	49 48
-	-57667	.81698	.59084	.80679	.60483	.79635	.61864	.78568	.63225	·77494	
13	.57691	.81681	.59108	.80662	.60506	.79618	.61887	.78550	.63248	·77476 ·77458	47 46
15	.57715	.81664	.59131	.80644	.60529	.79600	.61909	.78532	.63271	.77439	45
15 16	-57738	.81647	.59154	.80627	.60553	-79583	.61932	.78514	.63293	.77421	44
	-57762	.81631	.59178	.80610	.60576	-79565	.61955	.78496	.63316	.77402	43
17	.57786	.81614	.59201	.80593	.60599	-79547	.61978	.78478	.63338	-77384	42
19	.57810	.81597	-59225	.80576	.60622	-79530	.62001	.78460	.63361	.77366	41
20	-57833	.81580	.59248	.80558	.60645	.79512	.62024	.78442	.63383	.77347	40
21	-57857	.81563	.59272	.80541	.60668	•79494	.62046	.78424	.63406	.77329	39 38
22	.57881	.81546		.80524	.60691	·79477 ·79459	.62069	.78405 .78387	.63428		
23	.57904 .57928	.81530	.59318	.80489	.60738	.79439	.62115	.78369	.63473	.77292 .77273	37 36
25	-57932	.81/96	.59365	S0472	,60761	-79424	.62138	.78351	.63496	-77255	35
26	.57976	.81479		.80455	.60784	.79406	.62160	.78333	.63518	.77236	34
27	-57999	.81462	-59412	.80438	.60807	.79388		.78315	.63540	.77218	33
28	.58023	.81445	.59436	.80420	.60830		.62206	.78297	.63563	.77199	32
29	.58047	.81428	.59459	.80403	.60853	.79353	.62229	.78279	.63585	.77181	31
30	.58070	.81412	-59482	.80386	.60876	+79335	.62251	.78261	.63608	.77162	30
31	.58094	.81395	-59506	.80368	.60899	.79318	.62274	.78243	.63630	.77144	29
32	.58118	.81378	-59529	.80351	.60922	.79300 .79282		.78225	.63653	.77125	28
33	.58141		-59552	.80334 .80316	.60945			.78188	.63675	.77107	27
34 35	.58189	.81344	-59576 -59599	.80299	.60991	-79247	.62365	.78170		.77070	25
36	.58212	.81310	.59622	.80282		.79229			.63742	.77051	24
27	.58236	.81293	.59646	.80264	.61038	.79211	.62411	.78134	-	-77033	23
37 38	.58260	.81276	.59669			.79193		.78116		.77014	22
39	.58283	.81259	.59693	.80230		.79176	.62456	.78098	.63810	.76996	21
40	.58307	.81242	.59716	.80212		.79158		.78079	.63832	.76977	20
41	-58330	.81225	-59739	.80195	.61130	.79140		.78061			19
42	-58354	-	-59763	.80178		.79122	.62524	_		.76940	18
43	.58378		.59786	.80160		.79105	.62547	.78025			17
44	.58401	.81174	.59809 59832	.80143	.61199	.79069			.63922		15
45 46	58440	.81140	.59856			.79051		.77970	.63966		14
	.58472	.81123	.59879	.80091			.62638		.63989	.76847	13
47 48	.58496			.80073		.79016					12
49	.58519	.81089	-59926	.80056	.61314	.78998	.62683	.77916	.64033	.76810	11
50	.58543	.81072	.59949	.80038	.61337	.78980	.62706	77807	64056	.76791	10
	.58567	.81055	-59972	.80021	.61360	.78962	.62728	.77879	.64078	.76772	9
52	-58590	.81038	-59995	.80003		.78944	.62751	.77861	.64100		8
53	.58614	.81021								1 , , , , ,	7 6
51 52 53 54 55 56 57 58 59		.81004									
55	.58681										-5 4
57	.58708	.80970									3
58	.58731	.80936				78837	.62887				3 2
59	.58755	.80919	.60158	.79881	.61543	.78819	.62909	.77733	.64256	.76623	1
60	.58779	.80902	.60182	.79864	.61566	.78801	.62932	-77715	.64279	-76604	0
	N. cos.	N. sine	N. cos.	N. sine	N. cos.	N. sine	N. cos.	N. sine	N. cos.	N. sine	,
-	1	4°		3°	_	2°		10		0°	-
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	4	0°	4	1°	4	2°	4	3°	4	<b>4</b> °	
,	N. sine	N. cos.	N. sine	N. cos.	N. sine	N. cos.	N. sine	N. cos.	N. sine	N. cos.	`
0	.64279	.76604	.65606		66913		.68200	,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,	.69466		60
I 2	.64301 .64323	. 76586 . 76567			.66935 .66956	·74295 ·74276	.68221 .68242		.69487 .69508		59 58
3	.64346	.76548	.65672	.75414	.66978	.74256	.68264	.73076	69529	.71873	57
4	.64368 .64390	.76530 .76511	.65694 .65716	·75395 ·75375	.66999 .67021	.74237   .7421 <b>7</b>	.68285 .68306		.69549 .69570		56 55
5	.64412	.76492	.65738	.75356	.67043	.74198	.68327	.73016	.69591		54
7 8	.64435	.76473 .76455	.65759 .65781	·75337 ·75318	.67064 .67086	.74178 .74159	.68349 .68370	.72996 .72976	.69612 .69633	.71792	53
ا ۋ	.64457 .64479	76436	.65803	.75299	.67107		.68391	.72957	.69654	.71772 .71752	52 51
10	.64501	.76417	.65825 .65847	.75280 .75261	.67129 .67151	.74120 .74100	.68412 .68434		.69675	.71732	50
11	.64524 .64546	. <b>76398</b> . 76380		.75241	.67172	.74080	.68455	.72897	.69696 .69717		49 48
13	.64568	.76361	.65891	.75222	.67194	.74061	.68476	.72877	.69737	.71671	47
14	.64590 .64612	. 76342 . 76323	.65913 .65935	.75203 .75184	.67215 .67237	.74041 .74022	.68497 .68518	.72857 .72837	.69758 .6977 <b>9</b>	.71650   .71630	46 45
15 16	.64635	.76304	.65956	.75165	.67237 .67258	74002	.68539	.72817	.69800	.71610	44
17 18	.64657 .64679	.76286 .76267	.65978 .66000	.75146 .75126	.67280 .67301	.73983 .73963	.68561 .68582	·72797 ·72777	.69821 .69842	.71590 .71569	43 42
19	.64701	.76248	.66022	.75107	.67323	·73944	.68603	.72757	.69862	.71549	41
20	.64723	.76229	.66044	.75088	.67344	-73924	.68624	.72737	.69883	.71529	40
2 I 22	.64746 .64768	76210 76192	.66066 .66088	.75069 .75050	.67366 .67387	.73904 .73885	.68645 .68666	. <b>72</b> 717 . <b>72</b> 697	.69904 .69925	. 71508   . 71488	39 38
23	.64790	.76173	.66109	.75030	67409	. 73865	.68688	.72677	.69946	.71468	37
24	.64812	.76154 .76135	.66131	.75011	.67430	.73846 .73826	.68709	.72657 .72637	.69966		36 3r
25 26	64876	.76116	66175	·74992 ·74973	.67452 .67473	.73806	.68751	.72617	.70008	.71427 .71407	35 34
27	.64878	.76097	.66197	·74953	.67495	.73787	.68772 .68793	.72597	.70029		33
28 29	.64901 .64923	.76078 .76059	.66218 .66240	·74934 ·74915	.67516 .67538	·73767 ·73747	.68814	·72577 ·72557	. 70049 . 70070	.71366 .71345	32 31
30	.64945	.76041	.66262	.74896	.67559	.73728	.68835	·72537	.70091	.71325	30
31	.64967	. 76022 . 76003	.66284 .66306	.74876 .74857	.67580 .6 <b>7</b> 602	.73708 .73688	.68857 .68878	.72517 .72497	.70112 .70132	.71305 .71284	29 28
32 33	.64989 .65011	.75984			.67623	.73669	.68899		.70152		.27
34	.65033	.75965	.66349		.67645 .67666	.73649	68920	.72457	.70174	.71243	26
35 36	.65055 .65077	75940 75927	.66371 .66393	·74799 ·74780	.67688	. <b>7</b> 3629 . <b>7</b> 3610	.68941 .68962	.72437 .72417	.70195 .70215	.71223 .71203	25 24
37 38	.65100	.75908	.66414	.74760	.67709	.73590	.68983		.70236		23
	.65122 .65144	. 75889 . 75870	.66436 .66458	·74741 ·74722	.67730 .67752	·73570 ·73551	.69004 .69025	·72377 ·72357	.70257 .70277		22 21
39 40	.65166	.75851	.66480	·74703	67773	.73531	.69046	·72337	.70298		20
41 42	.65188 .65210	.75832 .75813	.66501 .66523	·74683 ·74664	.67795 .67816	-73511 -73491	.69067 .69088		.70319 .70339		19 18
43	.65232	·75794	66545	.74644	.67837	73472	.69109	.72277	.70360		17
44	.65254	·75775	.66566	74625	67859	.73452	.69130	.72257	.70381	.71039	16
45 46	.65276 .65298	·75756 ·75738	.66588 .66610		.67880 .67901	·73432 ·73413	.69151 .69172	.72236 .72216	.70401 .70422	.71019 .70 <b>9</b> 98	15 14
47 48	.65320	.75719	.66632	.74567	.67923	·73393	.69193	.72196	70443	.70978	13
	.65342	.757∞ .75680	.66653	·74548 ·74528	.67944 .67965	·73373 ·73353	.69214	.72176 .72156	· 70463 · 70484		12 11
49 50	.65386	.75661	.66697	.74509	.67987	.73333	69256	.72136	.70505	.70916	- 10
51	.65408	.75642	.66718	.74489	.68008	.73314	.69277	.72116 .72095	.70525	. 70896	9
52 53	.65430 .65452	.75623 .75604	.66762	.74451	.68051	.73274	.69319	.72075	.70567	.70855	7
54	.65474	.75585	.66783	·7443I	.68072	·73254	.69340		.70587	.70834	_ 6
55 56	.65496 .65518	.75566 ·75547	.66805 .66827	74412	.68093 .68115	.73234 .73215			.70608 .70628		5 4
57 58	.65540	.75528	.66848	·74373	.68136	.73195	.69403	.71995	70649	.70772	4 3 2
58	.65562 .65584	.75509	.66870	·74353	.68157 .68179		.69424 .69445		. 70670 . 70690		2 I
59 60	.65606	.75490 .75471			.68200		.69466		.70711		0
	N. cos.	N. sine	N. cos.	N. sine	N. cos.	N. sine	N. cos.	N. sine	N. cos.	N. sine	<del>,</del>
	4	9°	4	8°	4	7°	4	6°	4	5°	

## TABLE VI.

## ADDITION AND SUBTRACTION LOGARITHMS.

## PRECEPTS.

I. When difference of given logarithms is less than 2.00.

ADDITION.—Enter table with difference between logarithms as Arg. A, and take out B.

Add B to subtracted logarithm.

SUBTRACTION.—Subtract lesser from greater logarithm; enter with the difference as B, and take out A.

Add A to the subtracted logarithm.

II. When difference of given logarithms exceeds 2.00.

Subtract lesser from greater.

ADDITION.—Enter table with difference as Arg. A, take out B-A and add it to the greater logarithm.

SUBTRACTION.—Enter column B with difference of logarithms; take out B-A, and subtract it from greater logarithm.

		. 1		2 1	- 1		- 1		_ 1	- 1		
A.	В.	0	1	2	8	4	5	6	7	8	. 9	Prop. Pts.
5.	0.00	000	100	001	100	100	001	002	002	003	003	
6.0	-	004	004	005	∞5	003	∞5	<b>∞</b> 5	005	005	005	
6. I	7	205	006	006	006	006	006	006	006	007	007	3   4   5   6
6.2		207	007	007	007	800	008	∞8	008	008	008	1 0.3 0.4 0.5 0.6
6.3	(	2009	0009	009	009	010	010	010	010	010	011	2 0.6 0.8 1.0 1.2
6.4		110	011	011	012	012	012	013	013	013	013	3 0.9 1.2 1.5 1.8 4 1.2 1.6 2.0 2.4
6.5		014	014	014	015	015	015	016	016	017	017	5 1.5 2.0 2.5 3.0
6.6	(	017	018	018	019	019	019	020	020	021	021	6 1.8 2.4 3.0 3.6
6.7	(	022	022	023	023	024	024	025	026	026	027	7 2.1 2.8 3.5 4.2 8 2.4 3.2 4.0 4.8
6.8	(	027	028	029	029	030	031	031	032	033	034	9 2.7 3.6 4.5 5.4
6.9	(	034	035	036	037	038	039	040	041	041	042	"
7.0	_	043	044	045	047	048	049	050	051	052	053	171810110
7.1	1	055	056	057	059	060	<b>o</b> 61	063	064	066	067	7 8 9 10 1 0.7 0.8 0.0 1.0
7.2		069	070	072	074	075	077	079	081	083	085	2 1.4 1.6 1.8 2.0
7.3	,	087	089	091	093	095	097	099	102	104	106	3 2.1 2.4 2.7 3.0
7.4	ł	109	111	114	117	119	122	125	128	131	134	4 2.8 3.2 3.6 4.0
7.5	ŀ	137	140	144	147	150	154	157	161	165	169	5 3.5 4.0 4.5 5.0 6 4.2 4.8 5.4 6.0
7.6	1	173	177	181	185	189	194	198	203	207	212	7 4.9 5.6 6.3 7.0
7.7		217	222	227	233	238	244	249	255	261	267	8 5.6 6.4 7.2 8.0
7.8	1	27.3	280	286	293	299	306	313		328	336	9 6.3 7.2 8.1 9.0
7.9	_	344	352	360	<b>3</b> 68	377	385	394	403	413	422	
8.0		432	442	452	463	474	485	496	507	519	531	
A.	В.	0	1	2	8	4	5	6	7	8	9	Prop. Pts.
										تحقا		

AD	<b>D.</b> { lo	og b og (æ	- log	ga = 1	: A. og a	+ <i>B</i> .		St	лв. {	log a log (a	— lo	$gb = B.$ $0) = \log b + A.$
A.	B.	0	1	2	8	.4	5	6	7	8	8	Prop. Pts.
8.00	0.00		433	434	435	436	437	438	439	440	441	
8.01 8.02		442 452	443 453	444 454	445 456	446 457	447 458	448 459	449 460	450 461	451 462	
8.03		463	464	465	466	467	468	469	470		473	
8.04		474	475	476	477	478	479	480	481	482	483	
8.05 8.06		48 <u>5</u> 496	486 497	487 498	488 499	489 500	490 502	491 503	492 504	494 505	495 506	
8.07		507	508	510	511	512	513	514	515	517	518	
8.08 8.09		519	520	521	523	524	523	526	527	529	530	1 0.2
8.10		531 543	532 545	533 546	535 547	536 548	537 550	538	540	541	542	2 0.4
8.11		556	557	558	560	561	562	551 564	552 565	553 566	55 <u>5</u> 567	3 0.6 4 0.8
8.12		569	570	57 I	573	574	575	577	578	579	581	5 I.O 6 I.2
8.13		582	583	585	586	587	589	590	591	593	594	7 1.4
8.14 8.15		595 609	597 611	598 612	599 613	601 519	602 616	604 618	605 619	606 620	608 622	8 1.6 9 1.8
8.16		623	623	626	628	629	630	632	633	635	636	
8.17 8.18		638	639	641	642	644	643	646	648	649	651	
8.19		652 667	654 669	655 671	657 672	658 674	660 675	661 677	663 678	664 680	666 681	
8.20	·	683	684	686	688	689	691	692	694	696	697	
8.21		699	700	702	703	705	707	708	710	712	713	
8.22 8.23		715 731	716 733	718 735	720 736	721 738	723 740	725 741	726 743	728 745	730	I 0.3 2 0.6
8.24		748	750	752	753	755	757	759	760	762	747 764	2 0.6 3 0.9
8.25		766	767	769	771	773	774	776	778	780	781	4 I.2
8.26 8.27		783 801	78 <u>5</u> 803	787 805	789 807	790 809	792 810	794	796	798	799	5 1.5 6 1.8
8.28		820	822	823	825	827	829	812 831	814 833	816 835	818	7 2.1 8 2.4
8.29		839	841	842	844	846	848	850	852	854	856	9 2.7
8.80		858	860	862	864	866	868	870	872	874	876	
8.31 8.32		878 898	880 900	882 902	884 904	886 906	888 908	910	892 912	89 <u>4</u> 91 <u>5</u>	896	
8.33		919	921	923	925	927	929	931	933	936	917 938	•
8.34		940	942	944	946	948	951	95 <u>3</u>	955	957	959	
8.35 8.36		962 984	964 986	966 988	968 990	970 993	97 <u>3</u> 995	97 5 997	977 999	979 *002	981 *004	1.4
8.37	0.01	006	009	011	013	016	810	020	022	025	027	1 0.4 2 0.8
8.38 8.39		030 053	032	034 058	037 060	039 063	041 065	044	046	048	051	3 1.2
8.40		077	056 080	082	085	087	090	068	070 093	073	100	4 1.0
8.41		102	105	107	110	112	115	117	120	097 I 22		6 2.4
8.42		128	130	133	135	138	140	143	146	148		7 2.8 8 3.2 9 3.6
8.43 8.44		153 180		159	161	164	167	169		175		9   3.6
8.45		207	183 210	185 213	188 215	191 218	193 221	196 224		202 229	204 232	
8.46		235	238	240	243	246	249	252	255	257		
8.47 8.48		263 292	266 295	269 298	272 301	275	278	280	283	286	289	٠.
8.49		322	325	328	331	304 334	307 337	310 340	313 343	316 346		
8.50		352	355	358	361	364	368	371	374	377	380	
A.	В.	0	1	2	8	4	5	6	7	8	9	Prop. Pts.

AD	D. { lo	$gb \cdot g(a)$	- log	ga = 1	: A. og a	+ <i>B</i> .		Su	лв. {	log a log (a	$-\log z - \delta$	gb = 0	B. $gb + A$ .
Α.	B.	0	1	2	8	4	5	6	7	8	9	Pı	rop. Pts.
8.50	10.0	352	355	358	361	364	368	371	374	377	380		
8.51 8.52		38 <u>3</u>	386 418	389 421	393 424	396 428	399 431	402	405 437	408 441	412	•	
8.53		447	450	454	457	460	464	434 467	470				
8.54		480	484	487	490	494	497	501	504	507	511		3   4
8.55 8.56		514 549	518 552	521 5 <b>5</b> 6	525 559	528 563	531 566	535 570	538 574	542 577	545 581	1	0.3 0.4
8.57		584	588	591	595	599	602	606	610	613		3	0.6 0.8 0.9 1.2
8.58		621	624 661	628 665	632	635	639	643	646 684	650 688	654	4	1.2 1.6 1.5 2.0
8.59 8.60	-	658 695	699	703	707	673	715	680	722	726	730	5	1.8 2.4
8.61	-	734	738	742	746	750	754	719 758	762	766	770	7 8	2.4 3.2
8.62		774	778	782	786	790	794	798	802	806	810	91	2.7 3.6
8.63		814	818	822	827	831	835	839	843 885	847	851		
8.64 8.65		856 898	860 902	864 906	868 911	872 915	877 919	881 924	928	889 932	894 937		
8,66		941	945	9 <u>5</u> 0	954	959	963	967	972	976	981	1	5   6
8.67 8.68	0.02	985	990	994	999	*003	*008	*012	*017 <b>0</b> 63	*02 I 067	*026	I 2	0.5 0.6 1.0 1.2
8.69	0.02	977	035	040 086	044 091	049 095	053 100	058 10 <u>5</u>	110	114	072	3	1.5 1.8
8.70	-	124	129	133	138	143	148	153	158	162	167	4 5 6	2.0 2.4 2.5 3.0
8.71	_	172	177	182	187	192	197	202	207	211	216		3.0 3.6 3.5 4.2
8.72 8.73		272	226 277	231 282	236 287	241 292	246 297	252 303	257 308	262 313	267 318	8	4.0 4.8
8.74		323	329	334	339	344	350	355	360		371	9	4.5  5 4
8.75 8.76		376	381	387	392	397	403	408	414 468	419	424		
8.77		430 48 <del>5</del>	435 490	441 496	446 502	452 507	457 513	463 518	524	474 530	479 535		
8.78		541	547	552	558	564	570	575	581	587	593		0.7 0.8
8.79	-	599	663	610	616	622	628 687	634	639	645	651	2	1.4 1.6
.8.80 8.81	-	657 717	723	669 729	675 735	681 742	748	693 754	699 760	705	711	3 4	2.1 2.4 2.8 3.2
8.82		779	785	791	797	803	810	816	822	829	835	5	3.5 4.0 4.2 4.8
8.83	<b>2</b> .	841	848	854	860	867	873	879	886	892	899	7 8	4.9 5.6
8.8 <sub>4</sub> 8.8 <sub>5</sub>		905 971	912 977	918 984	925 991	931 997	938 *004	944 *011	951 *017	957 *024	964 *031	9	5.6 6.4 6.3 7.2
8.86	0.03		044	051	ó <u>5</u> 8	ó65	<b>0</b> 7 i	078	085	092			
8.87 8.88	,	106	113 183	120	126	133	140	147	154 225	161	168		
8.89		175 247	254	190 261	197 268	204 276	211 283	218 290	298	232 305	312	] .	9   10
8.90	-	320	327	334	342	349	357	364	.371	379	386	- 1	0.0 1.0
8.91		394	401	409	417	424	432	439	447	455	462	2	1.8 2.0 2.7 3.0
8.92 8.93		470 548	478 555	485 563		501 579	509 587	516 595		532 611		3 4 5 6	3.6 4.0
8.01		627	635	643	651	659	667	675	683	691	700	6	4.5 5.0 5.4 6.0
8.95 8.96		708	716	724 807	732 816	741	749 832	757	765 849	774		8	0.31 7.0
8.97		790 875	799 883	892	901	909	918		1			9	7.2 8.0 8.1 9.0
8.98		96 i	970	979	987	996	*œ5	*Ó14	*023	*032	*040		
8.99	0.04		058	067	076	ó85	094 185	103			130		
9.00 A.	В.	139 0	148	157 2	167 8	176	185 5	194 <b>6</b>	203	8:	9	D.	rop. Pts.
_ 48.0	٠	V 1	* '		•	-				. 0,	1 0	. I')	CAN T FR

AD	o. { lo	g b - g (a	– log + ∂)	a = 1	: A. og a	+ <i>B</i> .		Su	тв. { }	log a log (a	— lo	$g b = B.$ $0) = \log b + A.$
A.	В.	0	1	2	8	4	5	6	7	8	9	Prop. Pts.
9.00	0.04	139	148	157	167	176	185	194	203	213	222	9   10   11
9.01		231 325	240 334	2 <u>5</u> 0 344	259 353	268 363	278 373	287 382	297 392	306 401	315	1 0.9 1.0 1.1
9.03		421	430	440	450	460	469	479	489	499	509	2 1.8 2.0 2.2 3 2.7 3.0 3.3
9.04		519 618	528 628	538	548	558	568	578	588	598	608	4 3.6 4.0 4.4 5 4.5 5.0 5.5
9.05		720	731	639 741	649 751	659 762	669 772	679 782	689 793	700 803	710 814	6 5.4 6.0 6.6
9.07		824	835	845	856	867	877	888	898	909	920	7 6.3 7.0 7.7 8 7.2 8.0 8.8
9.08	0.05	931 030	941 050	952 <b>0</b> 61	963 072	974 083	985 094	995 105	*006	*017 127	*028 139	9   8.1   9.0   9.9
9.10		150	161	172	183	195	206	217	229	240	251	12 13 14
9.11	•	263	274	286	297	308	320	332	343	355	366	2 2.4 2.6 2.8 3 3.6 3.9 4.2
9.12 9.13		378 496	<b>39</b> 0 <b>50</b> 8	401 519	413 531	425 543	436 555	448 567	460 579	472 591	484 604	4 4.8 5.2 5.6
9.14		616	628	640	652	664	677	689	701	714	726	6 7.2 7.8 8.4
9.15 9.16		738	751	763 889	775	788	800	813	825	838	851	7 8.4 9.1 9.8 8 9.6 10.4 11.2
9.10		863 991	876 *004	*017	901 *030	914 <b>*</b> 043	927 <b>*0</b> 56	939 *069	952 *082	965 *09 <u>5</u>	978 *108	9 10.8 11.7 12.6
9.18	0.06	121	134	147	161	174	187	200	214	227	240	15 16 17
9.19		254	267	281	<b>2</b> 94	308	321	335	348	362	376	2 3.0 3.2 3.4
9.21	-	389	403	417	430 569	<del>444</del> 583	458	472 612	486 626	500	513	4 6.0 6.4 6.8
9.21		527 668	541 683	555 697	711	725	597 740	754	769	640 783	654 798	5 7.5 8.0 8.5 6 9.0 9.6 10.2
9.23		812	827	841	856	870	885	900	914	929	944	7 10.5 11.2 11.9 8 12.0 12.8 13.6
9.24	0.07	959 108	973 123	988 138	*003 154	*018 169	*033 184	*048 199	*06 <u>3</u> 215	*078 230	*093 245	9 13.5 14.4 15.3
9.26	•	261	276	291	307	322	338	354	<b>3</b> 69	385	400	18 19 20 1 1.8 1.9 2.0
9.27 9.28		416 575	432 591	448 607	463 623	479	495	511 671	527 687	543	559	2 3.6 3.8 4.0
9.29		736	753	769	785	639 802	655 818	835	851	704 868	720 884	3 5+4 5.7 6.0 4 7.2 7.6 8.0
9.80		901	918	934	951	968	985	*001		*035	*052	5 9.0 9.5 10.0 6 10.8 11.4 12.0
9.31	0.08	-	086	103	120	137	154	171	188	206	223	7 12.6 13.3 14.0
9.32		240 415	257 432	275 450	292 468	309 485	327 503	344 521	362 539	379 557	397 574	8 14.4 15.2 16.0 9 16.2 17.1 18.0
9.34		592	610	628	646	664	683	701	719	737	755	21 22 23
9.35 9.36		774 958	792 977	810 996	829 *014	847 *033	865 *052	884 *071	902 *090	921 *108	940 *127	1 2.1 2.2 2.3 2 4.2 4.4 4.6
9.37	0.09	146	165	184	204	223	242	261	280	299	′	3 6.3 6.6 6.9 4 8.4 8.8 9.2
9.38		338 533	357 553	377 573	396	416 612	435	455	474 672	494	514	5 10.5 11.0 11.5 6 12.6 13.2 13.8
9.39 <b>9.40</b>	1	<u> </u>	752	773	<u>593</u> 793	813	833	853	874	692 894	712 914	7 14.7 15.4 16.1
9.41		935	955	976	<b>9</b> 96	*017		*058			*120	8   16.8   17.6   18.4 9   18.9   19.8   20.7
9.42 9.43	0. I <b>0</b>	141 351	162 373		204 415		246 458		288 501	309	,	24 25 26 1 2.4 2.5 2.6
9.43	l	565		609		437 652	674	479 696	1 -	522 739	1	2 4.8 5.0 5.2
9.45	٠	783	805	827	849	872	894	916	938	960	983	3 7.2 7.5 7.8 4 9.6 10.0 10.4
9.46 9.47	0.11	231	028 254	050 277	973 300	095	118	140 368	1 -			5 12.0 12.5 13.0 6 14.4 15.0 15.6
9.48		461	484	507	531	323 554	345 577	601	392 624	648	438 671	7 16.8 17.5 18.2
9.49		695			766	790	814		861		909	8 19.2 20.0 20.8 9 21.6 22.5 23.4
9.50 A.	B.	933	957 <b>1</b>	981 <b>2</b>	*005	*030 <b>4</b>	*054 <b>5</b>	*078 <b>6</b>				- There - Th
- Cha	, <u>v.</u>	-17	1 1		1 0	<u> </u>	1 0	1 0	7	8	9	Prop. Pts.

AD	n {·lo	g b . g (a	- log	ga = 1	$= A$ . $\log a$	+ <i>B</i> .		St	JB. {	log a	— lo	$g b = B.$ $0 = \log b + A.$
A.	B.	0	1	2	8	4	5	6	7	8	9	Prop. Pts.
9.50	0.11	933	957	981	*005	*030	*054	*078	*102	*127	*151	27   28   29   30
9.51	0.12	175 422	200	224	249	274	298	323	348	372 622	397	27 28 29 30 1 2:7 2.8 2.9 3.0
9.52		673	447 698	472 724	497 749	522 775	547 800	572   826	597   851	877	903	2 5.4 5.6 5.8 6.0 3 8.1 8.4 8.7 9.0
9.54		928	954	980	*006	*032	*o58	*084	*110	*136	*162	4 10.8 11.2 tr.5 12.0
9.55 9.56	0.13	188 452	479	240 505	267 532	293 559	319 <b>58</b> 6	346 613	372 640	399 667	425 694	5 13.5 14.0 14.5 15.0 6 16.2 16.8 17.4 18.0
9.57		721	748	775	802	829	857	884	911	939	966	7 18.9 19.6 20.3 21.0 8 21.6 22.4 23.2 24.0
9.58		994	*02 I	*049		*104	*132	*160	*188	*216	*244	9 24 . 3 25 . 2 26 . 1 27 . 0
9.59 <b>9.60</b>	9.14		300	328	356	384 668	412	441	469	497 783	526	31 32 33 34 1 3.1 3.2 3.3 3.4
9.61	-	554 841	583 870	899	640 928	957	697 986	726 *016	755 *045	703 *074	812 *104	2 6,2 6.4 6.6 6.8
9.62	0.15	133	162	192	221	95/ 25I	281	310	340	370	400	3 9.3 9.6 9.9 10.2 4 12.4 12.8 13.2 13.6
9.63	ŀ	430	460	489	520	550	580	610	640	670	701	5 15.5 16.0 16.5 17.0 6 18.6 19.2 19.8 20.4
9.64	0.16	731	761 068	792 099	822 130	853 161	8 <b>8</b> 4	914 224	94 <u>5</u> 25 <u>5</u>	976 286	*007 317	7 21 .7 22 .4 23 .1 23 .8
9.66		349	380	411	443	474	506	538	569	601	633	8 24 8 25 6 26 4 27.2 9 27 9 28 8 29 7 30 6
9.67		665	697	729	761	793	825	857	889	921	954	35   36   37   38
9.68 9.69	0.17	986 312	*018 345	*051 378	*083 411	*116 444	*148 477	*181 510	*214 544	*247 577	*279 610	1 3.5 3.6 3.7 3.8 2 7.0 7.2 7.4 7.6
9.70	, ·-	643	677	710	744	777	811	845	878	912	946	3 10.5 10.8 11.1 11.4
9.71	-	980	*014	*048	*082	*116	*150	*184	*218	*253	*287	4 14.0 14.4 14.8 15.2 5 17.5 18.0 18.5 19.0
9.72 9.73	0.18	322 668	356 703	390 738	425 773	460 808	494 844	<b>529</b> 879	564 914	<b>5</b> 99 <b>94</b> 9	63 <u>3</u> 985	6 21.0 21.6 22.2 22.8 7 24.5 25.2 25.0 26.6
9.74	0.19		056	091	127	163	198	234	270	306	342	8 28.0 28.8 29.6 30.4
9.75		378	414	450	486	522	558	595	631	667	704	9 31.5 32.4 33.3 34.2
9.76		740	777	813	850	887	923	960	997	*034	*071	1 3.9 4.0 4.1 4.2
9.78	0.20	108 481	145 519	182 557	220 594	257 632	294 670	331 708	369 746	406 784	444 822	2 7.8 8.0 8.2 8.4 3 11.7 12.0 12.3 12.6
9.79		860	898	937	975	*013	*052	*090	*128	*167	*206	4 15.6 16.0 16.4 16.8 5 19.5 20.0 20.5 21.0
9.80	0.21	244	283	322	361	399	438	477	516	556	595	6 23 4 24.0 24.6 25.2
9.81 9.82	0.22	634 029	673 <b>o</b> 69	712 109	752 149	791 189	831 229	870 269	309	949 349	989 389	7 27 3 28 0 28 7 29 4 8 31 2 32 0 32 8 33 0
9.83		430	470	510	551	591	632	673	713	754	795	9 35.1 36.0 36.9 37.8
9.84		836	877	918	959	*000	*041	*o82	*123	*165	*206	43 44 45 46 1 4.3 4.4 4.5 4.6
9.85 9.86		$\frac{247}{665}$	289 707	330 749		833	455 875	497   918	539 960	58ī *003	623 *045	2 8.6 8.8 9.0 9.2
9.87	0.24	-	130	173	216	258	301	344	387	430	473	3 12.9 13.2 13.5 13.8 4 17.2 17.6 18.0 18.4
9.88		516	559	603 *028	646 *082	689 *126	733 *170	776 *214	819 *2 <b>5</b> 8	863	907	5 21 .5 22 .6 22 .5 23 .0 6 25 .8 26 .4 27 .6 27 .6
9.90	0.25	950	994 434	*038 479	523	568	612	657	701	*302 746	*346 791	7 30.1 30.8 31.5 32.2
9.91		836				1 -		*106			*242	8 34 4 35 2 36 0 36 8 9 38 7 39 6 40 5 41 4
9.92	0.26	287	332	378	423	469	515	560	606	652	698	47 48 49 50
9.93	•	744	790	1	1	-	ľ		l		*160	1 4.7 4.8 4.9 5.0 2 9.4 9.6 9.8 10.0
9.9 <del>1</del> 9.95	İ	675	253 722	300 769		393 864	440 911	487 959	534 *006	581 *054	628 *101	3 14.1 14.4 14.7 15.0 4 18.8 19.2 19.6 20.0
9.96		149	197	245	292	340	388	436	484	532	581	5 23.5 24.0 24.5 25.0
9.97 9. <b>9</b> 8	0.29	629	677 163	726 212	1	310	871	920		*017	*066	6 28.2 28.8 29.4 30.0 7 32.9 33.6 34.3 35.0
9.99		606		705	1	ι×	359 854	409 903	458   953	507 *003	556 *053	8 37.6 38.4 39.2 40.0 9 42.3 43.2 44.1 45.9
0.00		103	153	203	253	303	354	404	454	505	555	2144,3143+4144-149-1
Α	В.	θ	1	2	8	4	5	6	7	8	9	Prop. Pts.

AD	o. { lo	g a - g (a	- log	b = 1	• A. og b	+ <i>B</i> .		Su	тв. {	log a log (a	$-\log z - b$	$gb = B.$ $0 = \log b + A.$
A.	B.	U	1	2	8	4	5	6	7	8	9	Prop. Pts.
0.00	0.30	103	153	203	253	303	354	404	454	505	555	lealer lealer
0.01		606	656	707	758	809	859	910	961	*012		50 51 52 53 1 5.0 5.1 5.2 5.3
0.02	0.31	629	166 188	217 732	268 784	320 836	371 888	422 940	474   992	526 *045	577 * <b>0</b> 97	2 10.0 10.2 10.4 10.6
0.04	0.32	-	201	254	306	359	411	464	517	569		3 15.0 15.3 15.6 15.9 4 20.0 20.4 20.8 21.2
0.05		675	728	78 i	834	887	940	993	*046	*100		5 25.0 25.5 26.0 26.5
0.06	0.33	207	260	314	367	421	474	528	582	636		6 30.0 30.6 31.2 31.8 7 35.0 35.7 36.4 37.1
0.07	0.34	744 287	798 342	852 396	906 451	960 506	<b>*0</b> 15 <b>5</b> 61	*069 616	*123 670	*178 726		8 40.0 40.8 41.6 42.4
0.09	0.34	836	891	946	*001	*057	*112			*279	781 *334	9 45 · 0 45 · 9 46 · 8 47 · 7
0.10	0.35	390	446	502	558	614	670	726	782	838	894	1 5-4 5-5 5-6 5.7
0.11		950	*007	*063	*119	*176	*233	*289	*346	*403	*459	2 10.8 11.0 11.2 11.4 3 16.2 16.5 16.8 17.1
0.12	0.36	516 088	573	630	687 260	744	801	858	916	973	*030	4 21.6 22.0 22.4 22.8
0.13	0.37	665	145	203 781		318 897	375	433 *014	491	549	607	5 27.0 27.5 28.0 28.5 6 32.4 33.0 33.6 34.2
0.15	0.38	247	723 306	365	839 423	482	955 541	600	*072 659	*130 718	*189 777	7 37.8 38.5 39.2 39.9
0.16	_	836	893	954		*073	*132	*191	*251		*370	8 43.2 44.0 44.8 45.6 9 48.6 49.5 50.4 51.3
0.17	0.39		489	549	609	669	729	789	849	909	969	58   59   60   6z
0.18	0.40	634	08 <u>9</u> 69 <u>5</u>	149 756	210 816	270 877	331 938	391 999	452 *061	512 *122	573 *183	1 5.8 5.9 6.0 6.1
0.20	0.41		306	367	428	490	552	613	675		798	3 17.4 17.7 18.0 18.3
0.21		860	922	984	*046	*108	*170	*232	*294	737 *357	*419	4 23.2 23.6 24.0 24.4
0.22	0.42	481	544	606	669	731	794	857	920	982		5 29.0 29.5 30.0 30.5 6 34.8 35.4 36.0 36.6
0.23	0.43	108	171	234	297	360	423	487	550	613	677	7 40.6 41.3 42.0 42.7
0.24	0.44	740 378	804	867	931	995	*058	*122	*186	*250		8 46.4 47.2 48.0 48.8 9 52.2 53.1 54.0 54.0
0.26	0.44	020	442 085	506 149	570 214	279	698 344	763 408	827 473	891 538	956 603	62   63   64   65
0.27		668	733	799	864	929	994				_	1 6.2 6.3 6.4 6.5 2 12.4 12.6 12.8 13.0
0.28	0.46	322	387	453	518	584	650	716	782	848	914	3 18.6 18.9 19.2 19.5
0.29	~ ~~	980	*046	*112	*178	*245	*311	*377	*444	*510		4 24.8 25.2 25.6 26.0 5 31.0 31.5 32.0 32.5
1 1	0.47	643	710	777	844	910	977	*044	*111	*178	*245	6 37.2 37.8 38.4 39.0
0.31	0.48	312 986	379 *054	447 *121	514 *189	581 *257	648 *32 <u>5</u>	716 *393	783 *461	851 *520	918 *597	7 43.4 44.1 44.8 45.5 8 49.6 50.4 51.2 52.0
0.33	0.49		733	801	869	938	*006	*074	*143	*211	*280	9 35.8 56.7 57.6 58.5
0.34		349	417	486	55 <u>5</u>	624	692	761	830	899	968	66 67 68 69 1 6.6 6.7 6.8 6.9
0.35	0.51	73I	107 801	176 870	245	314 *010	384 *080	4 <u>5</u> 3 *150	522 <b>*</b> 220	592 *289	*661	2 13.2 13.4 13.6 13.8
0.37	0.52		500	570	640	710	781	851	921	992	*360 * <b>0</b> 62	3 19.8 20.1 20.4 20.7 4 26.4 26.8 27.2 27.6
0.38	0.53	133	204	274	345	416	486	557	628	699	770	5 33-0 33-5 34-0 34-5
0.39		841	912	983	*055	*126	*197	*268	*340	*411	*483	6 39 6 40 2 40 8 41 4 7 46 2 46 9 47 6 48 3
0.40	0.54		626	697	769	841	912	984	*056	*128	*200	8 52.8 53.6 54.4 55.2
0.41 0.42	0.55	272 994	344 *066	416 *130	488	560 *284	632	704	777	849	921	9 59.4 60.3 61.2 62.1
0.43	0.56		794	867	940	*013	*086	*159	*232	*305	*370	70 71 72 73
0.44	0.57	452	525	<b>59</b> 9	672	746	819	893		•	*114	2 14.0 14.2 14.4 14.6
0.45	0.58		262	<b>3</b> 36	410	484	558	632	706	780	854	3 21.0 21.3 21.6 21.9 4 28.0 28.4 28.8 29.2
0.46			*003	_ :	_			*375			*598	5 35.0 35.5 36.0 36.5
0.48	0.60	422	748 497	822 572	897 648	972 723	*047 798	*122 874	*197 040	*272 *024	*347 *100	6 42.0 42.6 43.2 43.8 7 49.0 49.7 50.4 51.1
0.49	0.61	175	251	327	402	478	554	630	705	781	857	8 56.0 56.8 57.6 58.4 9 63.0 63.0 64.8 65.7
0.50		933	*009	*o85		*237	*314	*390	*466	*542		31°3.0103.9104.0105.7
Α.	В.	0	1	2	8	4	5	6	7	8	9	Prop. Pts.

 $\begin{cases} \log a - \log b = A. \\ \log (a + b) = \log b + B. \end{cases}$  $\begin{cases} \log a - \log b = B. \\ \log (a - b) = \log b + A. \end{cases}$ ADD. SUB. B. A. 1 Prop. Pts. \*o85 0.50 0.61 \*161 933 000 \*237 \*314 \*390 **\***466 \*542 \*619 74 75 o.62 695 0.51 848 \*00 I **\***077 \*154 \*231 \*307 771 924 \*384 7-4 7-5 7.6 0.52 0.63 461 538 615 692 768 845 \*000 \*077 \*154 923 2 14.8 15.0 15.2 463 540 0.53 0.64 231 308 386 618 695 773 850 928 22.2 22.5 22.8 3 0.65 005 083 160 238 29.6 30.0 30.4 0.54 316 394 472 549 627 705 783 861 \*0ì8|\*096 \*174 \*252 \*330 37.0 37.5 38.0 \*409 \*487 0.55 939 0.66 565 958 \*037 \*115 44.4 45.6 45.6 644 0.56 722 801 879 \*194 \*273 51.8 52.5 53.2 588 983 \*062 O.57 0.67 351 430 509 667 746 825 904 59.2 60.0 60.8 0.68 141 0.58 220 300 379 458 538 617 606 776 855 9 66.6 67.5 68.4 \*573 \*652 \*094 \*253 \*493 **'**014 \*174 \*333|\*413 0.59 935 77 | 78 | 79 0.60 0.69 732 812 892 \*293 7.7 7.8 7.9 972 \*052 \*132 \*212 \*373|\*453 15.4 15.6 15.8 0.61 0.70 533 855 614 \*257 \*096 694 774 935 \*016 \*177 23.1 23.4 23.7 580 0.62 0.71 338 419 661 742 823 \*065 499 904 984 30.8 31.2 31.6 0.63 0.72 146 227 308 390 47 I 633 552 714 877 796 38.5 39.0 39.5 46.2 46.8 47.4 \*121 0.64 958 **\***040 \*202 \*284 \*365|\*447 \*529 \*610|\*692 53.9 54.6 55.3 0.65 0.73 774 855 \*019 \* 101 \*183 \*264 \*346|\*428|\*510 937 8 61.6 62.4 63.2 839 \*003|\*085| <u>|\*168|\*250|\*332</u> 0.66 0.74 592 674 757 921 9 69.3 70.2 71.1 0.67 0.75 415 497 579 662 744 827 \*075 \*157 909 992 So | 81 | 82 0.68 488 0.76 240 323 406 571 654 737 820 986 903 8.0 8.1 8.2 0.69 0.77 069 318 568 152 235 401 485 651 818 16.0 16.2 16.4 734 0.70 901 984 **\***068 \*151 \*235 \*318|\*402 24.0 24.3 24.6 \*485 \*569 \*653 32.0 32.4 32.8 0.78 736 820 987 \*155 \*323 \*407 \*491 0.71 904 \*07 I \*239 40.0 40.5 41.0 743 827 \*079 \*163 \*248 \*332 0.72 0.79 575 659 911 995 48.0 48.6 49.2 585 669 \*007 \*091 \*176 0.80 416 838 56.0 56.7 57.4 0.73 500 754 922 64.0 64.8 65.6 0.74 0.81 261 513 684 769 345 430 599 854 938 \*023 9 72.0 72.9 73.8 0.75 0.82 108 278 363 448 618 703 193 533 788 873 83 | 84 | \*129 \*214 \*300 0.76 044 \*556 \*641 959 \*385|\*470 \*727 8.3 8.4 8.5 0.83 812 0.77 898 983 \*069 \*154 \*240|\*325|\*411|\*497|\*583 16.6 16.8 17.0 \*097|\*183|\*269|\*355|\*441 926 \*012 0.84 668 0.78 754 840 24.9 25.2 25.5 958 \*044 \*130 \*217 0.79 0.85 527 613 700 786 872 \*303 33.2 33.6 34.0 41.5 42.0 42.5 0.80 o.86 389 476 562 648 735 821 908 994 \*081|\*167 49.8 50.4 51.0 0.81 0.87 254 340 427 514 600 687 861 \*034 58.1 58.8 59.5 774 947 0.82 0.88 121 208 382 817 904 66.4 67.2 68.0 295 469 556 643 730 \*165 9 74-7 75-6 76.5 0.83 **'0**78 \*252 \*339 \*601 | \*689 | \*776 991 427 \*514 86 | 87 | 88 0.84 o.89 863 \*038|\*125 \*300|\*388|\*475|\*563|\*651 951 \*213 8.6 8.7 8.8 o.85 0.90 738 826 914 \*001 \*089 177 \*264 **\*352|\*440|\*528** 17.2 17.4 17.6 o.86 0.91 616 791 879 967 \*055|\*143 \*231 \*319 \*408 704 25 8 26.1 26.4 0.87 584 848 936 \*025 \*113 34-4 34.8 35.2 0.92 496 672 760 \*201 \*290 0.93 378 908 \*086 \*174 0.88 466 553 643 732 820 43.0 43.5 44.0 997 0.94 263 706 883 51.6 52.2 52.8 0.89 617 972 \*061 351 440 529 795 60.2 60.9 61.6 0.90 0.95 150 327 239 416 505 594 683 772 861 950 68.8 69.6 70.4 0.96 039 77-4 78-3 79.2 128 217 306 485 663 0.91 395 574 752 841 \*109 \*288 \*556 \*645 0.92 020 \*198 377 \*467 \*735 931 89 90 91 0.97 824 \*003 \*093 \*272 \*362 \*451 \*541 0.93 \*182 \*631 914 8 9 9 0 9.1 17.8 18.0 18.2 0.98 720 989 \*079 810 900 \*169|\*259|\*349|\*439|\*528 0.94 26.7 27.0 27.3 \*068|\*158|\*248|\*338|\*428 0.99 618 708 798 888 978 0.95 35.6 36.0 36.4 879 969 \*060 \*150 \*240 \*330 0.96 1.00 519 609 699 789 44-5 45-0 45-5 511 782 0.97 1.01 421 601 692 873 963 \*053|\*144|\*234 53.4 54.0 54.6 . 687 506 778 959 +050 +140 62.3 63.0 63.7 0.98 1.02 325 597 868 415 71.2 72.0 72.8 957 \*048 683 867 1.03 231 322 776 0.99 413 503 594 9 80.1 81.0 81.9 685 1.00 503 1.04 139 230 321 412 594 776 867 958 B. 2 0 1 8 5 6 7 8 9 Prop. Pts.

AD	D. { lo	ga g(a	- log	g <i>b</i> = 1	= <i>A</i> . og <i>b</i>	+ <i>B</i> .		St	ј <b>в.</b> {	log a	- lo a - b	$g b = B.$ $0) = \log b + A.$
<u>A.</u>	В.	0	1	2	8	4	5	6	7	8	9	Prop. Pts.
1.00	1.04	139	230	321	412	503	594	685	776	867	958	
1.01	ţ.05		140	232	323	414	505	596	687	779	870	17775 F-15
I.02	1.06	961 875		*144 *058	*149	*326	*418 *222	*424	*601	*692	*783 *699	1 9.1 9.2
1.04	1.07		882		*065			,	*432		,	2 18.2 18.4
1.05	1.08		800	891		*075	*167	*259	*351	*443	*525	3 27-3 27 6 4 36.4 36 8
1.06	1.09	- 1	719	811	903	995	*087	*179	*271	*363	*455	5 45.5 46 0
1.08	01.1		640	732	824	916	<b>*00</b> 9	*101	*193	*285	*378	6 54.6 55.2 7 63.764.4
1.00	I.II I.I2		562 486	65 <u>5</u> 579	747 671	839 764	932 857	949	*117 *042	*124	*301 *227	8 72.8 73.6 9 81.9 82.8
1.10	1.13		412	505	598	690	783	876		*061	*154	9 81.982.8
1.11	1.14		340	432	525	618	711	804	897		*083	
1.12	1.15	175	268	361	454		640	733	826	920	*013	93
I 13	1.16		199	292	385	478	571	665	758	851	944	1 9.3 2 18.6
I.14 I.15	1.17	037 97 I	131 <b>*</b> 064	224 *157	317 *251	411 *244	504 *428	597 *537	691 *625	784	877	3 27.9
1.16	1.18		999	*092	*186	*344 *279	*373	*467	*560	*654	*748	4   37.2 5   46.5
1.17	1.19	1	935	<b>*02</b> 9	*122	*216	*310	*403	*497	*501	*68₹	5 46.5 6 55.8
1.18	1.20		872		*060	*154	*248	*342	*435	*529	*623	7 65.1 8 74.4
1.19	1.21		811	905	999	*093			*375			9 83.7
1.20	1.22		751	845	939	*034			*316			
I.21 I.22	I.23 I.24	599 541	693 635	787 730	881 824	975 918	*070	*104	*258 *202	*352 *206	*447 *390	94
1.23	1.25		579	674	768	863	957	*052	*146	*24I	*335	1 9.4 2 18.8
1.24	1.26	430	524	619	714	808	903	<b>9</b> 97	*092	*187	*281	3 28.2
1.25 1.26	1.27	376	471 418	565	660 608	755	850	944	*039	*134	*229	4 37.6 5 47.0
1	1.20	323	367	513 462	1	703 652	797 746	892 841				6 56.4
1.27	1.30		316	411	507	602	697	792	887		*126 *077	7  65.8 8  75.2
1.29	1.31		267	362	458	553	648	743	838	933	1	8   75.2 9   <b>84</b> .6
1.30	1.32	124	219	314	410	505	600	695	791	886	981	
1.31		077	172	267	363	458	553	649	744	840	200	95   96
I.32	1.34	985	126 <b>*0</b> 81	221 *176	317 *272	412 *367	508 *463	603 *559	699 *6 <b>5</b> 4	794 *750	890 *845	1 9.5 9.6
1.34	1.35	941	*037		*228			*515			*802	2   19.0   19.2 3   28.5   28.8
1.35	1.36	898	994	*089	*185	*281	*377	*472	*568	*664	*760	4   38.0   38.4
1.36	1.37	856	951		*143			*431		1	*718	5 47.5 48.0 6 57.0 57.6
1.37	1.38	814	910 870		*102 *062		*294 *254	*390	*486	*582	*678	7   66.5   67.2 8   76.0   76.8
1.38 1.39	1.39 1.40		830	926	*022	*119	*21 <u>5</u>	*311	*407	*503	*638 *599	9 85.5 86.4
1.40			792	888		*080	*176	*273	*360	*465	*56I	
1.41	1.42	658		850	946	*043	*139	*235	*332	*428	*524	1 97
1.42	1.43	621	717	813	910	1,000	T102	T199	1295	<b>~391</b>	7488	1 9.7
1.43			681	777	874		****	1103	*259	*356	*452	2 19.4 3 29.1
I.44 I.45			645. 611	742 707	838 804		*031	*004	*100	*321 *287	*418 *384	3   29. I 4   38. 8 5   48. 5 6   58. 2
1.46	1.47			674			964	*060	*157	*254	*350	
1.47	1.48		544	641	737	834	931	<b>*028</b>	<b>*</b> 124	*221	*318	7 67.9
1.48	1.49	415	512	608	705	802	899	996	*093	*189	*286	8 77.6 9 87.3
1.49 1.50	-		480		674		868		*061			
	1.51 B.	352 0	449 1	546 <b>2</b>	643 <b>3</b>	740 4	837 <b>5</b>	934	_	_	*225	Dman D4s
. <b>A.</b>	"Д.	v		4	1 0	*	0	6	7	8	9	Prop. Pts.

ADI	o. { lo	ga.	ار بر	b = 1	: A.	+ <i>B</i> .	<u></u>	St	тв. {	log a	— lo	$gb = B.$ $0) = \log b + A.$
<u>A.</u>	B.	0	1	2	8 I	Τ Δ. 4	1 5	6	7	10g (a	1 9	Prop. Pts.
1.50	1.51	352	449	546	643	740	837	934	*031		*225	
1.51	1.52		419	516	613	710	807	904	*001	*098		*
1.52	1.53	292	389	486	583	680	778	875	972	<b>*0</b> 69	*166	
1.53	1.54	263	360	457	553	652	749	846	943	* <b>04</b> 0	*138	
1.54	1.55	235	332	429	526	624	721	818	915		*110	
1.55 1.56	1.56 1.57		304 277	402	499 472	596 569	693 667	791 764	888 861	985	*083 *056	
1.57	1.58		251	375 348	446		640	738	835		*030	97
1.58	1.59		225	322	420	543 517	$61\overline{5}$	712	810		*00 <u>5</u>	1 9.7
1.59	1.60		200	297	395	492	590	687	785	882		2 19.4 3 29.1
1.60	1.61	077	175	273	370	468	565	663	760	858	956	4 38.8
1.61	1.62		151	248	346	444	541	639	737	834	932	5 48.5 6 58.2
1.62	1.63		127	225	322	420	518	616	713	811	909	7 67.9
1.64	1.64	984	104 <b>*0</b> 81	202	299	397 *373	495 *470	<b>593</b>	690 *669	788 *=66	886	8 77.6 9 87.3
1.65	1.65		*059	*179 *157	*277 *255	3/5 *353	473 *451	*570 *548	*646	*711	*842	,,,,,
1.66			*o38	*136	*233	*331		*527				
1.67		919	*017	*115	*212	*310	*408	<b>*</b> 506	<b>*6</b> 04	*702	*800	
1.68	1.68				*192		*388	*486	*584	*682	*78o	
1.69	1.69				*172			*466				
1.70	1.70				*152			*446				
1.71	I.7I I.72		937	*035	*133 *114	*231		*427				98
I.72	1.73	_	899	998	*096	*194		*409 *390				1 9.8 2 19.6
1.74	1.74		881		*078		- 1	*373			-	3 29.4
1.75	1.75	766	864	962	*060	*159	*257	*355	*453	*552	*6 <u>5</u> 0	4 39.2 5 49.0
1.76	1.76	748	847		*043		<b>*24</b> 0	*338	*436	*535	*633	6 58.8
1.77	1.77		830		*026			*321				7 68.6 8 78.4
1.78	I.78 I.79		813 797	896	*010	*092		*305 *289				8 78.4 9 88.2
1.80	1.80		781	880		*077		*274				·
1.81	1.81		766	864		*061		*258		*455		·
1.82	1.82		751	849	948	<b>*04</b> 6	*145	*244	*342	*441	*539	
1.83	1.83	638	736	835	933	*032	*130	*229	*328	*426	*525	
1.84	1.84		722	820	919	*018		*215				
1.85 1.86	1.85 1.86		708 694	806 793		*004 990	*080	*201 *187	*299 *286	*398 *387	*497 *482	
1.87	1.87		681	779	1	977		*174	ľ			99 1 9.9
1.88	1.88		667	766		964	*062	*161	*260	*358	*457	1 9.9 2 19.8
1.89	1.89		655	753	852	951	<b>*</b> 050	*148	*247	*346	*443	3 29.7
1.90	1 90	543	642		840		*037	<b>*</b> 136	*235	*333	*432	4 39.6 5 49.5
1.91					827	926	*025	*124	*223	*321	*420	6 59.4
1.92		519	618		815	914	*013	*112	*211	*310	*408	6   59.4 7   69.3 8   79.2 9   89.1
1.93				-							*397 *386	9  89.1
1.94	1.94 1.95	490	595 583	694 682	792 781	891 880	990	*078	*177	*276	*375	
1.96											*364	}
1.97	1.97			661	760	859					*353	
1.98	1.98	452	551		1						*343	
1.99						1-2-					*333	
2.00											*323	
Α.	В.	0	1	2	8	4	5	6	7	8	9	Prop. Pts.

 $\log a - \log b = A.$   $\log a - \log b = B.$   $\log (a + b) = \log a + (B - A).$   $\log (a - b) = \log a - (B - A).$ 

A.	В.	В-А.	A.	В,	B-A.	A.	В.	ВА.
1.9823	1.9868	.00450	2.0337	2.0377	.00400	2.0920	2.0955	.00350
.9833	.9878	449	.0348	.0388	399	.0932	.0967	349
.9842	.9887	448	.0359	.0399	398	.0945	.0900	348
.9852	.9897	447	.0370	.0410	397	.0957	.0992	347
.9862	.9907	446	.0381	.0421	396	.0970	.1005	346
1.9872	1.9917	.00445	2.0392	2.0432	.00395	2.0982	2.1017	.00345
.9882	.9926	444 443	.0403	.0443	394	.0995	. 1029 . 1042	344
.9891	·9935 ·9945	443 442	.0414	.0454	393 392	.1000	.1042	343 342
.9911	.9955	441	.0437	.0476	391	. 1033	.1067	341
1.9921	1.9965	.00440	2.0448	2.0487	.00390	2.1046	2.1080	.00340
.9931	.9975	430	.0459	.0498	380	.1059	.1093	339
.9941	.9985	438	.0470	.0509	388	.1072	. 1106	338
.9951	-9995	437	.0481	.0520	387	. 1085	.1119	337
.9961	2.0005	436	.0493	.0532	386	. 1098	.1132	336
1.9971	2.0015	.00435	2.0504	2.0543	.00385	2.1111	2.1144	.00335
.9981	.0024	434	.0515	.0553	384	.1124	.1157	334
.9991	.0034	433	.0527	.0565	383	.1137	.1170	333
2.0001	.0044	432	.0538	.0576 .0588	382 381	.1150	.1183	332
1100.	2.0054	431	2.0561	2.0600	.00380	2.1176		331
2.0021	.0075	.00430	.0573	.0611	379	.1190	2.1209 .1223	00330 329
.0032	.0085	429	.0584	.0622	379	.1190	.1236	328
.0052	.0095	427	.0596	.0634	377	.1216	.1249	327
.0062	.0105	426	.0607	.0645	376	.1229	.1262	326
2.0073	2.0115	.00425	2.0619	2.0656	.00375	2.1243	2.1275	.00325
.0083	.0125	424	.0630	.0667	374	.1256	.1288	324
.0093	.0135	423	.0642	.0679	.373	.1270	. 1 302	323
.0104	.0146	422	.0654	.0691	372	.1283	.1315	322
.0114	.0156	421	.0666	.0703	371	.1297	.1329	321
2.0124	2.0166	.00420	2.0677	2.0714	.00370	2.1310	2.1342	.00320
.0135	.0177 .0187	419 418	.0689 .0701	.0726	369 368	.1324	.1356	319
.0145 .0156	.0107	417	.0713	.0738	367	.1338	.1370	317
.0166	.0208	416	.0725	.0762	366	.1365	1397	316
2.0177	2.0218	.00415	2.0737	2.0773	.00365	2.1379	2.1410	.00315
.0187	.0228	414	.0749	.0785	364	.1393	.1424	314
.0198	.0239	413	.0761	.0797	363	.1407	.1438	313
.0208	.0249	412	.0773	.0809	362	.1421	.1452	312
.0219	.0260	411	.0785	.0821	361	.1435	.1466	311
2.0229	2.0270	.00410	2.0797	2.0833	.00360	2.1449	2.1480	.00310
.0240	.0281	409	.0809	.0845	359	.1463	.1494	309
.0251	.0292	408	.0821	.0857	358	.1477	.1508	308
.0261	.0302	<b>4</b> 07 <b>4</b> 06	.0845	.0869	357 356	.1491	.1522	307 306
2.0283			2.0858	2.0893				
.0294	2.0324	.00405	.0870	.0905	.00355	2.1520 .1534	2,1550	.00305
.0305	.0334	403	.0882	.0905	353	.1548	.1578	303
.0315	.0355	402	.0895	.0930	352	.1563	.1593	302
.0326	.0366	401	.0907	.0942	351	.1577	.1607	301
2.0337	2.0337	.00400	2.0920	2.0955	.00350	2.1592	2 1622	.00300
A.	В.	B-A.	A	В.	B-A.	A.	В.	B-A.

 $\log a - \log b = A.$   $\log (a + b) = \log a + (B - A).$ 

 $\log a - \log b = B.$  $\log (a - b) = \log a - (B - A).$ 

Α.	В.	B-A.	A.	В.	B-A.	A.	В.	B-A.
2.1592	2.1622	.00300	2.2386	2.2411	.00250	2.3358	2.3378	.00200
.1606	.1636	299	.2403	.2428	249	•3379	.3399	199
.1621	. 1651	298	.2421	.2446	248	.3401	. 3421	198
.1635	. 1665	297	.2439	.2464	247	.3423	.3443	197
. 1650	. 1680	296	.2456	.2481	246	. 3446	. 3466	196
2.1665	2.1694	.00295	2.2474	2.2498	.00245	2.3468	2.3487	.00195
.1680	. 1709	294	.2492	.2516	244	. 3490	. 3509	194
.1694	.1723	293	.2510	.2534	243	.3513	.3532	193
.1710	. 1739	292 291	.2528	.2552 .2570	242 241	.3535	.3554	192
	2.1768	,00200	2.2564	2.2588	.00240	.3558	·3577	.00100
2.1739	.1783	280	.2582	.2606	239	2.3581 .3604	2.3600 .3623	180
.1754	. 1799	288	.2600	.2624	238	. 3627	.3646	188
.1785	.1814	287	.2618	.2642	237	.3650	.3669	187
.1800	.1829	286	.2637	.2661	236	. 3673	.3692	186
2.1815	2.1844	.00285	2.2656	2.2679	.00235	2.3697	2.3715	.00185
.1830	. 1858	284	.2674	.2697	234	.3720	.3738	184
.1846	. 1874	283	.2693	.2716	233	•3744	.3762	183
.1861	. 1889	282	. 2711	. 2734	232	.3768	.3786	182
.1877	. 1905	281	. 2730	.2753	231	. 3792	.3810	181
2.1892	2.1920	.00280	2.2749	2.2772	.00230	2.3816	2.3834	.00180
8001.	. 1936	279	. 2768	.2791	229	.3840	.3858	179
.1923	. 1951	278	.2787	.2810	228	.3865	.3883	178
.1939	.1967	277	.2806	. 2829	227	.3889	.3907	177
.1955	. 1983	276	. 2825	. 2848	226	.3914	.3932	176
2.1971	2.1998	.00275	2.2845	2.2867	.00225	2.3939	2.3956	.00175
.1987	.2014	274	.2864	.2886	224	. 3964	.3981	174
.2002	.2029	273	.2884	.2906	223	.3989		173
.2019	.2046	272	.2903	.2925	222	.4014	.4031	172
.2035	. 2062	271	.2923	.2945	221	.4039	.4056	171
2.2051	2.2078	.00270	2.2943	2.2965	.00220	2.4065	2.4082	.00170
.2067	.2094	269	.2962	.2984	219	.4090	.4107	169
.2083	.2110	268	.2982	.3004	218	.4116	.4133	168
.2099	.2126	267 266	.3002	.3024	217	.4142	.4159	167
.2116	.2143		.3022	. 3044	216	.4168	.4185	166
2.2132	2.2159	.00265	2.3043	2.3064	.00215	2.4195	2.4211	.00165
.2149	.2175	264	.3063	.3084	214	.4221	.4237	164
.2165	.2191	263 262	.3083	.3104	213	.4248	.4264	163 162
.2102	.2224	261	.3104 .3124	.3125	211	.4275 .4302	.4291	161
2,2215	2.224	.00260	2.3145	2.3166	.00210		2.4345	.00160
.2232	.2258	259	.3145	.3187	209	2.4329 .4356	.4372	159
.2249	.2275	258	.3187	.3208	208	.4383	.4399	158
.2266	.2292	257	.3208	.3229	207	.4411	.4427	157
.2283	.2309	256	.3229	.3250	206	.4439	.4455	156
2.2300	2.2325	.00255	2.3250	2.3271	.00205	2.4467	2.4482	.00155
.2317	.2342	254	.3271	.3291	204	.4495	.4510	154
.2334	.2359	253	.3293	.3313	203	.4523	.4538	153
.2351	.2376	252	.3314	.3334	202	.4552	.4567	152
.2369	.2394	251	. 3336	.3356	201	.4581	.4596	151
2.2386	2.2411	.00250	2.3358	2.3378	.00200	2.4609	2 4624	.00150
A.	B.	B-A.	Α.	В.	B-A.	A.	В.	B-A.

 $\log a - \log b = A.$ 

 $\log a - \log b = B.$  $\log(a+b) = \log a + (B-A). \qquad \log(a-b) = \log a - (B-A).$ 

A.	B.	B-A.	Λ.	В.	B-A.	A.	B.	В-А.
2.4609	2.4624	.00150	2.6373	2.6383	.00100	2.9385	2.9390	.00050
.4638	.4653	149	.6416	.6426	.00099	·947 <del>4</del>	.9479	49
.4668	.4683	148	.6461	.6471	98	.9563	.9568	48
.4697	.4712	147	.6505	.6515	97	.9655	.9660	47
.4727	.4742	146	.6550	.6560	96	.9748	·9753	46
2.4757 .4787	2.4773 .4801	.00145	2.6596	2.6606 .6651	.00095	2.9844	2.9848	.00045
.4817	.4831	144 143	.6688	.6697	94 93	2.9941 3.0041	2.9945 3.0045	44
.4818	4862	143		.6744	93	.0143	.0147	43 42
.4878	.4892	141	.6735 .6783	.6792	91	.0248	.0252	41
2.4910	2.4924	.00140	2.6831	2.6840	.00000	3.0356	3.0360	.00040
.4941	4955	139	.6880	.6889	<b>8</b> 9	.0466	.0470	39
.4972	.4986	138	.6928	.6937	88	.0578	.0582	38
.5004	. 5018	137	.6978	.6987	87	.0694	.0698	37
. 5036	. 5050	136	.7028	.7037	86	.0813	.0817	36
2.5068	2.5081	.00135	2.7079	2.7088	.00085	3.0935	3.0939	.00035
.5100	.5113	134	.7131	.7139	84	. 1061	.1064	34
.5133	. 5146	133	.7183	.7191	83	.1191	.1194	33
.5165	.5178	132	.7236	.7244	82 81	.1324	.1327	32
.5199	. 5212	131	.7289	.7297		.1463	.1466	3I
2.5232	2.5245	.00130	2.7343	2.7351	.00080	3.1606	3.1609	.00030
.5266	. 5279	129 128	.7398	.7406 .7461	79 78	.1753	.1756	29 28
·5299	. 5312 . 5346	120	·7453 ·7509	.7517	77	.1905	.1908 .2066	27
.5368	.5381	126	.7566	.7574	76	,2226	.2229	26
2.5402	2.5415	.00125	2.7623	2.7631	.00075	3.2396	3.2399	.00025
.5437	.5449	124	.7682	.7689	74	.2575	.2577	24
5472	.5484	123	.7741	.7748	73	.2760	.2762	23
.5508	. 5520	122	.7801	.7808	72	.2952	.2954	22
.5544	.5556	121	.7862	.7869	71	.3154	.3156	21
2.5580	2.5592	.00120	2.7923	2.7930	.00070	3.3366	3.3368	.00020
.5616	. 5628	119	.7985	.7992	69	.3590	.3592	19
.5653	. 5665	218	.8050	.8057	68	. 3825	. 3827	18
. 5690	. 5702	317	.8114	.8121	67	.4072	.4074	17
.5727	-5739	116	.8180	.8187	66	·4335	-4337	16
2.5765	2.5776	.00115	2.8245	2.8252	.00065	3.4617	3.4619	.00015
. 5803	.5814	114	.8313	.8319	64	.4917	.4918	14
. 5841	. 5852 . 5891	113	.8381 .8451	.8387 .8457	63 62	.5237 .5587	.5238 .5588	13
.5919	. 5930	111	.8521	.8527	61	.5964	.5965	11
2.5958	2.5969	01100.	2.8593	2.8599	.00060	3.6377	3.6378	.00010
.5998	.6009	100	.8666	.8672	59	.6835	.6836	09
.6038	.6049	108	.8741	.8747	58	.7345	.7346	08
6079	.6090	107	.8816	.8822	57	.7925	.7926	07
.6120	:6131	106	.8893	.8899	56	.8595	.8596	<b>o</b> 6
2.6161	2.6172	.00105	2.8971	2.8977	,00055	3.9390	3.9391	.000075
.6202	.6212	104	.9051	.9056	54	4.0355	4.0355	04
.6244	.6254	103	.9132	.9137	53	4.1600	4.1600	<b>0</b> 3
.6287	.6297	102	.9215	.9220	52	4.3375	4.3375	02
2.6373	2.6383	101	2.9385	2.9390	.00050	4.6367 ∞	4.6367	10
2.03/3 A.	B.	B-A.	2.9305 A.				·	
Δ.	В.	D-A.	Λ.	В.	B-A.	A.	В.	B-A.

## TABLE VII.

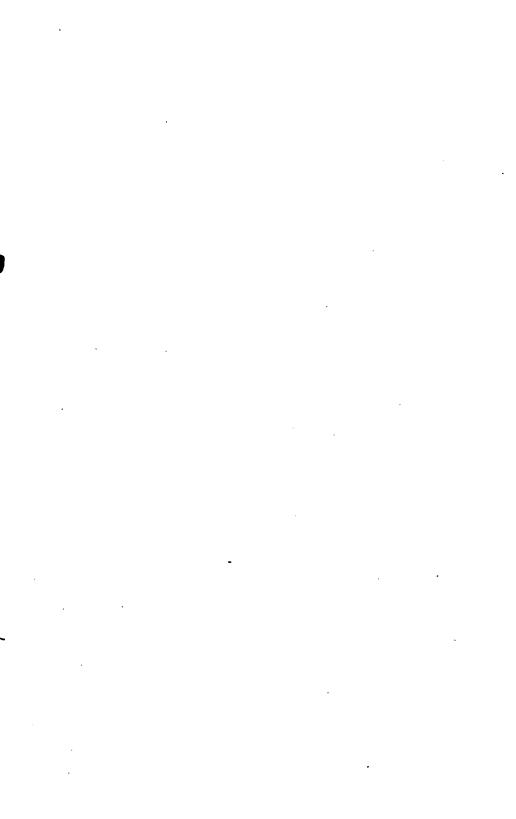
## SQUARES OF NUMBERS.

No.	Square.	No.	Square.	No.	Square.	No.	Square.	No.	Square.
0	0	20	400	40	1600	60	3600	80	6400
1	I	. 21	441	41	1881	61	3721	81	6561
2	4	22	484	42	1764	62	3844	82	6724
3	. 9	23	529	43	1849	63	3969	83	6889
4	16	24	576	44	1936	64	4096	84	7056
5	25	25	625	45	2025	65	4225	85	7225
6	36	26	676	46	2116	66	4356	86	7396
7	49	27	729	47	2209	67	4489	87	7569
8	64	28	784	48	2304	68	4624	88	7744
9	81	29	841	49	2401	69	4761	89	7921
10	100	30	900	50	2500	70	4900	90	8100
11	121	31	961	51	2601	71	5041	91	8281
12	144	32	1024	52	2704	72	5184	92	8464
13	169	33	1089	53	2809	73	5329	93	8649
14	196	34	1156	54	2916	74	5476	94	8836
15	225	35	1225	55	3025	75	<b>5</b> 625	95	9025
16	256	36	1296	56	3136	76	5776	96	9216
17	289	37	1369	57	3249	77	5929	97	9409
18	324	38	1444	58	3364	78	6084	98	9604
19	361	39	1521	59	3481	<b>7</b> 9	6241	99	9801
20	400	40	1600	60	3600	80	6400	100	10000

	144	244	300	400	544	644	744	844	900	1	Diff.
00	100	400	900	1600	2500	3600	4900	6400	8100		
01	102	404 408	906	1608	2510	3612	4914	6416	8118	01	3
02 03	104 106	408 412	912 918	1616 1624	2520 2530	3624 3636	4928 4942	6432 6448	8136 8154	04 09	5 7
04	108	416	924	1632	2540	3648 3660	4956	6464 6480	8172	16	9
05 06	110	420 424	930 936	1640 -1648	2550 2560	3672	4970 4984	6496	8190 8208	25 36	11
07 08	114 . 116	428 432	942 948	1656 1664	2570 2580	3684 3696	4998 5012	6512 6528	8226 8244	49 64	15
09	118	436	954	1672	2590	3708	5026	6544	8262	81	17
10	121	441	961	1681	2601	3721	5041	6561	8281	∞	21
II. I2	123 125	445 449	967 973	1689 1697	2611 2621	3733 3745	5055 5069	6577 6593	8299 8317	21 44	23 25
13	127	453	979	1705	2631	3757	5083	6609	8335	69	27
14 15 16	132	457 462	985 992	1713	2641 2652 2662	3769 3782	5097 5112	6625 6642	8353 8372	96 25	29* 31
17	134	466 470	998	1730	2672	3794 3806	5126 5140	6658 6674	8390 8408	56 89	33
18 19	139	475 479	1011	1747 1755	2683 2693	3819 3831	5155 5169	6691 6707	8427 8445	24 61	35** 37
20	144	484	1024	1764	2704	3844	5184	6724	8464	00	39* 41
21	146	488	1030	1772 1780	2714	3856	5198	6740	8482	41	43
22	148	492 497	1036	1780	2724 2735	3868 3881	5212 5227	6756 6773	8500 8519	84 29	45* 47
24 25	153 156	501 506	1049 1056	1797 1806	2745 2756	3893 3906	5241 5256	6789 6806	8537	76 25	49*
25 26	158	510	1062	1814	2766	3918	5270	6822	8556 8574	76	51 53*
27 28	161 163	515 519	1069 1075	1823 1831	2777 2787	3931 3943	5285 5299	6839 6855	8593 8611	29 84	55
29	166	524	1075	1840	2798	3956	5314	6872	8630	4I	57* 59*
80	169	529	1089	1849	2809	3969	5329	6889	8649	∞ 	61
31 32	171	533 538	1095 1102 1108	1857 1866 1874	2819 2830	3981 3994	5343 5358	6905 6922	8667 8686	61 24	63* 65
33 34	176	542 547	1115	1883	2840 2851	4006	5372 5387	6938 6955	8704 8723	89 56	67
35 36	179 182 184	552 556	1122	1892 1900	2862 2872	4032 4044	5402 5416	6972	8742 8760	25 96	69* 71
37 38	187	561	1135	1900	2883	4057	5431	7005	8779	69	73* 75*
38 39	193	566 571	1142 1149	1918 1927	2894 2905	4070 4083	5446 5461	7022 7039	8798 8817	44 21	77* 79*
40	196	576	1156	1936	2916	4096	5476	7056	8836	∞	8r
41 42	198 201	580 585	1162 1169	1944 1953	2926 2937	4108 4121	5490 5505	7072 7089	8854 8873	81 64	83*
43	204	590	1176	1962	2948 2948	4134	5520	7106	8892	49	85* 87*
44 45	207 210	595 600	1183 1190	1971 1980	2959 2970	4147 4160	5535 5550	7123 7140	8911 8930	36 25	89*
46	213	605	1197	1989	2981	4173	5565	7157	8949	25 16	91 ° 93 °
47 48	216 219	615	1204	1998 2007	2992 3003	4186 4199	5580 5595	7174 7191	8968 8987	09 04	95* 97*
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53 54 55	234 237 240	645 650	1253	2061 2070	3069 3080	427 <b>7</b> 4290	5685 5700	7293 7310	9101 9120	16	9
55 56	243 246	655 660	1267 1274	2079 2088	3091 3102	4303 4316	5 <b>715</b> 5730	7327 7344	9139 9158	25 36 49	13
57 58 59	249 252	665 670	1281	2097 2106	3113 3124	4329 4342	5745 5760	7361 7378	9177 91 <b>9</b> 6	64 81	15 17 19*
60	256	676 681	1296	2116	3136	4356	5776	7396	9216	00	21
61 62 63	259 262 265	686 691	1303 1310 1317	2125 2134 2143	3147 3158 3169	4369 4382 4395	5791 5806 5821	7413 7430 7447	9235 9254 9273	21 44 69	23 25 27
64 65 66	268 272 275	696 702 707	1324 1332 1339	2152 2162 2171	3180 3192 3203	4408 4422 4435	5836 5852 5867	7464 7482 7499	9292 9312 9331	96 25 56	29* 31 33
67 68 69	278 282 285	712 718 723	1346 1354 1361	2180 2190 2199	3214 3226 3237	4448 4462 4475	5882 5898 5913	7516 7534 7551	9350 9370 9389	89 24 61	35** 37' 39**
70	289	729	1369	2209	3249	4489	5929	7569	9409	∞	43
71 72 73	292 295 299	734 739 745	1376 1383 1391	2218 2227 2237	3260 3271 3283	4502 4515 4529	5944 5959 5975	7586 7603 7621	9428 9447 9467	41 84 29	43 45** 47
74 75 76	302 306 309	750 756 761	1398 1406 1413	2246 2256 2265	3294 3306 3317	4542 4556 4569	5990 6006 6021	7638 7656 7673	9486 9506 9525	76 25 76	49 <sup>8</sup> 53 53 <sup>8</sup>
77 78 79	313 316 320	767 772 778	1421 1428 1436	2275 2284 2294	3329 3340 3352	4583 4596 4610	6037 6052 6068	7691 7708 7726	9545 9564 9584	29 84 41	55 57** 59**
80	3 <del>24</del>	784	1444	2304	3364	4624	6084	7744	9604	∞	61 61
81 82 83	3 <sup>2</sup> 7 33 <sup>1</sup> 334	789 795 800	1451 1459 1466	2313 2323 2332	3375 3387 3398	4637 4651 4664	6099 6115 6130	7761 7779 7796	9623 9643 9662	61 24 89	63* 63 67*
84 85 86	338 342 345	806 812 817	1474 1482 1489	2342 2352 2361	3410 3422 3433	4678 4692 4705	6146 6162 6177	7814 7832 7849	9682 9702 9721	56 25 96	69* 71 73*
87 88 89	349 353 357	823 829 835	1497 1505 1513	2371 2381 2391	3445 3457 3469	4719 4733 4747	6193 6209 6225	7867 7885 7903	9741 9761 9781	69 44 21	75* 77* 79*
90	361	841	1521	2401	3481	4761	6241	7921	9801	∞	8z
91 92 93	364 368 372	846 852 858	1528 1536 1544	2410 2420 2430	3492 3504 3516	4774 4788 4802	6256 6272 6288	7938 7956 7974	9820 9840 9860	81 64 49	83* 85* 87*
94 95 <b>9</b> 6	376 380 384	864 870 876	1552 1560 1568	2440 2450 2460	3528 3540 3552	4816 4830 4844	6304 6320 6336	7992 8010 8028	9880 9900 9920	36 25 16	89* 91* 93*
97 98 <b>9</b> 9	388 392 396	882 888 894	1576 1584 1592	2470 2480 2490	3564 3576 3588	4858 4872 4886	6352 6368 6384	8046 8064 8082	9940 9960 9980	09 04 01	95* 97* 99*
100	400	900	1600	2500	3600	4900	6400	8100	10000	∞	<u> </u>



D.	H. M. S.	H, M. S.	H.M.S.	D.	H. M. S.	H. M. S.	H.M.S.
<i>d</i> .	h. m. s.	m. s.	s.	<i>d</i> .	h. m. s.	m, s.	<u>s.</u>
0.01	0 14 24	o 8.64	0.09	0.51	12 14 24	7 20.64	4.41
0.02	0 28 48	o 17.28	0.17	0.52	12 28 48	7 29.28	4.49
0.03	0 43 12	o 25.92	0.26	0.53	12 43 12	7 37.92	4.58
0.04	0 57 36	o 34.56	0.35	0.54	12 57 36	7 46.56	4.67
0.05	1 12 0	o 43.20	0.43	0.55	13 12 0	7 55.20	4.75
0.06	1 26 24	0 51.84	0.52	0.56	13 26 24	8 3.84	4.84
0.07	1 40 48	1 0.48	0.60	0.57	13 40 48	8 12.48	4.92
0.08	1 55 12	1 9.12	0.69	0.58	13 55 12	8 21.12	5.01
0.09	2 9 36	1 17.76	0.78	0.59	14 9 36	8 29.76	5.10
0.10	2 24 0	1 26.40	0.86	0.60	14 24 0	8 38.40	5.18
0.11	2 38 24	I 35.04	0.95	0.61	14 38 24	8 47.04	5.27
0.12	2 52 48	I 43.68	1.04	0.62	14 52 48	8 55.68	5.36
0.13	3 7 12	I 52.32	1.12	0.63	15 7 12	9 4.32	5.44
0.14	3 21 36	2 0.96	1.21	0.64	15 21 36	9 12.96	5.53
0.15	3 36 0	2 9.60	1.30	0.65	15 36 0	9 21.60	5.62
0.16	3 50 24	2 18.24	1.38	o.66	15 50 24	9 30.24	5.70
0.17	4 4 48	2 26.88	1.47	o.67	16 4 48	9 38.88	5.79
0.18	4 19 12	2 35.52	1.56	o.68	16 19 12	9 47.52	5.88
0.19	4 33 36	2 44.16	1.64	o.69	16 33 36	9 56.16	5.96
0.20	4 48 0	2 52.80	1.73	o.70	16 48 0	10 4.80	6.05
0.21	5 2 24	3 1.44	1.81	0.71	17 2 24	10 13.44	6.13
0.22	5 16 48	3 10.08	1.90	0.72	17 16 48	10 22.08	6.22
0.23	5 31 12	3 18.72	1.99	0.73	17 31 12	10 30.72	6.31
0.24	5 45 36	3 27.36	2.07	0.74	17 45 36	10 39.36	6.39
0.25	6 0 0	3 36.00	2.16	0.75	18 0 0	10 48.00	6.48
0.26	6 14 24	3 44.64	2.25	0.76	18 14 24	10 56.64	6.57
0.27	6 28 48	3 53.28	2.33	0.77	18 28 48	11 5.28	6.65
0.28	6 43 12	4 1.92	2.42	0.78	18 43 12	11 13.92	6.74
0.29	6 57 36	4 10.56	2.51	0.79	18 57 36	11 22.56	6.83
0.30	7 12 0	4 19.20	2.59	0.80	19 12 0	11 31.20	6.91
0.31	7 26 24	4 27.84	2.68	0.81	19 26 24	11 39.84	7.00
0.32	7 40 48	4 36.48	2.76	0.82	19 40 48	11 48.48	7.08
0.33	7 55 12	4 45.12	2.85	0.83	19 55 12	11 57.12	7.17
0.34	8 9 36	4 53.76	2.94	0.84	20 9 36	12 5.76	7.26
0.35	8 24 0	5 2.40	3.02	0.85	20 24 0	12 14.40	7.34
0.36	8 38 24	5 11.04-	3.11	o.86	20 38 24	12 23.04	7·43
0.37	8 52 48	5 19.68	3.20	o.87	20 52 48	12 31.68	7·52
0.38	9 7 12	5 28.32	3.28	o.88	21 7 12	12 40.32	7·60
0.39	9 21 36	5 36.96	3.37	o.89	21 21 36	12 48.96	7·69
0.40	9 36 0	5 45.60	3.46	o.90	21 36 0	12 57.60	7·78
0.41	9 50 24	5 54.24	3.54	0.91	21 50 24	13 6.24	7.86
0.42	10 4 48	6 2.88	3.63	0.92	22 4 48	13 14.88	7.95
0.43	10 19 12	6 11.52	3.72	0.93	22 19 12	13 23.52	8.04
0.44	10 33 36	6 20.16	3.80	0.94	22 33 36	13 32.16	8.12
0.45	10 48 0	6 28.80	3.89	0.95	22 48 0	13 40.80	8.21
0.46	11 2 24	6 37.44	3.97	0.96	23 2 24	13 49.44	8.29
0.47	11 16 48	6 46.08	4.06	0.97	23 16 48	13 58.08	8.38
0.48	11 31 12	6 54.72	4.15	0.98	23 31 12	14 6.72	8.47
0.49	11 45 36	7 3.36	4.23	0.99	23 45 36	14 15.36	8.55
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	25 26 27 28 29	I	40 44 48 52 56	85 86 87 88 89	5 5 5 5	40 44 48 52 56	145 146 147 148 149	9	40 44 48 52 56	205 206 207 208 209			265 266 267 268 269		44 48	325 326 327 328 329	21 21 21 21 21	40 44 48 52 56	25 26 27 28 29	1	40 44 48 52 56	25 26 27 28 29	1.6 1.7 1.8 1.8	33 00 66
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	42 41 42 43 44	2 2	40 44 48 52 56	100 101 102 103 104	6 6	48	160 161 162 163 164	10 10	40 44 48 52 56	220 221 222 223 224	14 14	44 48 52	280 281 282 283 284	18 18	40 44 48 52 56	340 341 342 343 344	22 22 22 22 22	40 44 48 52 56	40 41 42 43 44	2	40 44 48 52 56	40 41 42 43 44	2.6 2.7 2.8 2.8 2.9	733 800 866
	45 46 47 48 49	3	0 4 8 12 16	108	777	0 4 8 12 16	165 166 167 168 169	11	0 4 8 12 16	228	15	0 4 8 12 16	288	19 19	0 4 8 12 16	348	23 23	0 4 8 12 16	45 46 47 48 49	33333	0 4 8 12 16	45 46 47 48 49	3.0 3.1 3.2 3.2	33 200
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	55 56 57 58 <b>59</b>	3 3 3 3	40 44 48 52 56	115 116 117 118 119	777	40 44 48 52 56	175 176 177 178 179		40 44 48 52 56	235 236 237 238 239	15 15	40 44 48 52 56	295 296 297 298 299	19 19	44 48 52	355 356 357 358 359	23 23 23 23 23	40 44 48 52 56	55 56 57 58 <b>5</b> 9	3 3 3 3	40 44 48 52 56	55 56 57 58 59	3.6 3.7 3.8 3.8 3.9	733 800 866

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I	0 10 20 30 40 50	0	9.86 11.50 13.14 14.78 16.43 18.07	9	0 10 20 30 40 50	1	28.71 30.35 31.99 33.64 35.28 36.92	17	0 10 20 30 40 50	2	47.56 49.20 50.85 52.49 54.13 55.77	2	20 30 40 50 0 10 20 30	0.22 0.25 0.27 0.30 0.33 0.36 0.38 0.41
2	0 10 20 30 40 50	0	19.71 21.36 23.00 24.64 26.28 27.93	IO -	0 10 20 30 40 50	I	38.56 40.21 41.85 43.49 45.14 46.78	18	0 10 20 30 40 50	3	57.42 59.06 0.70 2.34 3.99 5.63	3	40 50 0 10 20 30 40 50	0.44 0.47 0.49 0.52 0.55 0.57 0.60 0.63
3	0 10 20 30 40 50		29.57 31.21 33.86 34.50 36.14 37.78	11	0 10 20 30 40 5	I	48.42 50.06 51.71 53.35 54.99 56.64	19	0 10 20 30 40 50	3	7.27 8.92 10.56 12.20 13.84 15.49	. 5	0 10 20 30 40 50	0.66 0.68 0.71 0.74 0.77 0.79
4	0 10 20 30 40 50	0	39.43 41.07 42.71 44.35 46.00 47.64	12	0 10 20 30 40 50	I 2	58.28 59.92 1.56 3.21 4.85 6.49	20	0 10 20 30 40 50	3	17.13 18.77 20.42 22.06 23.70 25.34	6	10 20 30 40 50	0.85 0.88 0.90 0.93 0.96 0.99
5	0 10 20 30 40 50	0	49.28 50.92 52 57 54.21 55.85 57.50	13	0 10 20 30 40 50	2	8.13 9.78 11.42 13.06 14.70 16.35	21	0 10 20 30 40 50	3	26.99 28.63 30.27 31.91 33.56 35.20	7	20 30 40 50 0 10 20 30	1.04 1.07 1.10 1.12 1.15 1.18 1.21 1.23
6	0 10 20 30 40 50	OI	59.14 0.78 2.42 4.07 5.71 7.35	14	0 10 20 30 40 50	2	17.99 19.63 21.28 22.92 24.56 26.20	22	0 10 20 30 40 50	3	36.84 38.48 40.13 41.77 43.41 45.06	8	40 50 0 10 20 30 40 50	1.26 1.29 1.31 1.34 1.37 1.40 1.42 1.45
7	0 10 20 30 40 50	1	9.00 10.64 12.28 13.92 15.57 17.21	15	0 10 20 30 40 50	2	27.85 29.49 31.13 32.77 34.42 36.06	23	0 10 20 30 40 50	3	46.70 48.34 49.98 51.63 53.27 54.91	9	0 10 20 30 40 50	1 .48 1 .50 1 .53 1 .56 1 .59 1 .62

104		IAI	SLE XO.	-10	CON	VE.	KI SIDI	LKEA	T 1	NIC	MEAN	TIN	1L.	
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ı	0 10 20 30 40 50	0	9.83 11.47 13.11 14.74 16.38 18.02	9	0 10 20 30 40 50	I	28.47 30.10 31.74 33.38 35.02 36.66	17	0 10 20 30 40 50	2	47.10 48.74 50.38 52.02 53.66 55.29	2	20 30 40 50 0 10 20 30	0.22 0.25 0.27 0.30 0.33 0.35 0.38 0.41
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5	0 10 20 30 40 50	0	49.15 50.79 52.42 54.06 55.70 57.34	13	0 10 20 30 40 50	2	7.78 9.42 11.06 12.70 14.34 15.98	21	0 10 20 30 40 50	3	26.42 28.06 29.70 31.34 32.97 34.61	7	30 40 50 0 10 20 30	1.06 1.09 1.12 1.15 1.17 1.20 1.23
6	0 10 20 30 40 50	1	58.98 0.62 2.25 3.89 5.53 7.17	14	0 10 20 30 40 50	2	17.61 19.25 20.89 22.53 24.17 25.80	22	0 10 20 30 40 50	3	36.25 37.89 39.53 41.16 42.80 44.44	8	40 50 0 10 20 30 40 50	1.26 1.28 1.31 1.34 1.37 1.39 1.42 1.45
7	0 10 20 30 40 50	I	8.81 10.44 J2.08 13.72 15.36 17.00	15	0 10 20 30 40 50	2	27.44 29.08 30.72 32.36 34.00 35.64	23	10 20 30 40 50	3	46.08 47.72 49.36 51.00 52.63 54.27	9	0 10 20 30 40 50	1.47 1.50 1.53 1.56 1.58 1.61







## TABLES

MATHERIA LAL COURSE

4 F F S 47 K W - 1 P T ERS